

PROJECT HYDROLOGY REPORT

FOR

**ANSUYA ENTERPRISE OF CLINTON, L.L.C
ANSUYA RIVERBEND, L.L.C**

**BLOCK 17, LOT 2
BLOCK 18, LOTS 2.03, 2.04, 6
TOWN OF CLINTON
HUNTERDON COUNTY, NJ**

Project #020128104

**September 20, 2002
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Prepared For:

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A. PURPOSE

This report is intended to demonstrate compliance with the Town of Clinton and Hunterdon County Land Development Ordinances and the New Jersey Department of Environmental Protection (NJDEP) regulations. The regulation requires the storm-water management to attenuate the 2, 10 and 100-year storm post development peak runoff to 50%, 75% and 80% of its pre-development peak runoff values. The report contains storm sewer collection computations, stormwater basin design and routings, water quality analysis and soil erosion computations.

B. PROJECT LOCATION & DESCRIPTION

The site is currently shown on the Town of Clinton Tax Maps as Block 17, Lot 2 and Block 18 , Lots 2.03, 2.04 and 6 totals 13± acres situated along NJ State Highway 31 northbound in the Town of Clinton, Hunterdon County. The applicant proposes to construct a three (3) story, 100 room, 56,946 SF hotel, a 7,500 SF restaurant, and a 21,660 SF office building with a parking area with 274 parking spaces. The access to the site is proposed from Route 31. The proposed development is located within Block 18, Lot 2.03 and 2.04. The remaining lots are proposed to remain undeveloped due to environmental constraints.

C. SITE HYDROLOGIC ANALYSIS & METHODOLOGY

A hydrologic analysis of the site was performed to determine the peak rates of stormwater runoff so that adequate measures for drainage conveyance and stormwater management may be designed and implemented. A separate analysis has been made for pre-development and post-development conditions using the southwesterly corner of the site as the point of study.

Hydrologic computations are accomplished with Hydraflow Hydrographs 2002 computer program, using USDA Soil Conservation Service (SCS) methodology as described in National Engineering Handbook, Section 4 - Hydrology (NEH-4). The SCS Type III, 24-hour storm distribution was used to develop runoff hydrographs. The following 24-hour rainfall values for Hunterdon County were used:

| TABLE NO. 1 Rainfall Frequency | |
|--|-----------------|
| FREQUENCY | RAINFALL |
| 2 year | 3.2" |
| 10 year | 5.0" |
| 25 year | 5.7" |
| 50 year | 6.5" |
| 100 year | 7.3" |

Runoff Curve Number values were selected to reflect the soils and land uses on the site for both pre- and post-development conditions. The values were taken from "Urban Hydrology for Small Watersheds, TR-55" by SCS, 1986. The following values were used in the analysis presented in this report:

| TABLE NO. 2 Curve Number Data | |
|---|----------------------------------|
| LAND USE | HYDROLOGIC SOIL GROUP "B" |
| Woods | 55 |
| Open Space (Lawn, Good Condition) | 61 |
| Impervious Area | 98 |

Times of concentration were also calculated using SCS methodology as described in TR-55 (Refer to Table 3-1 of TR-55).

D. PRE-DEVELOPMENT CONDITIONS ANALYSIS

The site consists of approximately 8.3± acres of drainage area and generally drains in the westerly direction towards the South Branch of the Raritan River. The site is presently undeveloped and consists of brush and scrub vegetation and hardwood forest. The upland portion of the site located in the eastern portion of the site consists of medium slopes (5%-7%) and the areas in the western portion of the site along the river consist of steep slopes in excess of 30%. The area located along the Raritan River is not included in the

site consists of medium slopes (5%-7%) and the areas in the western portion of the site along the river consist of steep slopes in excess of 30%. The area located along the Raritan River is not included in the analysis since it is to remain undeveloped due to floodplain and wetland buffers. See drainage area map located in the rear jacket for watershed details.

The Soil Survey of Hunterdon County (USDA, Soil Conservation Service) indicates that the site contains the following soils, with the majority of the site being Birdsboro Silt Loam (See Plate #4).

| TABLE NO. 3 Onsite Soil Data | | |
|---------------------------------|---------------------|----------------------|
| Mapping Unit | Soil Type | Hydrologic Soil Type |
| Ac | Alluvial Land | D |
| BdB | Birdsboro Silt Loam | B |
| SpF | Steep Stony Land | B |

| TABLE NO. 4 Hydrologic Data for the Pre-Development Condition Watershed | | | | |
|--|-----------------------|----|----------|--|
| Sub-Area | Drainage Area (Acres) | CN | TC (Min) | Description |
| 1 | 8.27 Acres | 61 | 14.4 | This is the entire area under study and drains in the westerly direction into the South Branch of the Raritan River. The watershed consists of Hydrologic soil type "B". |

| TABLE NO. 5 Peak Runoff Under Pre-Development Conditions | | | | | |
|---|--------------------------------------|---------|---------|---------|----------|
| Sub-Area | Storm Frequency / Peak Runoff (cfs.) | | | | |
| | 2-Year | 10-Year | 25-Year | 50-Year | 100-Year |
| 1 | 2.12 | 8.97 | 12.27 | 16.30 | 20.55 |

E. POST-DEVELOPMENT ANALYSIS

The proposed development adds approximately 4.5 ± acres of impervious area to the site. The watershed is broken down in six (6) sub areas under the post-development condition to better reflect the watershed characteristics. The following tables outline both the Hydrologic parameters and the runoff for these sub-

areas. See Plate No. 4 for watershed map.

| TABLE NO. 6 Hydrologic Data for the Post-Development Condition Watershed | | | | |
|---|--------------------------|----|-------------|---|
| Sub-Area | Drainage Area (Acres) | CN | TC (Min) | Description |
| 1a | 1.90 Acres | 85 | 10.6 | This subarea consists of the proposed restaurant area development. The runoff from this watershed is collected by a storm sewer system and drained to retention basin no.1 |
| 1b | 0.28 Acres | 61 | 6.0 | This Subarea contains retention basin no 1 along route 31. |
| 2a | 2.32 Acres | 88 | 14.5 | This Subarea consists of some offsite areas located along Moebus road and the proposed office/court along with the respective parking areas. This area drains in the easterly direction. The runoff from this Subarea is collected by a storm sewer system and drained to detention basin no.2. |
| 2b | 0.27 Acres | 61 | 6.0 | This Subarea contains some offsite drainage area and the proposed detention basin no.2. |
| 3a | 3.15 Acres | 85 | 7.5 | This Subarea consists of the proposed hotel and its supporting parking area. The runoff from this Subarea is collected by a storm sewer system and drained to detention basin no.3 |
| 3b | 0.35 Acres | 61 | 6.0 | This Subarea consists of the proposed detention basin no.3. |

| TABLE NO. 7 Peak Runoff Under Post-Development Conditions Without Stormwater Management | | | | | |
|--|--------------------------------------|---------|---------|---------|----------|
| Sub-Area | Storm Frequency / Peak Runoff (cfs.) | | | | |
| | 2-Year | 10-Year | 25-Year | 50-Year | 100-Year |
| 1a | 3.26 | 6.21 | 7.37 | 8.70 | 10.02 |
| 1b | 0.09 | 0.40 | 0.54 | 0.72 | 0.91 |
| 2a | 4.02 | 7.26 | 8.53 | 9.96 | 11.39 |
| 2b | 0.09 | 0.38 | 0.53 | 0.70 | 0.88 |
| 3a | 5.89 | 11.18 | 13.26 | 15.64 | 18.02 |
| 3b | 0.11 | 0.50 | 0.68 | 0.91 | 1.14 |

F. STORMWATER RUNOFF COLLECTION

The stormwater collection system has been designed in accordance with the requirements of the Town of Clinton Ordinances. Calculations to determine runoff to individual inlets were based on the Rational Method, $Q = (C)(I)(A)$:

Q = peak discharge (cfs.)

C = runoff coefficient

I = rainfall intensity (in/hr.)

A = drainage area (acres)

Rainfall intensity values were taken from the New Jersey State Department of Transportation "Rainfall Intensity/Duration Curves for Northern New Jersey" using the Time of Concentration as the duration. Values for Time of Concentration were derived using the "Nomograph for the Calculation of Tc" prepared by the New Jersey Highway Authority - Garden State Parkway, 1952. Where small impervious areas were encountered, a minimum time of concentration of six (6) minutes was used. The following values were used to compute weighted runoff coefficient to each inlet.

Grassed Areas C = 0.35

Impervious Areas C = 0.95

The peak flows to the inlets were kept below 5 cfs. According to Campbell Foundry Flow Charts, grate pattern No. 2618 (Bicycle Safe) can pass up to 7.8 cfs with a 4" depth of flow over the grate. Eight (8) inch curb headpieces are specified. The storm sewer collection system is designed to convey the runoff resulting from the 25-year frequency storm.

Storm sewer pipes were designed so that in all cases design velocities are greater than two feet per second (2 fps) to maintain self-cleaning. All proposed storm sewer pipes on site are reinforced concrete (RCP) pipes. Calculations were based on Manning's Equation using an "n" value of 0.013. Refer to *Appendix "C"* for storm sewer calculations.

G. STORMWATER MANAGEMENT

The proposed development increases the peak runoff from the site. To address this increase in runoff, the development plan calls for the construction of two (2) detention and one (1) retention basin onsite prior to draining to the South branch of the Raritan River. The runoff from the site will be collected via a storm

collection system and drained to the proposed detention/retention basins for both peak attenuation and water quality treatment. The following tables outline the detention/retention basin configuration and performance data.

| TABLE NO. 8 Retention Basin No. 1 Configuration Details | |
|---|------------|
| Drainage Area Treated | 2.18 Acres |
| Basin Invert | 238.00 FT |
| Top of Dam | 246.50 FT |
| Toe of Dam | 242.00 FT |
| Berm Height | 4.50 FT |
| Volume in the Basin | 54,542 CF |
| Outlet Structure Data | |
| 3" Orifice @ Invert | 240.00 FT |
| 1' wide Weir @ Elevation | 243.00 FT |
| Top Of Box | 244.00 FT |
| 40' wide Emergency Spillway @ Elevation | 244.50 FT |
| Emergency Storm Water Surface Elevation | 244.45 FT |
| Freeboard | 2.05 FT |

| TABLE NO. 9 Retention Basin No. 1 Performance Data | | | |
|--|-------------------|--------------------|--------------|
| Storm Frequency | Basin Peak Inflow | Basin Peak Outflow | Peak W.S.E.L |
| 2-Year | 3.34 | 0.23 | 241.09 |
| 10-Year | 6.52 | 0.35 | 242.34 |
| 25-Year | 7.79 | 0.39 | 242.87 |
| 50-Year | 9.25 | 0.76 | 243.22 |
| 100-Year | 10.71 | 1.50 | 243.46 |
| | | | |

| TABLE NO. 10 Detention Basin No. 2 Configuration Details | |
|--|------------|
| Drainage Area Treated | 2.59 Acres |
| Basin Invert | 229.33 FT |

| | |
|---|-----------|
| Top Of Dam | 236.00 FT |
| Toe of Dam | 230.00 FT |
| Berm Height | 6.00 FT |
| Volume in the Basin | 51,716 CF |
| Outlet Structure Data | |
| 3" Orifice @ Invert | 231.00 FT |
| 8" Wide Weir @ Elevation | 232.00 FT |
| Top of Box | 235.50 FT |
| 20' Wide Emergency Spillway @ Elevation | 236.00 FT |
| Emergency Storm Water Surface Elevation | 236.05 FT |
| Freeboard | 1.95 FT |

TABLE NO. 11
Detention Basin No. 2 Performance Data

| Storm Frequency | Basin Peak Inflow | Basin Peak Outflow | Peak W.S.E.L |
|-----------------|-------------------|--------------------|--------------|
| 2-Year | 4.09 | 0.40 | 232.12 |
| 10-Year | 7.51 | 2.53 | 232.99 |
| 25-Year | 8.86 | 3.63 | 233.29 |
| 50-Year | 10.39 | 4.95 | 233.62 |
| 100-Year | 11.93 | 6.27 | 233.92 |

TABLE NO. 12
Detention Basin No. 3 Configuration Details

| | |
|--------------------------|------------|
| Drainage Area Treated | 3.50 Acres |
| Basin Invert | 219.00 FT |
| Top Of Dam | 228.50 FT |
| Toe of Dam | 218.00 FT |
| Berm Height | 10.50 FT |
| Volume in the Basin | 51,317 CF |
| Outlet Structure Data | |
| 3" Orifice @ Invert | 217.90 FT |
| 12" Orifice @ Invert | 224.00 FT |
| 1' wide Weir @ Elevation | 225.25 FT |

| | |
|---|-----------|
| 2' wide Weir @ Elevation | 226.00 FT |
| Top Of Box | 227.00 FT |
| 90' wide Emergency Spillway @ Elevation | 227.00 FT |
| Emergency Storm Water Surface Elevation | 227.05 FT |
| Freeboard | 1.45 FT |

TABLE NO. 13
Detention Basin No. 3 Performance Data

| Storm Frequency | Basin Peak Inflow | Basin Peak Outflow | Peak W.S.E.L |
|-----------------|-------------------|--------------------|--------------|
| 2-Year | 6.00 | 0.45 | 222.57 |
| 10-Year | 11.65 | 1.15 | 224.38 |
| 25-Year | 13.90 | 2.45 | 224.75 |
| 50-Year | 16.49 | 3.80 | 225.54 |
| 100-Year | 19.08 | 5.59 | 225.66 |

TABLE NO. 14
Peak Runoff @ The Point of Study

| Frequency | Pre-Development | Post (W/O Basin) | Post (With Basin) | Peak Attenuation* |
|-----------|-----------------|------------------|-------------------|-------------------|
| 2-Year | 2.12 | 13.10 | 1.10 | 48.1% (50%) |
| 10-Year | 8.97 | 24.99 | 4.21 | 53.1% (25%) |
| 25-Year | 12.27 | 29.71 | 7.01 | 42.9% |
| 50-Year | 16.30 | 35.12 | 9.95 | 38.9% |
| 100-Year | 20.55 | 40.54 | 13.56 | 34.8% (20%) |

*Required Attenuation in ().

The proposed stormwater management system attenuates the post-development peaks from the site to less than the pre-development as required by the regulations. See table-14 for information.

H. WATER QUALITY ANALYSIS

Water quality criteria as found in NJAC 7:8 for commercial sites, required detention of 90% of the rainfall volume from 1¼" of rainfall over a 2-hour period or a 1-year, 24-hour Type III frequency rainfall for 36-

hours.

The following table outlines the retention times provided by the proposed detention/retention basins. The regulations require a commercial facility to provide a minimum of 36 hours of retention within the basins.

| Detention Basin No. | Retention Time Provided (Hours) | Comments |
|---------------------|---------------------------------|--|
| 1 | 33.53 Hours | This is less than the required 36-hours. To compensate this deficiency the detention basin is converted to a 4.5 feet deep retention pond with a permanent water surface elevation of 240.00 and a standing volume of 11,128CF of water. This increases the TSS removal capacity of the basin. |
| 2 | 37.16 Hours | This is greater than the required 36-hours. |
| 3 | 10.76 Hours | This is less than the required 36-hours. To compensate this deficiency the detention basin catch basin no. 17 is fitted with a stormceptor unit. |

I. SOIL EROSION COMPUTATIONS

On-site detention basin is constructed prior to any site disturbance trapping sediment during construction within the basin. Local best management practices such as silt fences, inlet filters tracking pads and temporary seeding are proposed to reduce erosion. Outlet protection is provided to the headwalls (see calculations in Appendix-E)

J. CONCLUSIONS

The data contained herein is in compliance with the Town, County, and State guidelines for stormwater management. It is anticipated that the proposed development will not cause any negative downstream impacts.

APPENDIX "A"
STORM SEWER COMPUTATIONS

| INLET NO. | AREA AC. | C | Δ IMP. AREA C x A | Σ IMP. AREA C x A | INLET | | PIPE | | SIZE IN. | MIN. SLOPE | ACT. SLOPE | MAX. Q CFS. | VEL. FPS |
|----------------------|-------------|------|-------------------|-------------------|----------------|-----|----------------|--------------------|----------|------------|------------|-------------|----------|
| | | | | | T _c | i | T _c | i | | | | | |
| 26 | 0.81 | 0.66 | 0.53 | 0.53 | 16 | 4.5 | 16 | 4.5 | 15" | 0.0010 | 0.0100 | 7.5 | 6.1 |
| 25 | 0.38 | 0.81 | 0.31 | 0.31 | 5 | 7.0 | 5 | 7.0 | 15" | 0.0008 | 0.0100 | 7.5 | 6.0 |
| 24 | 0.27 | 0.83 | 0.22 | 1.06 | 5 | 7.0 | 16 | 5.5 ⁽¹⁾ | 15" | 0.0052 | 0.0100 | 7.5 | 6.9 |
| | 1.46 | | | | | | | | | | | | |
| W 24B | 0.16 | 0.82 | 0.13 | 1.19 | 5 | 7.0 | 17 | 5.3 ⁽¹⁾ | 18" | 0.0025 | 0.0041 | 8.0 | 4.8 |
| W 24C | -- | -- | -- | 1.19 | -- | -- | 17 | 5.3 ⁽¹⁾ | SWALE | | | | |
| OUT 1 | 0.09 | 0.87 | 0.08 | 1.27 | 5 | 7.0 | 18 | 5.2 ⁽¹⁾ | 15" | 0.0120 | 0.0603 | 19 | 15.0 |
| TOTAL BASIN 1 | 1.71 | | | | | | | | | | | | |
| 10C | 0.31 | 0.83 | 0.26 | 0.26 | 5 | 7.0 | 5 | 7.0 | 15" | 0.0005 | 0.0100 | 7.5 | 5.6 |
| 10B | 0.92 | 0.61 | 0.56 | 0.56 | 6 | 6.6 | 6 | 6.6 | 15" | 0.0023 | 0.0100 | 7.5 | 6.6 |
| 10A | 0.06 | 0.78 | 0.05 | 0.87 | 5 | 7.0 | 6 | 8.5 ⁽¹⁾ | 15" | 0.0092 | 0.0100 | 7.5 | 6.9 |
| 10 | 0.24 | 0.87 | 0.21 | 1.08 | 5 | 7.0 | 7 | 7.0 ⁽¹⁾ | 15" | 0.0100 | 0.0225 | 11.5 | 10.1 |
| 9 | 0.16 | 0.89 | 0.14 | 1.22 | 5 | 7.0 | 8 | 7.0 ⁽¹⁾ | 15" | 0.0010 | 0.0120 | 11.5 | 10.2 |
| STM 8 | -- | -- | -- | 1.22 | -- | -- | 8 | 6.6 ⁽¹⁾ | 15" | 0.0010 | 0.0120 | 12.0 | 10.6 |
| 7 | 0.16 | 0.89 | 0.14 | 1.36 | 5 | 7.0 | 9 | 7.2 ⁽¹⁾ | 15" | 0.0165 | 0.0251 | 12.0 | 10.7 |
| 7A | 0.11 | 0.89 | 0.10 | 1.46 | 5 | 7.0 | 9 | 7.2 ⁽¹⁾ | 15" | 0.0190 | 0.0251 | 12.0 | 10.5 |
| 5 | 0.18 | 0.69 | 0.12 | 0.12 | 5 | 7.0 | 5 | 7.0 | 15" | 0.0002 | 0.0100 | 7.5 | 4.4 |
| 4 | 0.07 | 0.71 | 0.05 | 0.17 | 5 | 7.0 | 5 | 7.0 | 15" | 0.0003 | 0.0100 | 7.5 | 5.0 |
| 3 | 0.23 | 0.81 | 0.19 | 0.36 | 5 | 7.0 | 6 | 6.6 | 15" | 0.0080 | 0.0250 | 12.0 | 8.3 |
| 2 | 0.30 | 0.82 | 0.25 | 0.61 | 5 | 7.0 | 7 | 8.2 ⁽¹⁾ | 15" | 0.0042 | 0.0400 | 15.1 | 12.0 |
| 1 | 0.56 | 0.87 | 0.49 | 2.56 | 6 | 6.6 | 10 | 6.9 ⁽¹⁾ | 24" | 0.0042 | 0.0100 | 27.0 | 9.2 |
| | 3.46 | | | | | | | | | | | | |

| INLET NO. | AREA AC. | C | Δ IMP. AREA C x A | Σ IMP. AREA C x A | INLET | | | PIPE | | | SIZE IN. | MIN. SLOPE | ACT. SLOPE | MAX. Q CFS. | VEL. FPS |
|---------------|----------|------|-------------------|-------------------|----------------|-----|-------|--------------------|------|-------|----------|------------|------------|-------------|----------|
| | | | | | T _c | i | Q-CFS | T _c | i | Q-CFS | | | | | |
| HW1A | OUT 3 | -- | -- | 2.56 | -- | -- | 10 | 7.0 ⁽¹⁾ | 17.9 | SWALE | | | | | |
| OUT3 | STM 1B | 0.30 | 0.03 | 2.64 | 5 | 7.0 | 11 | 6.6 ⁽¹⁾ | 17.4 | 24" | 0.0042 | 0.0100 | 27 | 9.6 | |
| STM 1B | STM 1C | -- | -- | 2.64 | -- | -- | 11 | 6.6 ⁽¹⁾ | 17.4 | 24" | 0.0042 | 0.0100 | 27 | 9.2 | |
| STM 1C | STM 1D | -- | -- | 2.64 | -- | -- | 11 | 6.6 ⁽¹⁾ | 17.4 | 24" | 0.0042 | 0.0100 | 27 | 9.2 | |
| STM 1D | NW 1E | -- | -- | 2.64 | -- | -- | 12 | 6.4 ⁽¹⁾ | 17.4 | 30" | 0.0012 | 0.005 | 35 | 7.6 | |
| TOTAL BASIN 3 | | | | 3.71 | | | | | | | | | | | |
| 23A | 23 | 0.99 | 0.59 | 0.59 | 8 | 5.9 | 8 | 5.9 | 1.2 | 15" | 0.0003 | 0.0100 | 7.5 | 4.8 | |
| 23 | 20 | 0.11 | 0.09 | 0.68 | 5 | 7.0 | 8 | 5.9 | 4.0 | 15" | 0.0027 | 0.0542 | 16.2 | 11.0 | |
| 20A | 20 | 0.38 | 0.25 | 0.25 | 6 | 6.6 | 12 | 5.0 | 1.3 | 15" | 0.0003 | 0.0100 | 7.5 | 5.1 | |
| 20 | 19 | 0.04 | 0.04 | 1.10 | 5 | 7.0 | 12 | 5.0 | 5.5 | 15" | 0.0052 | 0.0100 | 7.5 | 6.9 | |
| 19 | 17 | 0.31 | 0.27 | 1.37 | 6 | 6.6 | 13 | 4.8 | 6.6 | 15 | 0.0075 | 0.0150 | 9.5 | 8.0 | |
| 17 | HW17A | 0.63 | 0.47 | 1.84 | 8 | 5.9 | 14 | 4.7 | 8.6 | 18" | 0.0048 | 0.0167 | 16 | 14.1 | |
| HW17A | OUT 2 | -- | -- | 1.84 | -- | -- | 14 | 4.7 | 8.6 | SWALE | | | | | |
| OUT2 | LS | 0.28 | 0.08 | 1.92 | 6 | 6.6 | 15 | 5.7 | 5 | 24" | 0.0042 | 0.0100 | 27 | 6.9 | |
| | | 2.74 | | | | | | | | | | | | | |
| OFF. BLDG. | | 0.90 | 0.14 | 0.14 | 5 | 7.0 | 5 | 7.0 | 1.0 | 8" | 0.0045 | 0.0125 | 1.6 | 4.5 | |
| TOTAL BASIN 2 | | | | 3.64 | | | | | | | | | | | |
| 27 | EX DOT | 0.31 | 0.26 | 0.26 | 5 | 7.0 | 5 | 7.0 | 1.8 | 15" | 0.0006 | 0.0100 | 7.5 | 5.3 | |

ESIGN STORM = 15 YEAR PROJECT NAME: ANSUYA
 = 0.011 PROJECT NUMBER: 020128111

APPENDIX "B"
PRE-DEVELOPMENT CONDITION COMPUTATIONS

TR-55 Worksheet 2: Runoff curve number and runoff

Project Ansuya Enterprises of Clinton By MRC Date 10/1/2004
 Location Clinton Twp, Hunterdon Co. revised

Circle Present Developed Subarea 1
 one:

1. Runoff and curve number (CN)

| Soil Name and Hydrologic Group (Appendix A) | Cover Description (cover type, treatment, and hydrologic condition; percent impervious; unconnected/connecte | CN Table 2-2 | Area | | Product of CN x area |
|--|---|---------------------|-------|-------------------------------|----------------------|
| | | | X | acres mi ² % | |
| Birdsboro "B" | wooded | 55 | 1.220 | | 67.100 |
| Birdsboro "B" | meadow | 58 | 6.330 | | 367.140 |
| Birdsboro "B" | impervious | 98 | 0.720 | | 70.560 |
| Totals = | | | 8.270 | | 504.800 |

CN (weighted) = $\frac{\text{total product}}{\text{total area}} = \frac{504.8}{8.27} = 61.040$ Use CN = 61

2. Runoff

Frequency.....yr
 Rainfall, P (24 hour).....in

| Storm # 1 | Storm # 2 | Storm # 3 | Storm # 4 | Storm # 5 | Storm # 6 |
|-----------|-----------|-----------|-----------|-----------|-----------|
| 2 | 5 | 10 | 25 | 50 | 100 |
| 3.3 | 4.3 | 5.2 | 6.0 | 6.5 | 7.5 |

Worksheet 3: Time of concentration (Tc) or travel time (Tt)

Project: Ansuya Enterprises of Clinton

By: MRC

Date: 10/6/2004

Location: Clinton Twp., Hunterdon County

Checked: _____

Date: _____

Select One: Present Developed

Select One: Tc Tt through subarea

1

NOTES: Space for as many as two segments per flow type can be used for each worksheet.

Include a map, schematic, or description of flow segments.

Sheet Flow (Applicable to Tc only)

1. Surface description (table 3-1)
2. Manning's roughness coeff., n (table 3-1)
3. Flow length, L (total L ≤ 150 ft)
4. Two-yr 24-hr rainfall, P2
5. Land Slope, s
6. $Tt = \frac{0.007 (n L)^{0.8}}{P2^{0.5} s^{0.4}}$ Compute Tt

Segment ID

| | | | | | |
|---------|---------------|------|------|---|-------|
| | AB | | | | |
| | Dense Grasses | | | | |
| | 0.24 | 0.00 | | | |
| ft | 150.00 | 0.00 | | | |
| in | 3.20 | 0.00 | | | |
| ft / ft | 0.07 | 0.00 | | | |
| hr | 0.203 | + | 0.00 | = | 0.203 |

Shallow concentrated flow

7. Surface description (paved or unpaved)
8. Flow length, L
9. Watercourse slope, s
10. Average velocity, V (figure 3-1)
11. $Tt = \frac{L}{3600 V}$ Compute Tt

Segment ID

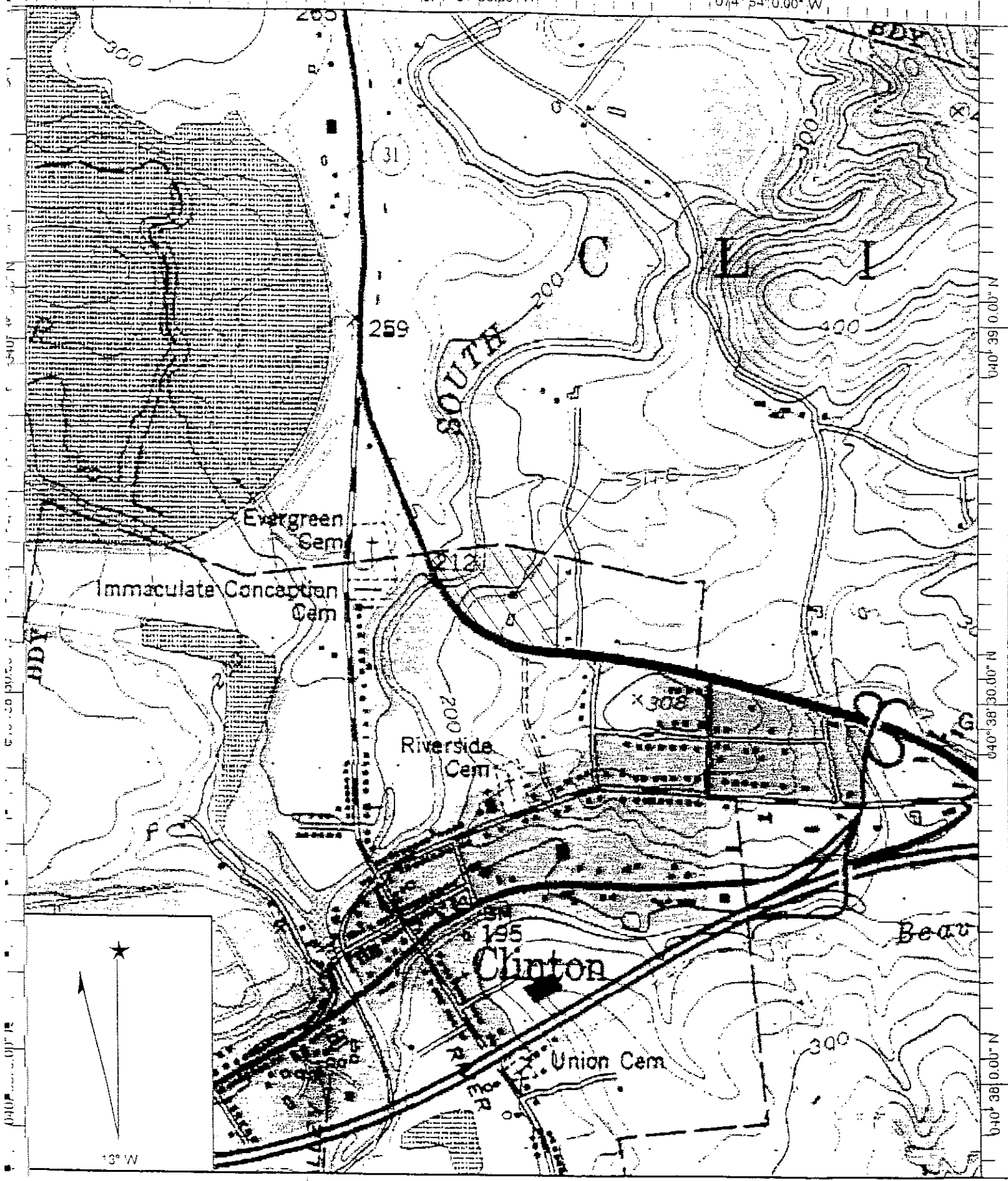
| | | | | | |
|---------|---------|---------|-------|---|-------|
| | BC | CD | | | |
| | Unpaved | Unpaved | | | |
| ft | 500.00 | 85.00 | | | |
| ft / ft | 0.06 | 0.42 | | | |
| ft / s | 4.10 | 10.50 | | | |
| hr | 0.034 | + | 0.002 | = | 0.036 |

Channel flow

12. Cross sectional flow area, a
13. Wetted perimeter, Pw
14. Hydraulic radius, r = a / Pw
15. Channel slope, s
16. Manning's roughness coeff., n
17. $V = \frac{1.49 r^{2/3} s^{1/2}}{N}$ Compute V
18. Flow length, L
19. $Tt = \frac{L}{3600 V}$ Compute Tt
20. Watershed or subarea Tc or Tt (add Tt in steps 6, 11 and 19)

Segment ID

| | | | | | |
|---------|------|------|------|---|-------|
| | | | | | |
| sf | 0.00 | 0.00 | | | |
| ft | 0.00 | 0.00 | | | |
| ft / ft | 0.00 | 0.00 | | | |
| ft / s | 0.00 | 0.00 | | | |
| hr | 0.00 | 0.00 | | | |
| ft | 0.00 | 0.00 | | | |
| hr | 0.00 | + | 0.00 | = | 0.000 |
| hr | | | | | 0.239 |
| min | | | | | 14.4 |



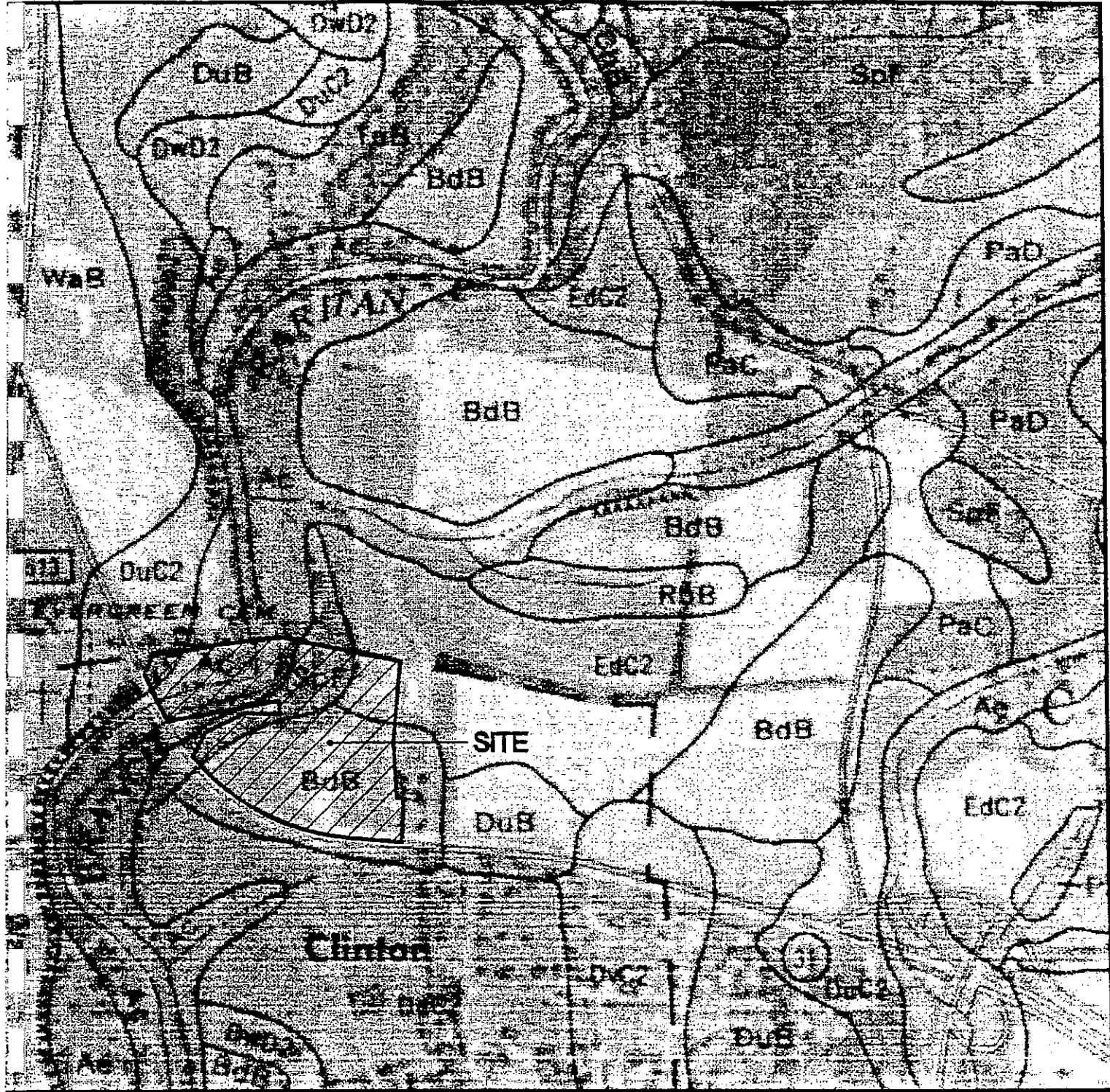
Name: HIGH BRIDGE

Date: 11/2/2001

Scale: 1 inch equals 1000 feet

Location: 040° 38' 38.4" N 074° 54' 27.9" W

Caption: ANSUYA ENTERPRISE, L.L.C



SOILS MAP

PLATE NO. 2

-NOTICE-

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| DATE | REVISIONS | ORDER NO. | SCALE | DATE | DRAWN BY | CHK'D BY | FILE NO. | FIELD BOOK |
|------|-----------|-----------|---------|---------|----------|----------|----------|------------|
| | | | 1"=600' | 11/2/01 | JB | SYI | E01284 | |

APPENDIX "C"
POST-DEVELOPMENT COMPUTATIONS

TR-55 Worksheet 2: Runoff curve number and runoff

Project Ansuya Enterprises of Clinton By MRC Date 10/1/2004
 revised

Location Clinton Twp, Hunterdon Co.

Circle Present **Developed** Subarea 1a
 one:

1. Runoff and curve number (CN)

| Soil Name and Hydrologic Group (Appendix A) | Cover Description (cover type, treatment, and hydrologic condition; percent impervious; unconnected/connecte | CN Table 2-2 | Area | | Product of CN x area |
|--|---|---------------------|-------|-------------------------------|----------------------|
| | | | X | acres mi ² % | |
| Birdsboro "B" | wooded | 55 | 0.075 | | 4.125 |
| Birdsboro "B" | open spaces | 61 | 0.594 | | 36.234 |
| Birdsboro "B" | impervious | 98 | 1.233 | | 120.834 |
| Totals = | | | 1.902 | | 161.193 |

CN (weighted) = $\frac{\text{total product}}{\text{total area}} = \frac{161.193}{1.902} = 84.749$ Use CN = 85

2. Runoff

Frequency.....yr
 Rainfall, P (24 hour).....in

| Storm # 1 | Storm # 2 | Storm # 3 | Storm # 4 | Storm # 5 | Storm # 6 |
|-----------|-----------|-----------|-----------|-----------|-----------|
| 2 | 5 | 10 | 25 | 50 | 100 |
| 3.3 | 4.3 | 5.2 | 6.0 | 6.5 | 7.5 |

Worksheet 3: Time of concentration (Tc) or travel time (Tt)

Project: Ansuya Enterprises of Clinton
 Location: Clinton Twp., Hunterdon County

By: MRC Date: 10/6/2004
 Checked: _____ Date: _____

Select One: Present Developed
 Select One: Tc Tt through subarea 1a

NOTES: Space for as many as two segments per flow type can be used for each worksheet.
 Include a map, schematic, or description of flow segments.

Sheet Flow (Applicable to Tc only)

1. Surface description (table 3-1)
2. Manning's roughness coeff., n (table 3-1)
3. Flow length, L (total L ≤ 150 ft)
4. Two-yr 24-hr rainfall, P2
5. Land Slope, s
6. $Tt = \frac{0.007 (n L)^{0.8}}{P2^{0.5} s^{0.4}}$ Compute Tt

| | | | | | |
|------------|---------------|--------|------|------|---------|
| Segment ID | AB | | | | |
| | Dense Grasses | | | | |
| | 0.24 | 0.00 | | | |
| | ft | 150.00 | 0.00 | | |
| | in | 3.20 | 0.00 | | |
| | ft / ft | 0.12 | 0.00 | | |
| | hr | 0.161 | + | 0.00 | = 0.161 |

Shallow concentrated flow

7. Surface description (paved or unpaved)
8. Flow length, L
9. Watercourse slope, s
10. Average velocity, V (figure 3-1)
11. $Tt = \frac{L}{3600 V}$ Compute Tt

| | | | | | |
|------------|---------|-------|--------|-------|---------|
| Segment ID | BC | CD | | | |
| | Unpaved | Paved | | | |
| | ft | 35.00 | 140.00 | | |
| | ft / ft | 0.05 | 0.04 | | |
| | ft / s | 3.80 | 4.00 | | |
| | hr | 0.003 | + | 0.010 | = 0.012 |

Channel flow

12. Cross sectional flow area, a
13. Wetted perimeter, Pw
14. Hydraulic radius, r = a / Pw
15. Channel slope, s
16. Manning's roughness coeff., n
17. $V = \frac{1.49 r^{2/3} s^{1/2}}{N}$ Compute V
18. Flow length, L
19. $Tt = \frac{L}{3600 V}$ Compute Tt
20. Watershed or subarea Tc or Tt (add Tt in steps 6, 11 and 19)

| | | | | | |
|------------|---------|-------|------|------|---------|
| Segment ID | DE | | | | |
| | sf | 1.23 | 0.00 | | |
| | ft | 3.93 | 0.00 | | |
| | ft / ft | 0.31 | 0.00 | | |
| | ft / s | 0.01 | 0.00 | | |
| | hr | 5.28 | 0.00 | | |
| | ft | 81.00 | 0.00 | | |
| | hr | 0.004 | + | 0.00 | = 0.004 |
| | hr | | | | 0.177 |
| | min | | | | 10.6 |

TR-55 Worksheet 2: Runoff curve number and runoff

Project Ansuya Enterprises of Clinton By MRC Date 10/1/2004

revised

Location Clinton Twp, Hunterdon Co.

Circle Present Developed Subarea 1b
one:

1. Runoff and curve number (CN)

| Soil Name and Hydrologic Group (Appendix A) | Cover Description (cover type, treatment, and hydrologic condition; percent impervious; unconnected/connecte | CN Table 2-2 | Area | | Product of CN x area |
|--|---|---------------------|-------|-------------------------------|----------------------|
| | | | X | acres mi ² % | |
| Birdsboro "B" | wooded | 55 | 0.000 | | 0.000 |
| Birdsboro "B" | open spaces | 61 | 0.280 | | 17.080 |
| Birdsboro "B" | impervious | 98 | 0.000 | | 0.000 |
| Totals = | | | 0.280 | | 17.080 |

CN (weighted) = $\frac{\text{total product}}{\text{total area}}$ = $\frac{17.08}{0.28}$ = 61.000 Use CN = 61

2. Runoff

Frequency.....yr
Rainfall, P (24 hour)in

| Storm # 1 | Storm # 2 | Storm # 3 | Storm # 4 | Storm # 5 | Storm # 6 |
|-----------|-----------|-----------|-----------|-----------|-----------|
| 2 | 5 | 10 | 25 | 50 | 100 |
| 3.3 | 4.3 | 5.2 | 6.0 | 6.5 | 7.5 |

TR-55 Worksheet 2: Runoff curve number and runoff

Project Ansuya Enterprises of Clinton By MRC Date 10/1/2004

revised

Location Clinton Twp, Hunterdon Co.

Circle Present Developed Subarea 2a
one:

1. Runoff and curve number (CN)

| Soil Name and Hydrologic Group (Appendix A) | Cover Description (cover type, treatment, and hydrologic condition; percent impervious; unconnected/connecte | CN Table 2-2 | Area | | Product of CN x area |
|--|---|---------------------|-------|-------------------------------|----------------------|
| | | | X | acres mi ² % | |
| Birdsboro "B" | wooded | 55 | 0.000 | | 0.000 |
| Birdsboro "B" | open spaces | 61 | 0.645 | | 39.345 |
| Birdsboro "B" | impervious | 98 | 1.674 | | 164.052 |
| Totals = | | | 2.319 | | 203.397 |

CN (weighted) = $\frac{\text{total product}}{\text{total area}} = \frac{203.397}{2.319} = 87.709$ Use CN = 88

2. Runoff

Frequency.....yr
Rainfall, P (24 hour)in

| Storm # 1 | Storm # 2 | Storm # 3 | Storm # 4 | Storm # 5 | Storm # 6 |
|-----------|-----------|-----------|-----------|-----------|-----------|
| 2 | 5 | 10 | 25 | 50 | 100 |
| 3.3 | 4.3 | 5.2 | 6.0 | 6.5 | 7.5 |

Worksheet 3: Time of concentration (Tc) or travel time (Tt)

Project: Ansuya Enterprises of Clinton
 Location: Clinton Twp., Hunterdon County

By: MRC Date: 10/7/2004
 Checked: _____ Date: _____

Select One: Present Developed
 Select One: Tc Tt through subarea 2a

NOTES: Space for as many as two segments per flow type can be used for each worksheet.
 Include a map, schematic, or description of flow segments.

Sheet Flow (Applicable to Tc only)

1. Surface description (table 3-1)
2. Manning's roughness coeff., n (table 3-1)
3. Flow length, L (total L ≤ 150 ft)
4. Two-yr 24-hr rainfall, P2
5. Land Slope, s
6. $Tt = \frac{0.007 (n L)^{0.8}}{P2^{0.5} s^{0.4}}$ Compute Tt

| | | | | | |
|------------|---------------|--------|------|------|---------|
| Segment ID | AB | | | | |
| | Dense Grasses | | | | |
| | 0.24 | 0.00 | | | |
| | ft | 150.00 | 0.00 | | |
| | in | 3.20 | 0.00 | | |
| | ft / ft | 0.05 | 0.00 | | |
| | hr | 0.223 | + | 0.00 | = 0.223 |

Shallow concentrated flow

7. Surface description (paved or unpaved)
8. Flow length, L
9. Watercourse slope, s
10. Average velocity, V (figure 3-1)
11. $Tt = \frac{L}{3600 V}$ Compute Tt

| | | | | | |
|------------|---------|-------|--------|-------|---------|
| Segment ID | BC | CD | | | |
| | Unpaved | Paved | | | |
| | ft | 90.00 | 160.00 | | |
| | ft / ft | 0.09 | 0.03 | | |
| | ft / s | 5.00 | 3.20 | | |
| | hr | 0.005 | + | 0.014 | = 0.019 |

Channel flow

12. Cross sectional flow area, a
13. Wetted perimeter, Pw
14. Hydraulic radius, r = a / Pw
15. Channel slope, s
16. Manning's roughness coeff., n
17. $V = \frac{1.49 r^{2/3} s^{1/2}}{N}$ Compute V
18. Flow length, L
19. $Tt = \frac{L}{3600 V}$ Compute Tt
20. Watershed or subarea Tc or Tt (add Tt in steps 6, 11 and 19)

| | | | | | |
|------------|---------|------|------|------|---------|
| Segment ID | | | | | |
| | sf | 0.00 | 0.00 | | |
| | ft | 0.00 | 0.00 | | |
| | ft / ft | 0.00 | 0.00 | | |
| | ft / s | 0.00 | 0.00 | | |
| | hr | 0.00 | 0.00 | | |
| | ft | 0.00 | 0.00 | | |
| | hr | 0.00 | + | 0.00 | = 0.000 |
| | hr | | | | 0.242 |
| | min | | | | 14.5 |

TR-55 Worksheet 2: Runoff curve number and runoff

Project Ansuya Enterprises of Clinton By MRC Date 10/1/2004

revised

Location Clinton Twp, Hunterdon Co.

Circle Present **Developed** Subarea 2b
one:

1. Runoff and curve number (CN)

| Soil Name and Hydrologic Group (Appendix A) | Cover Description (cover type, treatment, and hydrologic condition; percent impervious; unconnected/connecte | CN Table 2-2 | Area | | Product of CN x area |
|--|---|---------------------|-------|-------------------------------|----------------------|
| | | | X | acres mi ² % | |
| Birdsboro "B" | wooded | 55 | 0.000 | | 0.000 |
| Birdsboro "B" | open spaces | 61 | 0.265 | | 16.165 |
| Birdsboro "B" | impervious | 98 | 0.000 | | 0.000 |
| Totals = | | | 0.265 | | 16.165 |

CN (weighted) = $\frac{\text{total product}}{\text{total area}} = \frac{16.165}{0.265} = 61.000$ Use CN = 61

2. Runoff

Frequency.....yr
Rainfall, P (24 hour)in

| Storm # 1 | Storm # 2 | Storm # 3 | Storm # 4 | Storm # 5 | Storm # 6 |
|-----------|-----------|-----------|-----------|-----------|-----------|
| 2 | 5 | 10 | 25 | 50 | 100 |
| 3.3 | 4.3 | 5.2 | 6.0 | 6.5 | 7.5 |

TR-55 Worksheet 2: Runoff curve number and runoff

Project Ansuya Enterprises of Clinton By MRC Date 10/1/2004
 Location Clinton Twp, Hunterdon Co. revised

Circle Present Developed Subarea 3a
 one:

1. Runoff and curve number (CN)

| Soil Name and Hydrologic Group (Appendix A) | Cover Description (cover type, treatment, and hydrologic condition; percent impervious; unconnected/connecte | CN Table 2-2 | Area | | Product of CN x area |
|--|---|---------------------|-------|-------------------------------|----------------------|
| | | | X | acres mi ² % | |
| Birdsboro "B" | wooded | 55 | 0.000 | | 0.000 |
| Birdsboro "B" | open spaces | 61 | 1.118 | | 68.198 |
| Birdsboro "B" | impervious | 98 | 2.030 | | 198.940 |
| Totals = | | | 3.148 | | 267.138 |

CN (weighted) = $\frac{\text{total product}}{\text{total area}} = \frac{267.138}{3.148} = 84.860$ Use CN = 85

2. Runoff

Frequency.....yr
 Rainfall, P (24 hour).....in

| Storm # 1 | Storm # 2 | Storm # 3 | Storm # 4 | Storm # 5 | Storm # 6 |
|-----------|-----------|-----------|-----------|-----------|-----------|
| 2 | 5 | 10 | 25 | 50 | 100 |
| 3.3 | 4.3 | 5.2 | 6.0 | 6.5 | 7.5 |

Worksheet 3: Time of concentration (Tc) or travel time (Tt)

Project: Ansuya Enterprises of Clinton

By: MRC

Date: 10/6/2004

Location: Clinton Twp., Hunterdon County

Checked: _____

Date: _____

Select One: Present Developed

Select One: Tc Tt through subarea 3a

NOTES: Space for as many as two segments per flow type can be used for each worksheet.

Include a map, schematic, or description of flow segments.

Sheet Flow (Applicable to Tc only)

1. Surface description (table 3-1)
2. Manning's roughness coeff., n (table 3-1)
3. Flow length, L (total L ≤ 150 ft)
4. Two-yr 24-hr rainfall, P2
5. Land Slope, s
6. $Tt = \frac{0.007 (n L)^{0.8}}{P2^{0.5} s^{0.4}}$ Compute Tt

Segment ID

| | | |
|---------|---------------|-------|
| | AB | |
| | Dense Grasses | |
| | 0.24 | 0.00 |
| ft | 60.00 | 0.00 |
| in | 3.20 | 0.00 |
| ft / ft | 0.06 | 0.00 |
| hr | 0.103 | 0.00 |
| | + | = |
| | 0.103 | 0.103 |

Shallow concentrated flow

7. Surface description (paved or unpaved)
8. Flow length, L
9. Watercourse slope, s
10. Average velocity, V (figure 3-1)
11. $Tt = \frac{L}{3600 V}$ Compute Tt

Segment ID

| | | |
|---------|---------|-------|
| | Unpaved | Paved |
| | 0.00 | 0.00 |
| ft | 0.00 | 0.00 |
| ft / ft | 0.00 | 0.00 |
| ft / s | 0.00 | 0.00 |
| hr | 0.00 | 0.00 |
| | + | = |
| | 0.00 | 0.000 |

Channel flow

12. Cross sectional flow area, a
13. Wetted perimeter, Pw
14. Hydraulic radius, r = a / Pw
15. Channel slope, s
16. Manning's roughness coeff., n
17. $V = \frac{1.49 r^{2/3} s^{1/2}}{N}$ Compute V
18. Flow length, L
19. $Tt = \frac{L}{3600 V}$ Compute Tt
20. Watershed or subarea Tc or Tt (add Tt in steps 6, 11 and 19)

Segment ID

| | | |
|---------|--------|--------|
| | BC | CD |
| sf | 1.50 | 1.23 |
| ft | 3.50 | 3.93 |
| ft / ft | 0.43 | 0.31 |
| ft / s | 0.03 | 0.02 |
| hr | 12.42 | 7.66 |
| ft | 200.00 | 463.00 |
| hr | 0.004 | 0.017 |
| | + | = |
| | 0.021 | 0.125 |
| hr | | 7.5 |
| min | | 7.5 |

TR-55 Worksheet 2: Runoff curve number and runoff

Project Ansuya Enterprises of Clinton By MRC Date revised 10/1/2004

Location Clinton Twp, Hunterdon Co.

Circle Present Developed Subarea 3b
one:

1. Runoff and curve number (CN)

| Soil Name and Hydrologic Group (Appendix A) | Cover Description (cover type, treatment, and hydrologic condition; percent impervious; unconnected/connecte | CN Table 2-2 | Area | | Product of CN x area |
|--|---|---------------------|-------|-------------------------------|----------------------|
| | | | X | acres mi ² % | |
| Birdsboro "B" | wooded | 55 | 0.000 | | 0.000 |
| Birdsboro "B" | open spaces | 61 | 0.353 | | 21.533 |
| Birdsboro "B" | impervious | 98 | 0.000 | | 0.000 |
| Totals = | | | 0.353 | | 21.533 |

CN (weighted) = $\frac{\text{total product}}{\text{total area}} = \frac{21.533}{0.353} = 61.000$ Use CN = 61

2. Runoff

| | Storm # 1 | Storm # 2 | Storm # 3 | Storm # 4 | Storm # 5 | Storm # 6 |
|------------------------------|-----------|-----------|-----------|-----------|-----------|-----------|
| Frequency.....yr | 2 | 5 | 10 | 25 | 50 | 100 |
| Rainfall, P (24 hour).....in | 3.3 | 4.3 | 5.2 | 6.0 | 6.5 | 7.5 |

Hydrograph Summary Report

| Hyd. No. | Hydrograph type (origin) | Peak flow (cfs) | Time interval (min) | Time to peak (min) | Volume (cuft) | Inflow hyd(s) | Maximum elevation (ft) | Maximum storage (cuft) | Hydrograph description |
|----------|--------------------------|-----------------|---------------------|--------------------|---------------|---------------|------------------------|------------------------|------------------------|
| 1 | SCS Runoff | 2.12 | 2 | 738 | 12,995 | --- | --- | ---- | Predevelopment |
| 2 | SCS Runoff | 3.26 | 2 | 728 | 12,501 | --- | --- | ---- | Post Subarea 1a |
| 3 | SCS Runoff | 0.09 | 2 | 726 | 423 | --- | --- | ---- | Post Subarea 1b |
| 4 | SCS Runoff | 4.02 | 2 | 730 | 16,397 | --- | --- | ---- | Post Subarea 2a |
| 5 | SCS Runoff | 0.09 | 2 | 726 | 408 | --- | --- | ---- | Post Subarea 2b |
| 6 | SCS Runoff | 5.89 | 2 | 726 | 20,098 | --- | --- | ---- | Post Subarea 3a |
| 7 | SCS Runoff | 0.11 | 2 | 726 | 529 | --- | --- | ---- | Post Subarea 3b |
| 8 | Combine | 3.34 | 2 | 728 | 12,924 | 2, 3, | --- | ---- | Basin 1 In |
| 9 | Combine | 4.09 | 2 | 730 | 16,805 | 4, 5, | --- | ---- | Basin 2 In |
| 10 | Combine | 6.00 | 2 | 726 | 20,626 | 6, 7, | --- | ---- | Basin 3 In |
| 11 | Reservoir | 0.23 | 2 | 880 | 12,862 | 8 | 241.09 | 18,429 | Basin 1 Out |
| 12 | Reservoir | 0.40 | 2 | 822 | 13,778 | 9 | 232.12 | 9,694 | Basin 2 Out |
| 13 | Reservoir | 0.45 | 2 | 838 | 20,626 | 10 | 222.57 | 9,939 | Basin 3 Out |
| 14 | Combine | 1.10 | 2 | 812 | 47,272 | 11, 12, 13 | --- | ---- | |

Proj. file: ansuya.basin.9-30-04.gpw Return Period: 2 yr

Run date: 10-08-2004

Hydrograph Report

Hyd. No. 1

Predevelopment

| | | | |
|-----------------|--------------|--------------------|------------|
| Hydrograph type | = SCS Runoff | Peak discharge | = 2.12 cfs |
| Storm frequency | = 2 yrs | Time interval | = 2 min |
| Drainage area | = 8.27 ac | Curve number | = 61 |
| Basin Slope | = 0.0 % | Hydraulic length | = 0 ft |
| Tc method | = USER | Time of conc. (Tc) | = 14.4 min |
| Total precip. | = 3.20 in | Distribution | = Type III |
| Storm duration | = 24 hrs | Shape factor | = 484 |

Hydrograph Volume = 12,995 cuft

Hydrograph Discharge Table

| Time (min) | Outflow (cfs) | Time (min) | Outflow (cfs) | Time (min) | Outflow (cfs) | Time (min) | Outflow (cfs) |
|------------|---------------|------------|---------------|------------|---------------|------------|---------------|
| 720 | 0.18 | 856 | 0.39 | 992 | 0.23 | 1128 | 0.15 |
| 724 | 0.69 | 860 | 0.39 | 996 | 0.22 | 1132 | 0.15 |
| 728 | 1.39 | 864 | 0.38 | 1000 | 0.22 | 1136 | 0.15 |
| 732 | 1.92 | 868 | 0.38 | 1004 | 0.22 | 1140 | 0.15 |
| 736 | 2.11 | 872 | 0.38 | 1008 | 0.22 | 1144 | 0.15 |
| 740 | 2.09 | 876 | 0.37 | 1012 | 0.21 | 1148 | 0.14 |
| 744 | 1.91 | 880 | 0.37 | 1016 | 0.21 | 1152 | 0.14 |
| 748 | 1.67 | 884 | 0.36 | 1020 | 0.21 | 1156 | 0.14 |
| 752 | 1.44 | 888 | 0.36 | 1024 | 0.20 | 1160 | 0.14 |
| 756 | 1.19 | 892 | 0.35 | 1028 | 0.20 | 1164 | 0.14 |
| 760 | 0.97 | 896 | 0.35 | 1032 | 0.20 | 1168 | 0.14 |
| 764 | 0.82 | 900 | 0.34 | 1036 | 0.20 | 1172 | 0.14 |
| 768 | 0.74 | 904 | 0.34 | 1040 | 0.19 | 1176 | 0.14 |
| 772 | 0.69 | 908 | 0.33 | 1044 | 0.19 | 1180 | 0.14 |
| 776 | 0.65 | 912 | 0.33 | 1048 | 0.19 | 1184 | 0.14 |
| 780 | 0.62 | 916 | 0.32 | 1052 | 0.18 | 1188 | 0.14 |
| 784 | 0.59 | 920 | 0.32 | 1056 | 0.18 | 1192 | 0.14 |
| 788 | 0.56 | 924 | 0.31 | 1060 | 0.18 | 1196 | 0.13 |
| 792 | 0.54 | 928 | 0.30 | 1064 | 0.18 | 1200 | 0.13 |
| 796 | 0.52 | 932 | 0.30 | 1068 | 0.17 | 1204 | 0.13 |
| 800 | 0.51 | 936 | 0.29 | 1072 | 0.17 | 1208 | 0.13 |
| 804 | 0.50 | 940 | 0.29 | 1076 | 0.17 | 1212 | 0.13 |
| 808 | 0.50 | 944 | 0.28 | 1080 | 0.16 | 1216 | 0.13 |
| 812 | 0.49 | 948 | 0.27 | 1084 | 0.16 | 1220 | 0.13 |
| 816 | 0.48 | 952 | 0.27 | 1088 | 0.16 | 1224 | 0.13 |
| 820 | 0.47 | 956 | 0.26 | 1092 | 0.16 | 1228 | 0.13 |
| 824 | 0.46 | 960 | 0.26 | 1096 | 0.16 | 1232 | 0.13 |
| 828 | 0.45 | 964 | 0.25 | 1100 | 0.15 | 1236 | 0.13 |
| 832 | 0.45 | 968 | 0.24 | 1104 | 0.15 | 1240 | 0.13 |
| 836 | 0.44 | 972 | 0.24 | 1108 | 0.15 | 1244 | 0.12 |
| 840 | 0.43 | 976 | 0.24 | 1112 | 0.15 | 1248 | 0.12 |
| 844 | 0.42 | 980 | 0.23 | 1116 | 0.15 | 1252 | 0.12 |
| 848 | 0.41 | 984 | 0.23 | 1120 | 0.15 | 1256 | 0.12 |
| 852 | 0.40 | 988 | 0.23 | 1124 | 0.15 | 1260 | 0.12 |

Continues on next page...

Hydrograph Discharge Table**Time -- Outflow
(min cfs)**

| | |
|------|------|
| 1264 | 0.12 |
| 1268 | 0.12 |
| 1272 | 0.12 |
| 1276 | 0.12 |
| 1280 | 0.12 |
| 1284 | 0.12 |
| 1288 | 0.11 |
| 1292 | 0.11 |
| 1296 | 0.11 |
| 1300 | 0.11 |
| 1304 | 0.11 |
| 1308 | 0.11 |
| 1312 | 0.11 |
| 1316 | 0.11 |
| 1320 | 0.11 |
| 1324 | 0.12 |
| 1328 | 0.14 |
| 1332 | 0.14 |
| 1336 | 0.13 |
| 1340 | 0.12 |
| 1344 | 0.11 |
| 1348 | 0.11 |
| 1352 | 0.11 |
| 1356 | 0.11 |
| 1360 | 0.11 |

...End

Hydrograph Report

Hyd. No. 2

Post Subarea 1a

| | | | |
|-----------------|--------------|--------------------|------------|
| Hydrograph type | = SCS Runoff | Peak discharge | = 3.26 cfs |
| Storm frequency | = 2 yrs | Time interval | = 2 min |
| Drainage area | = 1.90 ac | Curve number | = 85 |
| Basin Slope | = 0.0 % | Hydraulic length | = 0 ft |
| Tc method | = USER | Time of conc. (Tc) | = 10.6 min |
| Total precip. | = 3.20 in | Distribution | = Type III |
| Storm duration | = 24 hrs | Shape factor | = 484 |

Hydrograph Volume = 12,501 cuft

Hydrograph Discharge Table

| Time -- Outflow (min cfs) | Time -- Outflow (min cfs) | Time -- Outflow (min cfs) |
|------------------------------|------------------------------|------------------------------|
| 666 0.16 | 802 0.34 | 938 0.17 |
| 670 0.18 | 806 0.33 | |
| 674 0.19 | 810 0.32 | |
| 678 0.21 | 814 0.32 | ...End |
| 682 0.23 | 818 0.31 | |
| 686 0.25 | 822 0.30 | |
| 690 0.28 | 826 0.29 | |
| 694 0.31 | 830 0.29 | |
| 698 0.38 | 834 0.28 | |
| 702 0.51 | 838 0.27 | |
| 706 0.68 | 842 0.26 | |
| 710 0.89 | 846 0.26 | |
| 714 1.13 | 850 0.25 | |
| 718 1.49 | 854 0.25 | |
| 722 2.25 | 858 0.24 | |
| 726 3.08 | 862 0.24 | |
| 730 3.23 | 866 0.23 | |
| 734 2.82 | 870 0.23 | |
| 738 2.26 | 874 0.23 | |
| 742 1.77 | 878 0.22 | |
| 746 1.45 | 882 0.22 | |
| 750 1.19 | 886 0.22 | |
| 754 0.94 | 890 0.21 | |
| 758 0.73 | 894 0.21 | |
| 762 0.61 | 898 0.20 | |
| 766 0.54 | 902 0.20 | |
| 770 0.50 | 906 0.20 | |
| 774 0.47 | 910 0.19 | |
| 778 0.44 | 914 0.19 | |
| 782 0.41 | 918 0.19 | |
| 786 0.39 | 922 0.18 | |
| 790 0.37 | 926 0.18 | |
| 794 0.36 | 930 0.17 | |
| 798 0.35 | 934 0.17 | |

Hydrograph Report

Hyd. No. 3

Post Subarea 1b

| | | | | | |
|-----------------|---|------------|--------------------|---|----------|
| Hydrograph type | = | SCS Runoff | Peak discharge | = | 0.09 cfs |
| Storm frequency | = | 2 yrs | Time interval | = | 2 min |
| Drainage area | = | 0.28 ac | Curve number | = | 61 |
| Basin Slope | = | 0.0 % | Hydraulic length | = | 0 ft |
| Tc method | = | USER | Time of conc. (Tc) | = | 6 min |
| Total precip. | = | 3.20 in | Distribution | = | Type III |
| Storm duration | = | 24 hrs | Shape factor | = | 484 |

Hydrograph Volume = 423 cuft

Hydrograph Discharge Table

| Time (min) | Outflow (cfs) | Time (min) | Outflow (cfs) | Time (min) | Outflow (cfs) | Time (min) | Outflow (cfs) |
|------------|---------------|------------|---------------|------------|---------------|------------|---------------|
| 718 | 0.01 | 854 | 0.01 | 990 | 0.01 | 1126 | 0.00 |
| 722 | 0.06 | 858 | 0.01 | 994 | 0.01 | 1130 | 0.00 |
| 726 | 0.09 << | 862 | 0.01 | 998 | 0.01 | 1134 | 0.00 |
| 730 | 0.07 | 866 | 0.01 | 1002 | 0.01 | 1138 | 0.00 |
| 734 | 0.06 | 870 | 0.01 | 1006 | 0.01 | 1142 | 0.00 |
| 738 | 0.06 | 874 | 0.01 | 1010 | 0.01 | 1146 | 0.00 |
| 742 | 0.05 | 878 | 0.01 | 1014 | 0.01 | 1150 | 0.00 |
| 746 | 0.05 | 882 | 0.01 | 1018 | 0.01 | 1154 | 0.00 |
| 750 | 0.03 | 886 | 0.01 | 1022 | 0.01 | 1158 | 0.00 |
| 754 | 0.03 | 890 | 0.01 | 1026 | 0.01 | 1162 | 0.00 |
| 758 | 0.02 | 894 | 0.01 | 1030 | 0.01 | 1166 | 0.00 |
| 762 | 0.02 | 898 | 0.01 | 1034 | 0.01 | 1170 | 0.00 |
| 766 | 0.02 | 902 | 0.01 | 1038 | 0.01 | | |
| 770 | 0.02 | 906 | 0.01 | 1042 | 0.01 | | |
| 774 | 0.02 | 910 | 0.01 | 1046 | 0.01 | ...End | |
| 778 | 0.02 | 914 | 0.01 | 1050 | 0.01 | | |
| 782 | 0.02 | 918 | 0.01 | 1054 | 0.01 | | |
| 786 | 0.02 | 922 | 0.01 | 1058 | 0.01 | | |
| 790 | 0.02 | 926 | 0.01 | 1062 | 0.01 | | |
| 794 | 0.02 | 930 | 0.01 | 1066 | 0.01 | | |
| 798 | 0.02 | 934 | 0.01 | 1070 | 0.01 | | |
| 802 | 0.02 | 938 | 0.01 | 1074 | 0.01 | | |
| 806 | 0.02 | 942 | 0.01 | 1078 | 0.01 | | |
| 810 | 0.02 | 946 | 0.01 | 1082 | 0.01 | | |
| 814 | 0.02 | 950 | 0.01 | 1086 | 0.01 | | |
| 818 | 0.02 | 954 | 0.01 | 1090 | 0.01 | | |
| 822 | 0.01 | 958 | 0.01 | 1094 | 0.01 | | |
| 826 | 0.01 | 962 | 0.01 | 1098 | 0.00 | | |
| 830 | 0.01 | 966 | 0.01 | 1102 | 0.00 | | |
| 834 | 0.01 | 970 | 0.01 | 1106 | 0.00 | | |
| 838 | 0.01 | 974 | 0.01 | 1110 | 0.00 | | |
| 842 | 0.01 | 978 | 0.01 | 1114 | 0.00 | | |
| 846 | 0.01 | 982 | 0.01 | 1118 | 0.00 | | |
| 850 | 0.01 | 986 | 0.01 | 1122 | 0.00 | | |

Hydrograph Report

Hyd. No. 4

Post Subarea 2a

| | | | |
|-----------------|--------------|--------------------|------------|
| Hydrograph type | = SCS Runoff | Peak discharge | = 4.02 cfs |
| Storm frequency | = 2 yrs | Time interval | = 2 min |
| Drainage area | = 2.32 ac | Curve number | = 88 |
| Basin Slope | = 0.0 % | Hydraulic length | = 0 ft |
| Tc method | = USER | Time of conc. (Tc) | = 14.5 min |
| Total precip. | = 3.20 in | Distribution | = Type III |
| Storm duration | = 24 hrs | Shape factor | = 484 |

Hydrograph Volume = 16,397 cuft

Hydrograph Discharge Table

| Time (min) | Outflow (cfs) | Time (min) | Outflow (cfs) | Time (min) | Outflow (cfs) |
|------------|---------------|------------|---------------|------------|---------------|
| 650 | 0.21 | 786 | 0.50 | 922 | 0.23 |
| 654 | 0.21 | 790 | 0.47 | 926 | 0.22 |
| 658 | 0.22 | 794 | 0.45 | 930 | 0.22 |
| 662 | 0.23 | 798 | 0.44 | 934 | 0.21 |
| 666 | 0.25 | 802 | 0.43 | 938 | 0.21 |
| 670 | 0.26 | 806 | 0.42 | 942 | 0.20 |
| 674 | 0.28 | 810 | 0.41 | | |
| 678 | 0.30 | 814 | 0.40 | | |
| 682 | 0.33 | 818 | 0.39 | ...End | |
| 686 | 0.36 | 822 | 0.38 | | |
| 690 | 0.39 | 826 | 0.37 | | |
| 694 | 0.43 | 830 | 0.36 | | |
| 698 | 0.51 | 834 | 0.35 | | |
| 702 | 0.65 | 838 | 0.34 | | |
| 706 | 0.85 | 842 | 0.33 | | |
| 710 | 1.11 | 846 | 0.32 | | |
| 714 | 1.41 | 850 | 0.31 | | |
| 718 | 1.82 | 854 | 0.31 | | |
| 722 | 2.59 | 858 | 0.30 | | |
| 726 | 3.52 | 862 | 0.30 | | |
| 730 | 4.02 << | 866 | 0.29 | | |
| 734 | 3.80 | 870 | 0.29 | | |
| 738 | 3.27 | 874 | 0.28 | | |
| 742 | 2.63 | 878 | 0.28 | | |
| 746 | 2.06 | 882 | 0.27 | | |
| 750 | 1.67 | 886 | 0.27 | | |
| 754 | 1.34 | 890 | 0.26 | | |
| 758 | 1.06 | 894 | 0.26 | | |
| 762 | 0.85 | 898 | 0.25 | | |
| 766 | 0.72 | 902 | 0.25 | | |
| 770 | 0.65 | 906 | 0.24 | | |
| 774 | 0.61 | 910 | 0.24 | | |
| 778 | 0.57 | 914 | 0.24 | | |
| 782 | 0.53 | 918 | 0.23 | | |

Hydrograph Report

Hyd. No. 5

Post Subarea 2b

| | | | |
|-----------------|--------------|--------------------|------------|
| Hydrograph type | = SCS Runoff | Peak discharge | = 0.09 cfs |
| Storm frequency | = 2 yrs | Time interval | = 2 min |
| Drainage area | = 0.27 ac | Curve number | = 61 |
| Basin Slope | = 0.0 % | Hydraulic length | = 0 ft |
| Tc method | = USER | Time of conc. (Tc) | = 6 min |
| Total precip. | = 3.20 in | Distribution | = Type III |
| Storm duration | = 24 hrs | Shape factor | = 484 |

Hydrograph Volume = 408 cuft

Hydrograph Discharge Table

| Time (min) | Outflow (cfs) | Time (min) | Outflow (cfs) | Time (min) | Outflow (cfs) | Time (min) | Outflow (cfs) |
|------------|---------------|------------|---------------|------------|---------------|------------|---------------|
| 718 | 0.01 | 854 | 0.01 | 990 | 0.01 | 1126 | 0.00 |
| 722 | 0.06 | 858 | 0.01 | 994 | 0.01 | 1130 | 0.00 |
| 726 | 0.09 << | 862 | 0.01 | 998 | 0.01 | 1134 | 0.00 |
| 730 | 0.07 | 866 | 0.01 | 1002 | 0.01 | 1138 | 0.00 |
| 734 | 0.06 | 870 | 0.01 | 1006 | 0.01 | 1142 | 0.00 |
| 738 | 0.06 | 874 | 0.01 | 1010 | 0.01 | 1146 | 0.00 |
| 742 | 0.05 | 878 | 0.01 | 1014 | 0.01 | 1150 | 0.00 |
| 746 | 0.04 | 882 | 0.01 | 1018 | 0.01 | 1154 | 0.00 |
| 750 | 0.03 | 886 | 0.01 | 1022 | 0.01 | 1158 | 0.00 |
| 754 | 0.03 | 890 | 0.01 | 1026 | 0.01 | 1162 | 0.00 |
| 758 | 0.02 | 894 | 0.01 | 1030 | 0.01 | 1166 | 0.00 |
| 762 | 0.02 | 898 | 0.01 | 1034 | 0.01 | 1170 | 0.00 |
| 766 | 0.02 | 902 | 0.01 | 1038 | 0.01 | | |
| 770 | 0.02 | 906 | 0.01 | 1042 | 0.01 | | |
| 774 | 0.02 | 910 | 0.01 | 1046 | 0.01 | ...End | |
| 778 | 0.02 | 914 | 0.01 | 1050 | 0.01 | | |
| 782 | 0.02 | 918 | 0.01 | 1054 | 0.01 | | |
| 786 | 0.02 | 922 | 0.01 | 1058 | 0.01 | | |
| 790 | 0.02 | 926 | 0.01 | 1062 | 0.01 | | |
| 794 | 0.02 | 930 | 0.01 | 1066 | 0.01 | | |
| 798 | 0.02 | 934 | 0.01 | 1070 | 0.01 | | |
| 802 | 0.02 | 938 | 0.01 | 1074 | 0.01 | | |
| 806 | 0.02 | 942 | 0.01 | 1078 | 0.01 | | |
| 810 | 0.02 | 946 | 0.01 | 1082 | 0.00 | | |
| 814 | 0.01 | 950 | 0.01 | 1086 | 0.00 | | |
| 818 | 0.01 | 954 | 0.01 | 1090 | 0.00 | | |
| 822 | 0.01 | 958 | 0.01 | 1094 | 0.00 | | |
| 826 | 0.01 | 962 | 0.01 | 1098 | 0.00 | | |
| 830 | 0.01 | 966 | 0.01 | 1102 | 0.00 | | |
| 834 | 0.01 | 970 | 0.01 | 1106 | 0.00 | | |
| 838 | 0.01 | 974 | 0.01 | 1110 | 0.00 | | |
| 842 | 0.01 | 978 | 0.01 | 1114 | 0.00 | | |
| 846 | 0.01 | 982 | 0.01 | 1118 | 0.00 | | |
| 850 | 0.01 | 986 | 0.01 | 1122 | 0.00 | | |

Hydrograph Report

Hyd. No. 6

Post Subarea 3a

Hydrograph type = SCS Runoff
Storm frequency = 2 yrs
Drainage area = 3.15 ac
Basin Slope = 0.0 %
Tc method = USER
Total precip. = 3.20 in
Storm duration = 24 hrs

Peak discharge = 5.89 cfs
Time interval = 2 min
Curve number = 85
Hydraulic length = 0 ft
Time of conc. (Tc) = 7.5 min
Distribution = Type III
Shape factor = 484

Hydrograph Volume = 20,098 cuft

Hydrograph Discharge Table

| Time -- Outflow (min cfs) | Time -- Outflow (min cfs) |
|------------------------------|------------------------------|
| 670 0.30 | 806 0.53 |
| 674 0.33 | 810 0.51 |
| 678 0.36 | 814 0.50 |
| 682 0.40 | 818 0.49 |
| 686 0.43 | 822 0.48 |
| 690 0.47 | 826 0.46 |
| 694 0.54 | 830 0.45 |
| 698 0.70 | 834 0.44 |
| 702 0.97 | 838 0.43 |
| 706 1.30 | 842 0.42 |
| 710 1.67 | 846 0.40 |
| 714 2.09 | 850 0.40 |
| 718 2.82 | 854 0.39 |
| 722 4.59 | 858 0.38 |
| 726 5.89 << | 862 0.38 |
| 730 5.14 | 866 0.37 |
| 734 3.77 | 870 0.37 |
| 738 2.92 | 874 0.36 |
| 742 2.48 | 878 0.35 |
| 746 2.07 | 882 0.35 |
| 750 1.63 | 886 0.34 |
| 754 1.23 | 890 0.34 |
| 758 0.98 | 894 0.33 |
| 762 0.87 | 898 0.32 |
| 766 0.82 | 902 0.32 |
| 770 0.77 | 906 0.31 |
| 774 0.73 | 910 0.31 |
| 778 0.68 | 914 0.30 |
| 782 0.64 | |
| 786 0.60 | |
| 790 0.57 | ...End |
| 794 0.56 | |
| 798 0.55 | |
| 802 0.54 | |

Hydrograph Report

Hyd. No. 7

Post Subarea 3b

Hydrograph type = SCS Runoff
Storm frequency = 2 yrs
Drainage area = 0.35 ac
Basin Slope = 0.0 %
Tc method = USER
Total precip. = 3.20 in
Storm duration = 24 hrs

Peak discharge = 0.11 cfs
Time interval = 2 min
Curve number = 61
Hydraulic length = 0 ft
Time of conc. (Tc) = 6 min
Distribution = Type III
Shape factor = 484

Hydrograph Volume = 529 cuft

Hydrograph Discharge Table

| Time (min) | Outflow (cfs) | Time (min) | Outflow (cfs) | Time (min) | Outflow (cfs) | Time (min) | Outflow (cfs) |
|------------|---------------|------------|---------------|------------|---------------|------------|---------------|
| 718 | 0.02 | 854 | 0.02 | 990 | 0.01 | 1126 | 0.01 |
| 722 | 0.07 | 858 | 0.02 | 994 | 0.01 | 1130 | 0.01 |
| 726 | 0.11 << | 862 | 0.02 | 998 | 0.01 | 1134 | 0.01 |
| 730 | 0.09 | 866 | 0.02 | 1002 | 0.01 | 1138 | 0.01 |
| 734 | 0.08 | 870 | 0.02 | 1006 | 0.01 | 1142 | 0.01 |
| 738 | 0.07 | 874 | 0.01 | 1010 | 0.01 | 1146 | 0.01 |
| 742 | 0.07 | 878 | 0.01 | 1014 | 0.01 | 1150 | 0.01 |
| 746 | 0.06 | 882 | 0.01 | 1018 | 0.01 | 1154 | 0.01 |
| 750 | 0.04 | 886 | 0.01 | 1022 | 0.01 | 1158 | 0.01 |
| 754 | 0.03 | 890 | 0.01 | 1026 | 0.01 | 1162 | 0.01 |
| 758 | 0.03 | 894 | 0.01 | 1030 | 0.01 | 1166 | 0.01 |
| 762 | 0.03 | 898 | 0.01 | 1034 | 0.01 | 1170 | 0.01 |
| 766 | 0.03 | 902 | 0.01 | 1038 | 0.01 | | |
| 770 | 0.03 | 906 | 0.01 | 1042 | 0.01 | | |
| 774 | 0.02 | 910 | 0.01 | 1046 | 0.01 | ...End | |
| 778 | 0.02 | 914 | 0.01 | 1050 | 0.01 | | |
| 782 | 0.02 | 918 | 0.01 | 1054 | 0.01 | | |
| 786 | 0.02 | 922 | 0.01 | 1058 | 0.01 | | |
| 790 | 0.02 | 926 | 0.01 | 1062 | 0.01 | | |
| 794 | 0.02 | 930 | 0.01 | 1066 | 0.01 | | |
| 798 | 0.02 | 934 | 0.01 | 1070 | 0.01 | | |
| 802 | 0.02 | 938 | 0.01 | 1074 | 0.01 | | |
| 806 | 0.02 | 942 | 0.01 | 1078 | 0.01 | | |
| 810 | 0.02 | 946 | 0.01 | 1082 | 0.01 | | |
| 814 | 0.02 | 950 | 0.01 | 1086 | 0.01 | | |
| 818 | 0.02 | 954 | 0.01 | 1090 | 0.01 | | |
| 822 | 0.02 | 958 | 0.01 | 1094 | 0.01 | | |
| 826 | 0.02 | 962 | 0.01 | 1098 | 0.01 | | |
| 830 | 0.02 | 966 | 0.01 | 1102 | 0.01 | | |
| 834 | 0.02 | 970 | 0.01 | 1106 | 0.01 | | |
| 838 | 0.02 | 974 | 0.01 | 1110 | 0.01 | | |
| 842 | 0.02 | 978 | 0.01 | 1114 | 0.01 | | |
| 846 | 0.02 | 982 | 0.01 | 1118 | 0.01 | | |
| 850 | 0.02 | 986 | 0.01 | 1122 | 0.01 | | |

Hydrograph Report

Hyd. No. 8

Basin 1 In

Hydrograph type = Combine
Storm frequency = 2 yrs
Inflow hyds. = 2, 3

Peak discharge = 3.34 cfs
Time interval = 2 min

Hydrograph Volume = 12,924 cuft

Hydrograph Discharge Table

| Time (min) | Hyd. 2 + (cfs) | Hyd. 3 + (cfs) | Outflow (cfs) |
|------------|----------------|----------------|---------------|
| 668 | 0.17 | 0.00 | 0.17 |
| 672 | 0.18 | 0.00 | 0.18 |
| 676 | 0.20 | 0.00 | 0.20 |
| 680 | 0.22 | 0.00 | 0.22 |
| 684 | 0.24 | 0.00 | 0.24 |
| 688 | 0.27 | 0.00 | 0.27 |
| 692 | 0.29 | 0.00 | 0.29 |
| 696 | 0.34 | 0.00 | 0.34 |
| 700 | 0.44 | 0.00 | 0.44 |
| 704 | 0.59 | 0.00 | 0.59 |
| 708 | 0.78 | 0.00 | 0.78 |
| 712 | 1.01 | 0.00 | 1.01 |
| 716 | 1.28 | 0.00 | 1.28 |
| 720 | 1.81 | 0.03 | 1.85 |
| 724 | 2.71 | 0.08 | 2.79 |
| 728 | 3.26 << | 0.08 | 3.34 << |
| 732 | 3.07 | 0.07 | 3.13 |
| 736 | 2.55 | 0.06 | 2.61 |
| 740 | 1.99 | 0.06 | 2.05 |
| 744 | 1.59 | 0.05 | 1.64 |
| 748 | 1.33 | 0.04 | 1.37 |
| 752 | 1.06 | 0.03 | 1.09 |
| 756 | 0.83 | 0.02 | 0.85 |
| 760 | 0.66 | 0.02 | 0.68 |
| 764 | 0.57 | 0.02 | 0.59 |
| 768 | 0.52 | 0.02 | 0.54 |
| 772 | 0.49 | 0.02 | 0.51 |
| 776 | 0.46 | 0.02 | 0.48 |
| 780 | 0.43 | 0.02 | 0.45 |
| 784 | 0.40 | 0.02 | 0.42 |
| 788 | 0.38 | 0.02 | 0.39 |
| 792 | 0.36 | 0.02 | 0.38 |
| 796 | 0.35 | 0.02 | 0.37 |
| 800 | 0.34 | 0.02 | 0.36 |
| 804 | 0.34 | 0.02 | 0.35 |
| 808 | 0.33 | 0.02 | 0.34 |
| 812 | 0.32 | 0.02 | 0.34 |
| 816 | 0.31 | 0.02 | 0.33 |

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Hydrograph Discharge Table

| Time (min) | Hyd. 2 + (cfs) | Hyd. 3 + (cfs) | Outflow (cfs) |
|-----------------------|---------------------------|---------------------------|--------------------------|
| 820 | 0.31 | 0.01 | 0.32 |
| 824 | 0.30 | 0.01 | 0.31 |
| 828 | 0.29 | 0.01 | 0.30 |
| 832 | 0.28 | 0.01 | 0.30 |
| 836 | 0.27 | 0.01 | 0.29 |
| 840 | 0.27 | 0.01 | 0.28 |
| 844 | 0.26 | 0.01 | 0.27 |
| 848 | 0.25 | 0.01 | 0.27 |
| 852 | 0.25 | 0.01 | 0.26 |
| 856 | 0.24 | 0.01 | 0.26 |
| 860 | 0.24 | 0.01 | 0.25 |
| 864 | 0.24 | 0.01 | 0.25 |
| 868 | 0.23 | 0.01 | 0.24 |
| 872 | 0.23 | 0.01 | 0.24 |
| 876 | 0.23 | 0.01 | 0.24 |
| 880 | 0.22 | 0.01 | 0.23 |
| 884 | 0.22 | 0.01 | 0.23 |
| 888 | 0.21 | 0.01 | 0.23 |
| 892 | 0.21 | 0.01 | 0.22 |
| 896 | 0.21 | 0.01 | 0.22 |
| 900 | 0.20 | 0.01 | 0.21 |
| 904 | 0.20 | 0.01 | 0.21 |
| 908 | 0.20 | 0.01 | 0.21 |
| 912 | 0.19 | 0.01 | 0.20 |
| 916 | 0.19 | 0.01 | 0.20 |
| 920 | 0.18 | 0.01 | 0.19 |
| 924 | 0.18 | 0.01 | 0.19 |
| 928 | 0.18 | 0.01 | 0.19 |
| 932 | 0.17 | 0.01 | 0.18 |
| 936 | 0.17 | 0.01 | 0.18 |
| 940 | 0.16 | 0.01 | 0.17 |
| 944 | 0.16 | 0.01 | 0.17 |

...End

Hydrograph Report

Hyd. No. 9

Basin 2 In

Hydrograph type = Combine
Storm frequency = 2 yrs
Inflow hyds. = 4, 5

Peak discharge = 4.09 cfs
Time interval = 2 min

Hydrograph Volume = 16,805 cuft

Hydrograph Discharge Table

| Time (min) | Hyd. 4 + (cfs) | Hyd. 5 + (cfs) | Outflow (cfs) |
|------------|----------------|----------------|---------------|
| 652 | 0.21 | 0.00 | 0.21 |
| 656 | 0.22 | 0.00 | 0.22 |
| 660 | 0.23 | 0.00 | 0.23 |
| 664 | 0.24 | 0.00 | 0.24 |
| 668 | 0.25 | 0.00 | 0.25 |
| 672 | 0.27 | 0.00 | 0.27 |
| 676 | 0.29 | 0.00 | 0.29 |
| 680 | 0.32 | 0.00 | 0.32 |
| 684 | 0.35 | 0.00 | 0.35 |
| 688 | 0.38 | 0.00 | 0.38 |
| 692 | 0.41 | 0.00 | 0.41 |
| 696 | 0.46 | 0.00 | 0.46 |
| 700 | 0.57 | 0.00 | 0.57 |
| 704 | 0.74 | 0.00 | 0.74 |
| 708 | 0.97 | 0.00 | 0.97 |
| 712 | 1.25 | 0.00 | 1.25 |
| 716 | 1.59 | 0.00 | 1.59 |
| 720 | 2.16 | 0.03 | 2.19 |
| 724 | 3.07 | 0.08 | 3.15 |
| 728 | 3.87 | 0.08 | 3.95 |
| 732 | 3.98 | 0.06 | 4.05 |
| 736 | 3.55 | 0.06 | 3.61 |
| 740 | 2.96 | 0.05 | 3.01 |
| 744 | 2.32 | 0.05 | 2.37 |
| 748 | 1.85 | 0.04 | 1.89 |
| 752 | 1.50 | 0.03 | 1.53 |
| 756 | 1.19 | 0.02 | 1.22 |
| 760 | 0.94 | 0.02 | 0.97 |
| 764 | 0.78 | 0.02 | 0.80 |
| 768 | 0.68 | 0.02 | 0.70 |
| 772 | 0.63 | 0.02 | 0.65 |
| 776 | 0.59 | 0.02 | 0.61 |
| 780 | 0.55 | 0.02 | 0.57 |
| 784 | 0.52 | 0.02 | 0.53 |
| 788 | 0.49 | 0.02 | 0.50 |
| 792 | 0.46 | 0.02 | 0.48 |
| 796 | 0.44 | 0.02 | 0.46 |
| 800 | 0.43 | 0.02 | 0.45 |

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Hydrograph Discharge Table

| Time (min) | Hyd. 4 + (cfs) | Hyd. 5 + (cfs) | Outflow (cfs) |
|---------------|-------------------|-------------------|------------------|
| 804 | 0.42 | 0.02 | |
| 808 | 0.41 | 0.02 | 0.44 |
| 812 | 0.40 | 0.01 | 0.43 |
| 816 | 0.39 | 0.01 | 0.42 |
| 820 | 0.38 | 0.01 | 0.41 |
| 824 | 0.37 | 0.01 | 0.40 |
| 828 | 0.36 | 0.01 | 0.39 |
| 832 | 0.35 | 0.01 | 0.38 |
| 836 | 0.35 | 0.01 | 0.37 |
| 840 | 0.34 | 0.01 | 0.36 |
| 844 | 0.33 | 0.01 | 0.35 |
| 848 | 0.32 | 0.01 | 0.34 |
| 852 | 0.31 | 0.01 | 0.33 |
| 856 | 0.30 | 0.01 | 0.32 |
| 860 | 0.30 | 0.01 | 0.32 |
| 864 | 0.29 | 0.01 | 0.31 |
| 868 | 0.29 | 0.01 | 0.31 |
| 872 | 0.28 | 0.01 | 0.30 |
| 876 | 0.28 | 0.01 | 0.30 |
| 880 | 0.28 | 0.01 | 0.29 |
| 884 | 0.27 | 0.01 | 0.29 |
| 888 | 0.27 | 0.01 | 0.28 |
| 892 | 0.26 | 0.01 | 0.28 |
| 896 | 0.26 | 0.01 | 0.27 |
| 900 | 0.25 | 0.01 | 0.27 |
| 904 | 0.25 | 0.01 | 0.26 |
| 908 | 0.24 | 0.01 | 0.26 |
| 912 | 0.24 | 0.01 | 0.25 |
| 916 | 0.23 | 0.01 | 0.25 |
| 920 | 0.23 | 0.01 | 0.24 |
| 924 | 0.22 | 0.01 | 0.24 |
| 928 | 0.22 | 0.01 | 0.23 |
| 932 | 0.21 | 0.01 | 0.23 |
| 936 | 0.21 | 0.01 | 0.22 |
| 940 | 0.20 | 0.01 | 0.22 |
| 944 | 0.20 | 0.01 | 0.21 |
| | | | 0.21 |

...End

Hydrograph Report

Hyd. No. 9

Basin 2 In

Hydrograph type = Combine
Storm frequency = 2 yrs
Inflow hyds. = 4, 5

Peak discharge = 4.09 cfs
Time interval = 2 min

Hydrograph Volume = 16,805 cuft

Hydrograph Discharge Table

| Time (min) | Hyd. 4 + (cfs) | Hyd. 5 + (cfs) | Outflow (cfs) |
|------------|----------------|----------------|---------------|
| 652 | 0.21 | 0.00 | 0.21 |
| 656 | 0.22 | 0.00 | 0.22 |
| 660 | 0.23 | 0.00 | 0.23 |
| 664 | 0.24 | 0.00 | 0.24 |
| 668 | 0.25 | 0.00 | 0.25 |
| 672 | 0.27 | 0.00 | 0.27 |
| 676 | 0.29 | 0.00 | 0.29 |
| 680 | 0.32 | 0.00 | 0.32 |
| 684 | 0.35 | 0.00 | 0.35 |
| 688 | 0.38 | 0.00 | 0.38 |
| 692 | 0.41 | 0.00 | 0.41 |
| 696 | 0.46 | 0.00 | 0.46 |
| 700 | 0.57 | 0.00 | 0.57 |
| 704 | 0.74 | 0.00 | 0.74 |
| 708 | 0.97 | 0.00 | 0.97 |
| 712 | 1.25 | 0.00 | 1.25 |
| 716 | 1.59 | 0.00 | 1.59 |
| 720 | 2.16 | 0.03 | 2.19 |
| 724 | 3.07 | 0.08 | 3.15 |
| 728 | 3.87 | 0.08 | 3.95 |
| 732 | 3.98 | 0.06 | 4.05 |
| 736 | 3.55 | 0.06 | 3.61 |
| 740 | 2.96 | 0.05 | 3.01 |
| 744 | 2.32 | 0.05 | 2.37 |
| 748 | 1.85 | 0.04 | 1.89 |
| 752 | 1.50 | 0.03 | 1.53 |
| 756 | 1.19 | 0.02 | 1.22 |
| 760 | 0.94 | 0.02 | 0.97 |
| 764 | 0.78 | 0.02 | 0.80 |
| 768 | 0.68 | 0.02 | 0.70 |
| 772 | 0.63 | 0.02 | 0.65 |
| 776 | 0.59 | 0.02 | 0.61 |
| 780 | 0.55 | 0.02 | 0.57 |
| 784 | 0.52 | 0.02 | 0.53 |
| 788 | 0.49 | 0.02 | 0.50 |
| 792 | 0.46 | 0.02 | 0.48 |
| 796 | 0.44 | 0.02 | 0.46 |
| 800 | 0.43 | 0.02 | 0.45 |

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Hydrograph Discharge Table

| Time (min) | Hyd. 4 + (cfs) | Hyd. 5 + (cfs) | Outflow (cfs) |
|-----------------------|---------------------------|---------------------------|--------------------------|
| 804 | 0.42 | 0.02 | 0.44 |
| 808 | 0.41 | 0.02 | 0.43 |
| 812 | 0.40 | 0.01 | 0.42 |
| 816 | 0.39 | 0.01 | 0.41 |
| 820 | 0.38 | 0.01 | 0.40 |
| 824 | 0.37 | 0.01 | 0.39 |
| 828 | 0.36 | 0.01 | 0.38 |
| 832 | 0.35 | 0.01 | 0.37 |
| 836 | 0.35 | 0.01 | 0.36 |
| 840 | 0.34 | 0.01 | 0.35 |
| 844 | 0.33 | 0.01 | 0.34 |
| 848 | 0.32 | 0.01 | 0.33 |
| 852 | 0.31 | 0.01 | 0.32 |
| 856 | 0.30 | 0.01 | 0.32 |
| 860 | 0.30 | 0.01 | 0.31 |
| 864 | 0.29 | 0.01 | 0.31 |
| 868 | 0.29 | 0.01 | 0.30 |
| 872 | 0.28 | 0.01 | 0.30 |
| 876 | 0.28 | 0.01 | 0.29 |
| 880 | 0.28 | 0.01 | 0.29 |
| 884 | 0.27 | 0.01 | 0.28 |
| 888 | 0.27 | 0.01 | 0.28 |
| 892 | 0.26 | 0.01 | 0.27 |
| 896 | 0.26 | 0.01 | 0.27 |
| 900 | 0.25 | 0.01 | 0.26 |
| 904 | 0.25 | 0.01 | 0.26 |
| 908 | 0.24 | 0.01 | 0.25 |
| 912 | 0.24 | 0.01 | 0.25 |
| 916 | 0.23 | 0.01 | 0.24 |
| 920 | 0.23 | 0.01 | 0.24 |
| 924 | 0.22 | 0.01 | 0.23 |
| 928 | 0.22 | 0.01 | 0.23 |
| 932 | 0.21 | 0.01 | 0.22 |
| 936 | 0.21 | 0.01 | 0.22 |
| 940 | 0.20 | 0.01 | 0.21 |
| 944 | 0.20 | 0.01 | 0.21 |

...End

Hydrograph Report

Hyd. No. 10

Basin 3 In

Hydrograph type = Combine
Storm frequency = 2 yrs
Inflow hyds. = 6, 7

Peak discharge = 6.00 cfs
Time interval = 2 min

Hydrograph Volume = 20,626 cuft

Hydrograph Discharge Table

| Time (min) | Hyd. 6 + (cfs) | Hyd. 7 + (cfs) | Outflow (cfs) |
|------------|----------------|----------------|---------------|
| 672 | 0.31 | 0.00 | 0.31 |
| 676 | 0.35 | 0.00 | 0.35 |
| 680 | 0.38 | 0.00 | 0.38 |
| 684 | 0.42 | 0.00 | 0.42 |
| 688 | 0.45 | 0.00 | 0.45 |
| 692 | 0.50 | 0.00 | 0.50 |
| 696 | 0.61 | 0.00 | 0.61 |
| 700 | 0.83 | 0.00 | 0.83 |
| 704 | 1.13 | 0.00 | 1.13 |
| 708 | 1.48 | 0.00 | 1.48 |
| 712 | 1.87 | 0.00 | 1.87 |
| 716 | 2.36 | 0.00 | 2.37 |
| 720 | 3.59 | 0.04 | 3.63 |
| 724 | 5.48 | 0.10 | 5.58 |
| 728 | 5.71 | 0.10 | 5.81 |
| 732 | 4.43 | 0.08 | 4.51 |
| 736 | 3.25 | 0.08 | 3.33 |
| 740 | 2.68 | 0.07 | 2.75 |
| 744 | 2.28 | 0.06 | 2.34 |
| 748 | 1.85 | 0.05 | 1.90 |
| 752 | 1.42 | 0.04 | 1.46 |
| 756 | 1.08 | 0.03 | 1.11 |
| 760 | 0.91 | 0.03 | 0.94 |
| 764 | 0.84 | 0.03 | 0.87 |
| 768 | 0.80 | 0.03 | 0.82 |
| 772 | 0.75 | 0.03 | 0.78 |
| 776 | 0.70 | 0.02 | 0.73 |
| 780 | 0.66 | 0.02 | 0.68 |
| 784 | 0.61 | 0.02 | 0.64 |
| 788 | 0.58 | 0.02 | 0.61 |
| 792 | 0.57 | 0.02 | 0.59 |
| 796 | 0.55 | 0.02 | 0.58 |
| 800 | 0.54 | 0.02 | 0.56 |
| 804 | 0.53 | 0.02 | 0.55 |
| 808 | 0.52 | 0.02 | 0.54 |
| 812 | 0.51 | 0.02 | 0.53 |
| 816 | 0.50 | 0.02 | 0.51 |
| 820 | 0.48 | 0.02 | 0.50 |

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Hydrograph Discharge Table

| Time (min) | Hyd. 6 + (cfs) | Hyd. 7 + (cfs) | Outflow (cfs) |
|-----------------------|---------------------------|---------------------------|--------------------------|
| 824 | 0.47 | 0.02 | 0.49 |
| 828 | 0.46 | 0.02 | 0.48 |
| 832 | 0.45 | 0.02 | 0.46 |
| 836 | 0.43 | 0.02 | 0.45 |
| 840 | 0.42 | 0.02 | 0.44 |
| 844 | 0.41 | 0.02 | 0.43 |
| 848 | 0.40 | 0.02 | 0.42 |
| 852 | 0.39 | 0.02 | 0.41 |
| 856 | 0.39 | 0.02 | 0.40 |
| 860 | 0.38 | 0.02 | 0.40 |
| 864 | 0.38 | 0.02 | 0.39 |
| 868 | 0.37 | 0.02 | 0.38 |
| 872 | 0.36 | 0.01 | 0.38 |
| 876 | 0.36 | 0.01 | 0.37 |
| 880 | 0.35 | 0.01 | 0.37 |
| 884 | 0.35 | 0.01 | 0.36 |
| 888 | 0.34 | 0.01 | 0.35 |
| 892 | 0.33 | 0.01 | 0.35 |
| 896 | 0.33 | 0.01 | 0.34 |
| 900 | 0.32 | 0.01 | 0.34 |
| 904 | 0.32 | 0.01 | 0.33 |
| 908 | 0.31 | 0.01 | 0.32 |
| 912 | 0.30 | 0.01 | 0.32 |
| 916 | 0.30 | 0.01 | 0.31 |
| 920 | 0.29 | 0.01 | 0.30 |

...End

Hydrograph Report

Hyd. No. 11

Basin 1 Out

Hydrograph type = Reservoir
 Storm frequency = 2 yrs
 Inflow hyd. No. = 8
 Max. Elevation = 241.09 ft

Peak discharge = 0.23 cfs
 Time interval = 2 min
 Reservoir name = Retention Basin N
 Max. Storage = 18,429 cuft

Storage Indication method used.

Outflow hydrograph volume = 12,862 cuft

Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 620 | 0.09 | 240.04 | 23.09 | 0.01 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.01 |
| 624 | 0.09 | 240.04 | 23.09 | 0.01 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.01 |
| 628 | 0.10 | 240.04 | 23.09 | 0.01 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.01 |
| 632 | 0.10 | 240.05 | 23.09 | 0.01 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.01 |
| 636 | 0.11 | 240.05 | 23.09 | 0.02 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.02 |
| 640 | 0.12 | 240.05 | 23.09 | 0.02 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.02 |
| 644 | 0.12 | 240.06 | 23.09 | 0.02 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.02 |
| 648 | 0.13 | 240.06 | 23.09 | 0.02 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.02 |
| 652 | 0.14 | 240.06 | 23.09 | 0.02 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.02 |
| 656 | 0.14 | 240.07 | 23.09 | 0.02 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.02 |
| 660 | 0.15 | 240.07 | 23.09 | 0.02 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.02 |
| 664 | 0.16 | 240.08 | 23.09 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.03 |
| 668 | 0.17 | 240.08 | 23.09 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.03 |
| 672 | 0.18 | 240.09 | 23.09 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.03 |
| 676 | 0.20 | 240.09 | 23.09 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.03 |
| 680 | 0.22 | 240.10 | 23.09 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.03 |
| 684 | 0.24 | 240.11 | 23.09 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.03 |
| 688 | 0.27 | 240.12 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 692 | 0.29 | 240.12 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 696 | 0.34 | 240.13 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 700 | 0.44 | 240.15 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 704 | 0.59 | 240.16 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 708 | 0.78 | 240.18 | 23.09 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |
| 712 | 1.01 | 240.21 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 716 | 1.28 | 240.25 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 720 | 1.85 | 240.30 | 23.09 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 724 | 2.79 | 240.38 | 23.09 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.12 |
| 728 | 3.34 << | 240.49 | 23.09 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 732 | 3.13 | 240.60 | 23.09 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |
| 736 | 2.61 | 240.70 | 23.09 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 740 | 2.05 | 240.78 | 23.09 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 744 | 1.64 | 240.84 | 23.09 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 748 | 1.37 | 240.88 | 23.09 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 752 | 1.09 | 240.92 | 23.09 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 756 | 0.85 | 240.95 | 23.09 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 760 | 0.68 | 240.97 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 764 | 0.59 | 240.98 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 768 | 0.54 | 240.99 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |

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Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 772 | 0.51 | 241.00 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 776 | 0.48 | 241.01 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 780 | 0.45 | 241.02 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 784 | 0.42 | 241.03 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 788 | 0.39 | 241.04 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 792 | 0.38 | 241.04 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 796 | 0.37 | 241.05 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 800 | 0.36 | 241.05 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 804 | 0.35 | 241.06 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 808 | 0.34 | 241.06 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 812 | 0.34 | 241.07 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 816 | 0.33 | 241.07 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 820 | 0.32 | 241.07 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 824 | 0.31 | 241.08 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 828 | 0.30 | 241.08 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 832 | 0.30 | 241.08 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 836 | 0.29 | 241.08 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 840 | 0.28 | 241.09 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 844 | 0.27 | 241.09 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 848 | 0.27 | 241.09 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 852 | 0.26 | 241.09 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 856 | 0.26 | 241.09 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 860 | 0.25 | 241.09 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 864 | 0.25 | 241.09 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 868 | 0.24 | 241.09 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 872 | 0.24 | 241.09 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 876 | 0.24 | 241.09 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 880 | 0.23 | 241.09 << | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 << |
| 884 | 0.23 | 241.09 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 888 | 0.23 | 241.09 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 892 | 0.22 | 241.09 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 896 | 0.22 | 241.09 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 900 | 0.21 | 241.09 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 904 | 0.21 | 241.09 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 908 | 0.21 | 241.09 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 912 | 0.20 | 241.09 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 916 | 0.20 | 241.09 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 920 | 0.19 | 241.09 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 924 | 0.19 | 241.09 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 928 | 0.19 | 241.08 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 932 | 0.18 | 241.08 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 936 | 0.18 | 241.08 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 940 | 0.17 | 241.08 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 944 | 0.17 | 241.08 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 948 | 0.17 | 241.07 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 952 | 0.16 | 241.07 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 956 | 0.16 | 241.07 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 960 | 0.15 | 241.07 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 964 | 0.15 | 241.06 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 968 | 0.15 | 241.06 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 972 | 0.14 | 241.06 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |

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Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 976 | 0.14 | 241.05 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 980 | 0.14 | 241.05 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 984 | 0.14 | 241.05 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 988 | 0.14 | 241.04 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 992 | 0.13 | 241.04 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 996 | 0.13 | 241.04 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 1000 | 0.13 | 241.03 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 1004 | 0.13 | 241.03 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 1008 | 0.13 | 241.03 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 1012 | 0.12 | 241.02 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 1016 | 0.12 | 241.02 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 1020 | 0.12 | 241.02 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 1024 | 0.12 | 241.01 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 1028 | 0.12 | 241.01 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 1032 | 0.12 | 241.01 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 1036 | 0.11 | 241.00 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 1040 | 0.11 | 241.00 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 1044 | 0.11 | 240.99 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 1048 | 0.11 | 240.99 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 1052 | 0.11 | 240.99 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 1056 | 0.10 | 240.98 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 1060 | 0.10 | 240.98 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 1064 | 0.10 | 240.97 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 1068 | 0.10 | 240.97 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 1072 | 0.10 | 240.97 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 1076 | 0.10 | 240.96 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 1080 | 0.09 | 240.96 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 1084 | 0.09 | 240.95 | 23.09 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 1088 | 0.09 | 240.95 | 23.09 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 1092 | 0.09 | 240.94 | 23.09 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 1096 | 0.09 | 240.94 | 23.09 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 1100 | 0.09 | 240.93 | 23.09 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 1104 | 0.09 | 240.93 | 23.09 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 1108 | 0.09 | 240.93 | 23.09 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 1112 | 0.09 | 240.92 | 23.09 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 1116 | 0.09 | 240.92 | 23.09 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 1120 | 0.09 | 240.91 | 23.09 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 1124 | 0.09 | 240.91 | 23.09 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 1128 | 0.08 | 240.90 | 23.09 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 1132 | 0.08 | 240.90 | 23.09 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 1136 | 0.08 | 240.89 | 23.09 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 1140 | 0.08 | 240.89 | 23.09 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 1144 | 0.08 | 240.89 | 23.09 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 1148 | 0.08 | 240.88 | 23.09 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 1152 | 0.08 | 240.88 | 23.09 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 1156 | 0.08 | 240.87 | 23.09 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 1160 | 0.08 | 240.87 | 23.09 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 1164 | 0.08 | 240.86 | 23.09 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 1168 | 0.08 | 240.86 | 23.09 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 1172 | 0.08 | 240.85 | 23.09 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 1176 | 0.08 | 240.85 | 23.09 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |

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Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 1180 | 0.08 | 240.85 | 23.09 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 1184 | 0.08 | 240.84 | 23.09 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 1188 | 0.08 | 240.84 | 23.09 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 1192 | 0.08 | 240.83 | 23.09 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 1196 | 0.08 | 240.83 | 23.09 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 1200 | 0.07 | 240.82 | 23.09 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 1204 | 0.07 | 240.82 | 23.09 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 1208 | 0.07 | 240.81 | 23.09 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 1212 | 0.07 | 240.81 | 23.09 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 1216 | 0.07 | 240.81 | 23.09 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 1220 | 0.07 | 240.80 | 23.09 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 1224 | 0.07 | 240.80 | 23.09 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 1228 | 0.07 | 240.79 | 23.09 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 1232 | 0.07 | 240.79 | 23.09 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 1236 | 0.07 | 240.78 | 23.09 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 1240 | 0.07 | 240.78 | 23.09 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 1244 | 0.07 | 240.78 | 23.09 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 1248 | 0.07 | 240.77 | 23.09 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 1252 | 0.07 | 240.77 | 23.09 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 1256 | 0.07 | 240.76 | 23.09 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 1260 | 0.07 | 240.76 | 23.09 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 1264 | 0.07 | 240.75 | 23.09 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 1268 | 0.07 | 240.75 | 23.09 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 1272 | 0.06 | 240.75 | 23.09 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 1276 | 0.06 | 240.74 | 23.09 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 1280 | 0.06 | 240.74 | 23.09 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 1284 | 0.06 | 240.73 | 23.09 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 1288 | 0.06 | 240.73 | 23.09 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 1292 | 0.06 | 240.72 | 23.09 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 1296 | 0.06 | 240.72 | 23.09 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 1300 | 0.06 | 240.71 | 23.09 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 1304 | 0.06 | 240.71 | 23.09 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 1308 | 0.06 | 240.71 | 23.09 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 1312 | 0.06 | 240.70 | 23.09 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 1316 | 0.06 | 240.70 | 23.09 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 1320 | 0.06 | 240.69 | 23.09 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 1324 | 0.07 | 240.69 | 23.09 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 1328 | 0.08 | 240.69 | 23.09 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 1332 | 0.08 | 240.68 | 23.09 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 1336 | 0.07 | 240.68 | 23.09 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 1340 | 0.06 | 240.67 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 1344 | 0.06 | 240.67 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 1348 | 0.06 | 240.67 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 1352 | 0.06 | 240.66 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 1356 | 0.06 | 240.66 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 1360 | 0.06 | 240.65 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 1364 | 0.06 | 240.65 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 1368 | 0.06 | 240.65 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 1372 | 0.06 | 240.64 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 1376 | 0.06 | 240.64 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 1380 | 0.06 | 240.63 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |

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Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 1384 | 0.06 | 240.63 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 1388 | 0.06 | 240.63 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 1392 | 0.05 | 240.62 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 1396 | 0.05 | 240.62 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 1400 | 0.05 | 240.61 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 1404 | 0.05 | 240.61 | 23.09 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |
| 1408 | 0.05 | 240.61 | 23.09 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |
| 1412 | 0.05 | 240.60 | 23.09 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |
| 1416 | 0.05 | 240.60 | 23.09 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |
| 1420 | 0.05 | 240.59 | 23.09 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |
| 1424 | 0.05 | 240.59 | 23.09 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |
| 1428 | 0.05 | 240.59 | 23.09 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |
| 1432 | 0.05 | 240.58 | 23.09 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |
| 1436 | 0.05 | 240.58 | 23.09 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |
| 1440 | 0.05 | 240.57 | 23.09 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |
| 1444 | 0.04 | 240.57 | 23.09 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |
| 1448 | 0.03 | 240.57 | 23.09 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |
| 1452 | 0.01 | 240.56 | 23.09 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |
| 1456 | 0.00 | 240.56 | 23.09 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 1460 | 0.00 | 240.55 | 23.09 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 1464 | 0.00 | 240.54 | 23.09 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 1468 | 0.00 | 240.54 | 23.09 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 1472 | 0.00 | 240.53 | 23.09 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 1476 | 0.00 | 240.53 | 23.09 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 1480 | 0.00 | 240.52 | 23.09 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 1484 | 0.00 | 240.52 | 23.09 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 1488 | 0.00 | 240.51 | 23.09 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 1492 | 0.00 | 240.51 | 23.09 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 1496 | 0.00 | 240.50 | 23.09 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 1500 | 0.00 | 240.50 | 23.09 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 1504 | 0.00 | 240.49 | 23.09 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 1508 | 0.00 | 240.49 | 23.09 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 1512 | 0.00 | 240.48 | 23.09 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 1516 | 0.00 | 240.48 | 23.09 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 1520 | 0.00 | 240.47 | 23.09 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 1524 | 0.00 | 240.47 | 23.09 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 1528 | 0.00 | 240.46 | 23.09 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 1532 | 0.00 | 240.46 | 23.09 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 1536 | 0.00 | 240.45 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 1540 | 0.00 | 240.45 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 1544 | 0.00 | 240.44 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 1548 | 0.00 | 240.44 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 1552 | 0.00 | 240.43 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 1556 | 0.00 | 240.43 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 1560 | 0.00 | 240.42 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 1564 | 0.00 | 240.42 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 1568 | 0.00 | 240.41 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 1572 | 0.00 | 240.41 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 1576 | 0.00 | 240.41 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 1580 | 0.00 | 240.40 | 23.09 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.12 |
| 1584 | 0.00 | 240.40 | 23.09 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.12 |

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Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 1588 | 0.00 | 240.39 | 23.09 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.12 |
| 1592 | 0.00 | 240.39 | 23.09 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.12 |
| 1596 | 0.00 | 240.38 | 23.09 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.12 |
| 1600 | 0.00 | 240.38 | 23.09 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.12 |
| 1604 | 0.00 | 240.38 | 23.09 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.12 |
| 1608 | 0.00 | 240.37 | 23.09 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.12 |
| 1612 | 0.00 | 240.37 | 23.09 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.11 |
| 1616 | 0.00 | 240.36 | 23.09 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.11 |
| 1620 | 0.00 | 240.36 | 23.09 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.11 |
| 1624 | 0.00 | 240.36 | 23.09 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.11 |
| 1628 | 0.00 | 240.35 | 23.09 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.11 |
| 1632 | 0.00 | 240.35 | 23.09 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.11 |
| 1636 | 0.00 | 240.34 | 23.09 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.11 |
| 1640 | 0.00 | 240.34 | 23.09 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.11 |
| 1644 | 0.00 | 240.34 | 23.09 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 1648 | 0.00 | 240.33 | 23.09 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 1652 | 0.00 | 240.33 | 23.09 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 1656 | 0.00 | 240.32 | 23.09 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 1660 | 0.00 | 240.32 | 23.09 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 1664 | 0.00 | 240.32 | 23.09 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 1668 | 0.00 | 240.31 | 23.09 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 1672 | 0.00 | 240.31 | 23.09 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 1676 | 0.00 | 240.31 | 23.09 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 1680 | 0.00 | 240.30 | 23.09 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 1684 | 0.00 | 240.30 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 1688 | 0.00 | 240.30 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 1692 | 0.00 | 240.29 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 1696 | 0.00 | 240.29 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 1700 | 0.00 | 240.29 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 1704 | 0.00 | 240.28 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 1708 | 0.00 | 240.28 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 1712 | 0.00 | 240.28 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 1716 | 0.00 | 240.27 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 1720 | 0.00 | 240.27 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 1724 | 0.00 | 240.27 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 1728 | 0.00 | 240.26 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 1732 | 0.00 | 240.26 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 1736 | 0.00 | 240.26 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 1740 | 0.00 | 240.26 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 1744 | 0.00 | 240.25 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 1748 | 0.00 | 240.25 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 1752 | 0.00 | 240.25 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 1756 | 0.00 | 240.24 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 1760 | 0.00 | 240.24 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 1764 | 0.00 | 240.24 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 1768 | 0.00 | 240.24 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 1772 | 0.00 | 240.23 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 1776 | 0.00 | 240.23 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 1780 | 0.00 | 240.23 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 1784 | 0.00 | 240.23 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 1788 | 0.00 | 240.22 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |

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Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 1792 | 0.00 | 240.22 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 1796 | 0.00 | 240.22 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 1800 | 0.00 | 240.22 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 1804 | 0.00 | 240.21 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 1808 | 0.00 | 240.21 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 1812 | 0.00 | 240.21 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 1816 | 0.00 | 240.21 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 1820 | 0.00 | 240.20 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 1824 | 0.00 | 240.20 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 1828 | 0.00 | 240.20 | 23.09 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |
| 1832 | 0.00 | 240.20 | 23.09 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |
| 1836 | 0.00 | 240.19 | 23.09 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |
| 1840 | 0.00 | 240.19 | 23.09 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |
| 1844 | 0.00 | 240.19 | 23.09 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |
| 1848 | 0.00 | 240.19 | 23.09 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |
| 1852 | 0.00 | 240.19 | 23.09 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |
| 1856 | 0.00 | 240.18 | 23.09 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |
| 1860 | 0.00 | 240.18 | 23.09 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |
| 1864 | 0.00 | 240.18 | 23.09 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |
| 1868 | 0.00 | 240.18 | 23.09 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |
| 1872 | 0.00 | 240.17 | 23.09 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |
| 1876 | 0.00 | 240.17 | 23.09 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |
| 1880 | 0.00 | 240.17 | 23.09 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |
| 1884 | 0.00 | 240.17 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 1888 | 0.00 | 240.17 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 1892 | 0.00 | 240.16 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 1896 | 0.00 | 240.16 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 1900 | 0.00 | 240.16 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 1904 | 0.00 | 240.16 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 1908 | 0.00 | 240.16 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 1912 | 0.00 | 240.16 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 1916 | 0.00 | 240.15 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 1920 | 0.00 | 240.15 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 1924 | 0.00 | 240.15 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 1928 | 0.00 | 240.15 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 1932 | 0.00 | 240.15 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 1936 | 0.00 | 240.14 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 1940 | 0.00 | 240.14 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 1944 | 0.00 | 240.14 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 1948 | 0.00 | 240.14 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 1952 | 0.00 | 240.14 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 1956 | 0.00 | 240.14 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 1960 | 0.00 | 240.14 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 1964 | 0.00 | 240.13 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 1968 | 0.00 | 240.13 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 1972 | 0.00 | 240.13 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 1976 | 0.00 | 240.13 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 1980 | 0.00 | 240.13 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 1984 | 0.00 | 240.13 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 1988 | 0.00 | 240.12 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 1992 | 0.00 | 240.12 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |

Continues on next page...

Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Civ A cfs | Civ B cfs | Civ C cfs | Civ D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|-----------------------|-----------------------|-------------------------|----------------------|----------------------|----------------------|----------------------|---------------------|---------------------|---------------------|---------------------|----------------------|------------------------|
| 2404 | 0.00 | 240.04 | 23.09 | 0.01 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.01 |
| 2408 | 0.00 | 240.04 | 23.09 | 0.01 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.01 |
| 2412 | 0.00 | 240.04 | 23.09 | 0.01 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.01 |
| 2416 | 0.00 | 240.04 | 23.09 | 0.01 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.01 |

...End

Reservoir Report

Reservoir No. 1 - Retention Basin No. 1

Hydraflow Hydrographs by Intelisolve

Pond Data

Pond storage is based on known contour areas. Average end area method used.

Stage / Storage Table

| Stage (ft) | Elevation (ft) | Contour area (sqft) | Incr. Storage (cuft) | Total storage (cuft) |
|------------|----------------|---------------------|----------------------|----------------------|
| 0.00 | 238.00 | 4,449 | 0 | 0 |
| 2.00 | 240.00 | 6,679 | 11,128 | 11,128 |
| 4.00 | 242.00 | 6,679 | 13,358 | 24,486 |
| 6.00 | 244.00 | 6,679 | 13,358 | 37,844 |
| 8.00 | 246.00 | 6,679 | 13,358 | 51,202 |
| 8.50 | 246.50 | 6,679 | 3,340 | 54,542 |

Culvert / Orifice Structures

| | [A] | [B] | [C] | [D] |
|---------------|----------|--------|------|------|
| Rise in | = 6.0 | 3.0 | 0.0 | 0.0 |
| Span in | = 6.0 | 3.0 | 0.0 | 0.0 |
| No. Barrels | = 10 | 1 | 0 | 0 |
| Invert El. ft | = 227.00 | 240.00 | 0.00 | 0.00 |
| Length ft | = 68.0 | 1.0 | 0.0 | 0.0 |
| Slope % | = 6.03 | 0.00 | 0.00 | 0.00 |
| N-Value | = .013 | .013 | .000 | .000 |
| Orif. Coeff. | = 0.60 | 0.60 | 0.00 | 0.00 |
| Multi-Stage | = n/a | Yes | No | No |

Weir Structures

| | [A] | [B] | [C] | [D] |
|--------------|----------|--------|--------|------|
| Crest Len ft | = 1.00 | 40.00 | 16.00 | 0.00 |
| Crest El. ft | = 243.00 | 244.50 | 244.00 | 0.00 |
| Weir Coeff. | = 3.33 | 2.60 | 3.33 | 0.00 |
| Weir Type | = Rect | Broad | Rect | --- |
| Multi-Stage | = Yes | Yes | Yes | No |

Exfiltration Rate = 0.00 in/hr/sqft Tailwater Elev. = 0.00 ft

Stage / Storage / Discharge Table

Note: All outflows have been analyzed under inlet and outlet control.

| Stage ft | Storage cuft | Elevation ft | Civ A cfs | Civ B cfs | Civ C cfs | Civ D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Total cfs |
|----------|--------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-----------|
| 0.00 | 0 | 238.00 | 0.00 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.00 |
| 0.20 | 1,113 | 238.20 | 23.09 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.00 |
| 0.40 | 2,226 | 238.40 | 23.09 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.00 |
| 0.60 | 3,338 | 238.60 | 23.09 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.00 |
| 0.80 | 4,451 | 238.80 | 23.09 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.00 |
| 1.00 | 5,564 | 239.00 | 23.09 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.00 |
| 1.20 | 6,677 | 239.20 | 23.09 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.00 |
| 1.40 | 7,790 | 239.40 | 23.09 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.00 |
| 1.60 | 8,902 | 239.60 | 23.09 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.00 |
| 1.80 | 10,015 | 239.80 | 23.09 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.00 |
| 2.00 | 11,128 | 240.00 | 23.09 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.00 |
| 2.20 | 12,464 | 240.20 | 23.09 | 0.06 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.06 |
| 2.40 | 13,800 | 240.40 | 23.09 | 0.12 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.12 |
| 2.60 | 15,135 | 240.60 | 23.09 | 0.16 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.16 |
| 2.80 | 16,471 | 240.80 | 23.09 | 0.19 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.19 |
| 3.00 | 17,807 | 241.00 | 23.09 | 0.22 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.22 |
| 3.20 | 19,143 | 241.20 | 23.09 | 0.25 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.25 |
| 3.40 | 20,479 | 241.40 | 23.09 | 0.27 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.27 |
| 3.60 | 21,814 | 241.60 | 23.09 | 0.29 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.29 |
| 3.80 | 23,150 | 241.80 | 23.09 | 0.31 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.31 |
| 4.00 | 24,486 | 242.00 | 23.09 | 0.32 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.32 |
| 4.20 | 25,822 | 242.20 | 23.09 | 0.34 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.34 |
| 4.40 | 27,158 | 242.40 | 23.09 | 0.36 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.36 |
| 4.60 | 28,493 | 242.60 | 23.09 | 0.37 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.37 |
| 4.80 | 29,829 | 242.80 | 23.09 | 0.39 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.39 |
| 5.00 | 31,165 | 243.00 | 23.09 | 0.40 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.40 |
| 5.20 | 32,501 | 243.20 | 23.09 | 0.41 | --- | --- | 0.30 | 0.00 | 0.00 | --- | --- | 0.71 |
| 5.40 | 33,837 | 243.40 | 23.09 | 0.43 | --- | --- | 0.84 | 0.00 | 0.00 | --- | --- | 1.27 |
| 5.60 | 35,172 | 243.60 | 23.09 | 0.44 | --- | --- | 1.55 | 0.00 | 0.00 | --- | --- | 1.99 |
| 5.80 | 36,508 | 243.80 | 23.09 | 0.45 | --- | --- | 2.38 | 0.00 | 0.00 | --- | --- | 2.84 |
| 6.00 | 37,844 | 244.00 | 23.09 | 0.47 | --- | --- | 3.33 | 0.00 | 0.00 | --- | --- | 3.80 |
| 6.20 | 39,180 | 244.20 | 23.09 | 0.48 | --- | --- | 4.38 | 0.00 | 4.77 | --- | --- | 9.62 |

Continues on next page...

Stage / Storage / Discharge Table

| Stage ft | Storage cuft | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Total cfs |
|-------------|-----------------|-----------------|--------------|--------------|--------------|--------------|-------------|-------------|-------------|-------------|--------------|--------------|
| 6.40 | 40,516 | 244.40 | 23.09 | 0.49 | --- | --- | 5.52 | 0.00 | 13.48 | --- | --- | 19.48 |
| 6.60 | 41,851 | 244.60 | 27.65 | 0.12 | --- | --- | 3.92 | 3.29 | 20.31 | --- | --- | 27.64 |
| 6.80 | 43,187 | 244.80 | 27.92 | 0.05 | --- | --- | 2.40 | 10.00 | 15.47 | --- | --- | 27.92 |
| 7.00 | 44,523 | 245.00 | 28.07 | 0.03 | --- | --- | 1.86 | 12.37 | 13.75 | --- | --- | 28.02 |
| 7.20 | 45,859 | 245.20 | 28.21 | 0.02 | --- | --- | 1.58 | 13.73 | 12.83 | --- | --- | 28.16 |
| 7.40 | 47,195 | 245.40 | 28.34 | 0.02 | --- | --- | 1.40 | 14.64 | 12.28 | --- | --- | 28.34 |
| 7.60 | 48,530 | 245.60 | 28.47 | 0.01 | --- | --- | 1.28 | 15.27 | 11.88 | --- | --- | 28.43 |
| 7.80 | 49,866 | 245.80 | 28.60 | 0.01 | --- | --- | 1.18 | 15.60 | 11.49 | --- | --- | 28.28 |
| 8.00 | 51,202 | 246.00 | 28.73 | 0.01 | --- | --- | 1.11 | 15.96 | 11.27 | --- | --- | 28.34 |
| 8.05 | 51,536 | 246.05 | 28.76 | 0.01 | --- | --- | 1.10 | 16.14 | 11.30 | --- | --- | 28.55 |
| 8.10 | 51,870 | 246.10 | 28.79 | 0.01 | --- | --- | 1.09 | 16.28 | 11.29 | --- | --- | 28.67 |
| 8.15 | 52,204 | 246.15 | 28.82 | 0.01 | --- | --- | 1.08 | 16.37 | 11.27 | --- | --- | 28.72 |
| 8.20 | 52,538 | 246.20 | 28.86 | 0.01 | --- | --- | 1.06 | 16.40 | 11.20 | --- | --- | 28.68 |
| 8.25 | 52,872 | 246.25 | 28.89 | 0.01 | --- | --- | 1.05 | 16.38 | 11.10 | --- | --- | 28.53 |
| 8.30 | 53,206 | 246.30 | 28.92 | 0.01 | --- | --- | 1.02 | 16.28 | 10.96 | --- | --- | 28.28 |
| 8.35 | 53,540 | 246.35 | 28.95 | 0.01 | --- | --- | 1.00 | 16.06 | 10.74 | --- | --- | 27.80 |
| 8.40 | 53,874 | 246.40 | 28.98 | 0.01 | --- | --- | 1.01 | 16.54 | 11.00 | --- | --- | 28.56 |
| 8.45 | 54,208 | 246.45 | 29.01 | 0.01 | --- | --- | 0.98 | 16.25 | 10.74 | --- | --- | 27.98 |
| 8.50 | 54,542 | 246.50 | 29.05 | 0.01 | --- | --- | 0.98 | 16.46 | 10.82 | --- | --- | 28.27 |

...End

Hydrograph Report

Hyd. No. 12

Basin 2 Out

Hydrograph type = Reservoir
 Storm frequency = 2 yrs
 Inflow hyd. No. = 9
 Max. Elevation = 232.12 ft

Peak discharge = 0.40 cfs
 Time interval = 2 min
 Reservoir name = Detention Basin 2
 Max. Storage = 9,694 cuft

Storage Indication method used.

Outflow hydrograph volume = 13,778 cuft

Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 732 | 4.05 | 231.16 | 6.68 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | 0.032 | 0.08 |
| 736 | 3.61 | 231.38 | 6.68 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | 0.035 | 0.15 |
| 740 | 3.01 | 231.57 | 6.68 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | 0.037 | 0.19 |
| 744 | 2.37 | 231.71 | 6.68 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | 0.039 | 0.22 |
| 748 | 1.89 | 231.83 | 6.68 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | 0.040 | 0.24 |
| 752 | 1.53 | 231.91 | 6.68 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | 0.041 | 0.25 |
| 756 | 1.22 | 231.98 | 6.68 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | 0.042 | 0.26 |
| 760 | 0.97 | 232.02 | 6.68 | 0.22 | ---- | ---- | 0.02 | ---- | ---- | ---- | 0.042 | 0.28 |
| 764 | 0.80 | 232.04 | 6.68 | 0.23 | ---- | ---- | 0.04 | ---- | ---- | ---- | 0.042 | 0.31 |
| 768 | 0.70 | 232.06 | 6.68 | 0.23 | ---- | ---- | 0.06 | ---- | ---- | ---- | 0.042 | 0.33 |
| 772 | 0.65 | 232.07 | 6.68 | 0.23 | ---- | ---- | 0.07 | ---- | ---- | ---- | 0.042 | 0.34 |
| 776 | 0.61 | 232.08 | 6.68 | 0.23 | ---- | ---- | 0.08 | ---- | ---- | ---- | 0.042 | 0.35 |
| 780 | 0.57 | 232.09 | 6.68 | 0.23 | ---- | ---- | 0.09 | ---- | ---- | ---- | 0.042 | 0.36 |
| 784 | 0.53 | 232.10 | 6.68 | 0.23 | ---- | ---- | 0.10 | ---- | ---- | ---- | 0.042 | 0.37 |
| 788 | 0.50 | 232.10 | 6.68 | 0.23 | ---- | ---- | 0.10 | ---- | ---- | ---- | 0.042 | 0.38 |
| 792 | 0.48 | 232.11 | 6.68 | 0.23 | ---- | ---- | 0.11 | ---- | ---- | ---- | 0.042 | 0.38 |
| 796 | 0.46 | 232.11 | 6.68 | 0.23 | ---- | ---- | 0.11 | ---- | ---- | ---- | 0.042 | 0.39 |
| 800 | 0.45 | 232.11 | 6.68 | 0.23 | ---- | ---- | 0.11 | ---- | ---- | ---- | 0.042 | 0.39 |
| 804 | 0.44 | 232.12 | 6.68 | 0.23 | ---- | ---- | 0.11 | ---- | ---- | ---- | 0.042 | 0.39 |
| 808 | 0.43 | 232.12 | 6.68 | 0.24 | ---- | ---- | 0.12 | ---- | ---- | ---- | 0.043 | 0.39 |
| 812 | 0.42 | 232.12 | 6.68 | 0.24 | ---- | ---- | 0.12 | ---- | ---- | ---- | 0.043 | 0.39 |
| 816 | 0.41 | 232.12 | 6.68 | 0.24 | ---- | ---- | 0.12 | ---- | ---- | ---- | 0.043 | 0.39 |
| 820 | 0.40 | 232.12 << | 6.68 | 0.24 | ---- | ---- | 0.12 | ---- | ---- | ---- | 0.043 | 0.40 |
| 824 | 0.39 | 232.12 | 6.68 | 0.24 | ---- | ---- | 0.12 | ---- | ---- | ---- | 0.043 | 0.40 |
| 828 | 0.38 | 232.12 | 6.68 | 0.24 | ---- | ---- | 0.12 | ---- | ---- | ---- | 0.043 | 0.39 |
| 832 | 0.37 | 232.12 | 6.68 | 0.24 | ---- | ---- | 0.12 | ---- | ---- | ---- | 0.043 | 0.39 |
| 836 | 0.36 | 232.12 | 6.68 | 0.24 | ---- | ---- | 0.11 | ---- | ---- | ---- | 0.043 | 0.39 |
| 840 | 0.35 | 232.12 | 6.68 | 0.23 | ---- | ---- | 0.11 | ---- | ---- | ---- | 0.042 | 0.39 |
| 844 | 0.34 | 232.11 | 6.68 | 0.23 | ---- | ---- | 0.11 | ---- | ---- | ---- | 0.042 | 0.39 |
| 848 | 0.33 | 232.11 | 6.68 | 0.23 | ---- | ---- | 0.11 | ---- | ---- | ---- | 0.042 | 0.39 |
| 852 | 0.32 | 232.11 | 6.68 | 0.23 | ---- | ---- | 0.11 | ---- | ---- | ---- | 0.042 | 0.38 |
| 856 | 0.32 | 232.11 | 6.68 | 0.23 | ---- | ---- | 0.10 | ---- | ---- | ---- | 0.042 | 0.38 |
| 860 | 0.31 | 232.10 | 6.68 | 0.23 | ---- | ---- | 0.10 | ---- | ---- | ---- | 0.042 | 0.38 |
| 864 | 0.31 | 232.10 | 6.68 | 0.23 | ---- | ---- | 0.10 | ---- | ---- | ---- | 0.042 | 0.38 |
| 868 | 0.30 | 232.10 | 6.68 | 0.23 | ---- | ---- | 0.10 | ---- | ---- | ---- | 0.042 | 0.37 |
| 872 | 0.30 | 232.10 | 6.68 | 0.23 | ---- | ---- | 0.09 | ---- | ---- | ---- | 0.042 | 0.37 |
| 876 | 0.29 | 232.09 | 6.68 | 0.23 | ---- | ---- | 0.09 | ---- | ---- | ---- | 0.042 | 0.37 |
| 880 | 0.29 | 232.09 | 6.68 | 0.23 | ---- | ---- | 0.09 | ---- | ---- | ---- | 0.042 | 0.36 |

Continues on next page...

Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 884 | 0.28 | 232.09 | 6.68 | 0.23 | ---- | ---- | 0.09 | ---- | ---- | ---- | 0.042 | 0.36 |
| 888 | 0.28 | 232.08 | 6.68 | 0.23 | ---- | ---- | 0.08 | ---- | ---- | ---- | 0.042 | 0.36 |
| 892 | 0.27 | 232.08 | 6.68 | 0.23 | ---- | ---- | 0.08 | ---- | ---- | ---- | 0.042 | 0.35 |
| 896 | 0.27 | 232.08 | 6.68 | 0.23 | ---- | ---- | 0.08 | ---- | ---- | ---- | 0.042 | 0.35 |
| 900 | 0.26 | 232.07 | 6.68 | 0.23 | ---- | ---- | 0.07 | ---- | ---- | ---- | 0.042 | 0.35 |
| 904 | 0.26 | 232.07 | 6.68 | 0.23 | ---- | ---- | 0.07 | ---- | ---- | ---- | 0.042 | 0.34 |
| 908 | 0.25 | 232.07 | 6.68 | 0.23 | ---- | ---- | 0.07 | ---- | ---- | ---- | 0.042 | 0.34 |
| 912 | 0.25 | 232.06 | 6.68 | 0.23 | ---- | ---- | 0.06 | ---- | ---- | ---- | 0.042 | 0.33 |
| 916 | 0.24 | 232.06 | 6.68 | 0.23 | ---- | ---- | 0.06 | ---- | ---- | ---- | 0.042 | 0.33 |
| 920 | 0.24 | 232.06 | 6.68 | 0.23 | ---- | ---- | 0.06 | ---- | ---- | ---- | 0.042 | 0.33 |
| 924 | 0.23 | 232.05 | 6.68 | 0.23 | ---- | ---- | 0.05 | ---- | ---- | ---- | 0.042 | 0.32 |
| 928 | 0.23 | 232.05 | 6.68 | 0.23 | ---- | ---- | 0.05 | ---- | ---- | ---- | 0.042 | 0.32 |
| 932 | 0.22 | 232.05 | 6.68 | 0.23 | ---- | ---- | 0.05 | ---- | ---- | ---- | 0.042 | 0.31 |
| 936 | 0.22 | 232.04 | 6.68 | 0.23 | ---- | ---- | 0.04 | ---- | ---- | ---- | 0.042 | 0.31 |
| 940 | 0.21 | 232.04 | 6.68 | 0.23 | ---- | ---- | 0.04 | ---- | ---- | ---- | 0.042 | 0.31 |
| 944 | 0.21 | 232.04 | 6.68 | 0.23 | ---- | ---- | 0.04 | ---- | ---- | ---- | 0.042 | 0.30 |
| 948 | 0.20 | 232.03 | 6.68 | 0.22 | ---- | ---- | 0.03 | ---- | ---- | ---- | 0.042 | 0.30 |
| 952 | 0.20 | 232.03 | 6.68 | 0.22 | ---- | ---- | 0.03 | ---- | ---- | ---- | 0.042 | 0.29 |
| 956 | 0.19 | 232.02 | 6.68 | 0.22 | ---- | ---- | 0.02 | ---- | ---- | ---- | 0.042 | 0.29 |
| 960 | 0.19 | 232.02 | 6.68 | 0.22 | ---- | ---- | 0.02 | ---- | ---- | ---- | 0.042 | 0.29 |
| 964 | 0.18 | 232.02 | 6.68 | 0.22 | ---- | ---- | 0.02 | ---- | ---- | ---- | 0.042 | 0.28 |
| 968 | 0.18 | 232.01 | 6.68 | 0.22 | ---- | ---- | 0.01 | ---- | ---- | ---- | 0.042 | 0.28 |
| 972 | 0.17 | 232.01 | 6.68 | 0.22 | ---- | ---- | 0.01 | ---- | ---- | ---- | 0.042 | 0.27 |
| 976 | 0.17 | 232.01 | 6.68 | 0.22 | ---- | ---- | 0.00 | ---- | ---- | ---- | 0.042 | 0.27 |
| 980 | 0.17 | 232.00 | 6.68 | 0.22 | ---- | ---- | 0.00 | ---- | ---- | ---- | 0.042 | 0.26 |
| 984 | 0.17 | 232.00 | 6.68 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | 0.042 | 0.26 |
| 988 | 0.17 | 231.99 | 6.68 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | 0.042 | 0.26 |
| 992 | 0.16 | 231.98 | 6.68 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | 0.042 | 0.26 |
| 996 | 0.16 | 231.98 | 6.68 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | 0.042 | 0.26 |
| 1000 | 0.16 | 231.97 | 6.68 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | 0.042 | 0.26 |
| 1004 | 0.16 | 231.97 | 6.68 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | 0.042 | 0.26 |
| 1008 | 0.15 | 231.96 | 6.68 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | 0.042 | 0.26 |
| 1012 | 0.15 | 231.96 | 6.68 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | 0.042 | 0.26 |
| 1016 | 0.15 | 231.95 | 6.68 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | 0.042 | 0.26 |
| 1020 | 0.15 | 231.94 | 6.68 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | 0.041 | 0.25 |
| 1024 | 0.15 | 231.94 | 6.68 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | 0.041 | 0.25 |
| 1028 | 0.14 | 231.93 | 6.68 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | 0.041 | 0.25 |
| 1032 | 0.14 | 231.92 | 6.68 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | 0.041 | 0.25 |
| 1036 | 0.14 | 231.92 | 6.68 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | 0.041 | 0.25 |
| 1040 | 0.14 | 231.91 | 6.68 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | 0.041 | 0.25 |
| 1044 | 0.13 | 231.90 | 6.68 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | 0.041 | 0.25 |
| 1048 | 0.13 | 231.90 | 6.68 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | 0.041 | 0.25 |
| 1052 | 0.13 | 231.89 | 6.68 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | 0.041 | 0.25 |
| 1056 | 0.13 | 231.88 | 6.68 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | 0.041 | 0.25 |
| 1060 | 0.13 | 231.88 | 6.68 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | 0.041 | 0.24 |
| 1064 | 0.12 | 231.87 | 6.68 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | 0.041 | 0.24 |
| 1068 | 0.12 | 231.86 | 6.68 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | 0.040 | 0.24 |
| 1072 | 0.12 | 231.85 | 6.68 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | 0.040 | 0.24 |
| 1076 | 0.12 | 231.85 | 6.68 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | 0.040 | 0.24 |
| 1080 | 0.11 | 231.84 | 6.68 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | 0.040 | 0.24 |
| 1084 | 0.11 | 231.83 | 6.68 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | 0.040 | 0.24 |

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Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 1088 | 0.11 | 231.82 | 6.68 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | 0.040 | 0.24 |
| 1092 | 0.11 | 231.82 | 6.68 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | 0.040 | 0.24 |
| 1096 | 0.11 | 231.81 | 6.68 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | 0.040 | 0.24 |
| 1100 | 0.11 | 231.80 | 6.68 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | 0.040 | 0.23 |
| 1104 | 0.11 | 231.79 | 6.68 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | 0.040 | 0.23 |
| 1108 | 0.11 | 231.79 | 6.68 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | 0.040 | 0.23 |
| 1112 | 0.11 | 231.78 | 6.68 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | 0.040 | 0.23 |
| 1116 | 0.10 | 231.77 | 6.68 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | 0.039 | 0.23 |
| 1120 | 0.10 | 231.77 | 6.68 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | 0.039 | 0.23 |
| 1124 | 0.10 | 231.76 | 6.68 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | 0.039 | 0.23 |
| 1128 | 0.10 | 231.75 | 6.68 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | 0.039 | 0.23 |
| 1132 | 0.10 | 231.74 | 6.68 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | 0.039 | 0.22 |
| 1136 | 0.10 | 231.74 | 6.68 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | 0.039 | 0.22 |
| 1140 | 0.10 | 231.73 | 6.68 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | 0.039 | 0.22 |
| 1144 | 0.10 | 231.72 | 6.68 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | 0.039 | 0.22 |
| 1148 | 0.10 | 231.71 | 6.68 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | 0.039 | 0.22 |
| 1152 | 0.10 | 231.71 | 6.68 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | 0.039 | 0.22 |
| 1156 | 0.10 | 231.70 | 6.68 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | 0.039 | 0.22 |
| 1160 | 0.10 | 231.69 | 6.68 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | 0.038 | 0.22 |
| 1164 | 0.10 | 231.69 | 6.68 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | 0.038 | 0.21 |
| 1168 | 0.10 | 231.68 | 6.68 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | 0.038 | 0.21 |
| 1172 | 0.10 | 231.67 | 6.68 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | 0.038 | 0.21 |
| 1176 | 0.09 | 231.67 | 6.68 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | 0.038 | 0.21 |
| 1180 | 0.09 | 231.66 | 6.68 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | 0.038 | 0.21 |
| 1184 | 0.09 | 231.65 | 6.68 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | 0.038 | 0.21 |
| 1188 | 0.09 | 231.65 | 6.68 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | 0.038 | 0.21 |
| 1192 | 0.09 | 231.64 | 6.68 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | 0.038 | 0.21 |
| 1196 | 0.09 | 231.63 | 6.68 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | 0.038 | 0.21 |
| 1200 | 0.09 | 231.63 | 6.68 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | 0.038 | 0.20 |
| 1204 | 0.09 | 231.62 | 6.68 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | 0.038 | 0.20 |
| 1208 | 0.09 | 231.61 | 6.68 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | 0.037 | 0.20 |
| 1212 | 0.09 | 231.60 | 6.68 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | 0.037 | 0.20 |
| 1216 | 0.09 | 231.60 | 6.68 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | 0.037 | 0.20 |
| 1220 | 0.09 | 231.59 | 6.68 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | 0.037 | 0.20 |
| 1224 | 0.09 | 231.59 | 6.68 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | 0.037 | 0.20 |
| 1228 | 0.09 | 231.58 | 6.68 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | 0.037 | 0.20 |
| 1232 | 0.09 | 231.57 | 6.68 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | 0.037 | 0.19 |
| 1236 | 0.08 | 231.57 | 6.68 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | 0.037 | 0.19 |
| 1240 | 0.08 | 231.56 | 6.68 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | 0.037 | 0.19 |
| 1244 | 0.08 | 231.55 | 6.68 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | 0.037 | 0.19 |
| 1248 | 0.08 | 231.55 | 6.68 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | 0.037 | 0.19 |
| 1252 | 0.08 | 231.54 | 6.68 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | 0.037 | 0.19 |
| 1256 | 0.08 | 231.53 | 6.68 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | 0.037 | 0.19 |
| 1260 | 0.08 | 231.53 | 6.68 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | 0.036 | 0.19 |
| 1264 | 0.08 | 231.52 | 6.68 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | 0.036 | 0.18 |
| 1268 | 0.08 | 231.52 | 6.68 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | 0.036 | 0.18 |
| 1272 | 0.08 | 231.51 | 6.68 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | 0.036 | 0.18 |
| 1276 | 0.08 | 231.50 | 6.68 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | 0.036 | 0.18 |
| 1280 | 0.08 | 231.50 | 6.68 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | 0.036 | 0.18 |
| 1284 | 0.08 | 231.49 | 6.68 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | 0.036 | 0.18 |
| 1288 | 0.08 | 231.49 | 6.68 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | 0.036 | 0.18 |

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Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 1292 | 0.08 | 231.48 | 6.68 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | 0.036 | 0.18 |
| 1296 | 0.07 | 231.47 | 6.68 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | 0.036 | 0.17 |
| 1300 | 0.07 | 231.47 | 6.68 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | 0.036 | 0.17 |
| 1304 | 0.07 | 231.46 | 6.68 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | 0.036 | 0.17 |
| 1308 | 0.07 | 231.46 | 6.68 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | 0.036 | 0.17 |
| 1312 | 0.07 | 231.45 | 6.68 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | 0.036 | 0.17 |
| 1316 | 0.07 | 231.44 | 6.68 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | 0.035 | 0.17 |
| 1320 | 0.07 | 231.44 | 6.68 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | 0.035 | 0.17 |
| 1324 | 0.08 | 231.43 | 6.68 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | 0.035 | 0.17 |
| 1328 | 0.09 | 231.43 | 6.68 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | 0.035 | 0.16 |
| 1332 | 0.09 | 231.43 | 6.68 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | 0.035 | 0.16 |
| 1336 | 0.09 | 231.42 | 6.68 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | 0.035 | 0.16 |
| 1340 | 0.08 | 231.42 | 6.68 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | 0.035 | 0.16 |
| 1344 | 0.07 | 231.41 | 6.68 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | 0.035 | 0.16 |
| 1348 | 0.07 | 231.41 | 6.68 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | 0.035 | 0.16 |
| 1352 | 0.07 | 231.40 | 6.68 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | 0.035 | 0.16 |
| 1356 | 0.07 | 231.40 | 6.68 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | 0.035 | 0.16 |
| 1360 | 0.07 | 231.39 | 6.68 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | 0.035 | 0.16 |
| 1364 | 0.07 | 231.39 | 6.68 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | 0.035 | 0.15 |
| 1368 | 0.07 | 231.38 | 6.68 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | 0.035 | 0.15 |
| 1372 | 0.07 | 231.38 | 6.68 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | 0.035 | 0.15 |
| 1376 | 0.07 | 231.37 | 6.68 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | 0.035 | 0.15 |
| 1380 | 0.07 | 231.37 | 6.68 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | 0.035 | 0.15 |
| 1384 | 0.07 | 231.36 | 6.68 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | 0.034 | 0.15 |
| 1388 | 0.07 | 231.36 | 6.68 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | 0.034 | 0.15 |
| 1392 | 0.07 | 231.35 | 6.68 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | 0.034 | 0.14 |
| 1396 | 0.07 | 231.35 | 6.68 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | 0.034 | 0.14 |
| 1400 | 0.07 | 231.34 | 6.68 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | 0.034 | 0.14 |
| 1404 | 0.06 | 231.34 | 6.68 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | 0.034 | 0.14 |
| 1408 | 0.06 | 231.33 | 6.68 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | 0.034 | 0.14 |
| 1412 | 0.06 | 231.33 | 6.68 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | 0.034 | 0.14 |
| 1416 | 0.06 | 231.33 | 6.68 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | 0.034 | 0.14 |
| 1420 | 0.06 | 231.32 | 6.68 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | 0.034 | 0.13 |
| 1424 | 0.06 | 231.32 | 6.68 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | 0.034 | 0.13 |
| 1428 | 0.06 | 231.31 | 6.68 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | 0.034 | 0.13 |
| 1432 | 0.06 | 231.31 | 6.68 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | 0.034 | 0.13 |
| 1436 | 0.06 | 231.30 | 6.68 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | 0.034 | 0.13 |
| 1440 | 0.06 | 231.30 | 6.68 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | 0.034 | 0.13 |
| 1444 | 0.05 | 231.30 | 6.68 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | 0.034 | 0.13 |
| 1448 | 0.04 | 231.29 | 6.68 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | 0.034 | 0.13 |
| 1452 | 0.02 | 231.29 | 6.68 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | 0.034 | 0.12 |
| 1456 | 0.01 | 231.28 | 6.68 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | 0.034 | 0.12 |
| 1460 | 0.00 | 231.27 | 6.68 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | 0.033 | 0.12 |
| 1464 | 0.00 | 231.27 | 6.68 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | 0.033 | 0.12 |
| 1468 | 0.00 | 231.26 | 6.68 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | 0.033 | 0.12 |
| 1472 | 0.00 | 231.25 | 6.68 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | 0.033 | 0.11 |
| 1476 | 0.00 | 231.25 | 6.68 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | 0.033 | 0.11 |
| 1480 | 0.00 | 231.24 | 6.68 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | 0.033 | 0.11 |
| 1484 | 0.00 | 231.23 | 6.68 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | 0.033 | 0.11 |
| 1488 | 0.00 | 231.23 | 6.68 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | 0.033 | 0.11 |
| 1492 | 0.00 | 231.22 | 6.68 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | 0.033 | 0.10 |

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Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 1496 | 0.00 | 231.21 | 6.68 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | 0.033 | 0.10 |
| 1500 | 0.00 | 231.21 | 6.68 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | 0.033 | 0.10 |
| 1504 | 0.00 | 231.20 | 6.68 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | 0.033 | 0.10 |
| 1508 | 0.00 | 231.20 | 6.68 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | 0.033 | 0.10 |
| 1512 | 0.00 | 231.19 | 6.68 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | 0.032 | 0.09 |
| 1516 | 0.00 | 231.19 | 6.68 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | 0.032 | 0.09 |
| 1520 | 0.00 | 231.18 | 6.68 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | 0.032 | 0.09 |
| 1524 | 0.00 | 231.17 | 6.68 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | 0.032 | 0.09 |
| 1528 | 0.00 | 231.17 | 6.68 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | 0.032 | 0.09 |
| 1532 | 0.00 | 231.16 | 6.68 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | 0.032 | 0.09 |
| 1536 | 0.00 | 231.16 | 6.68 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | 0.032 | 0.08 |
| 1540 | 0.00 | 231.15 | 6.68 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | 0.032 | 0.08 |
| 1544 | 0.00 | 231.15 | 6.68 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | 0.032 | 0.08 |
| 1548 | 0.00 | 231.15 | 6.68 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | 0.032 | 0.08 |
| 1552 | 0.00 | 231.14 | 6.68 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | 0.032 | 0.08 |
| 1556 | 0.00 | 231.14 | 6.68 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | 0.032 | 0.08 |
| 1560 | 0.00 | 231.13 | 6.68 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | 0.032 | 0.07 |
| 1564 | 0.00 | 231.13 | 6.68 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | 0.032 | 0.07 |
| 1568 | 0.00 | 231.12 | 6.68 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | 0.032 | 0.07 |
| 1572 | 0.00 | 231.12 | 6.68 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | 0.032 | 0.07 |
| 1576 | 0.00 | 231.11 | 6.68 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | 0.032 | 0.07 |
| 1580 | 0.00 | 231.11 | 6.68 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | 0.031 | 0.07 |
| 1584 | 0.00 | 231.11 | 6.68 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | 0.031 | 0.07 |
| 1588 | 0.00 | 231.10 | 6.68 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | 0.031 | 0.06 |
| 1592 | 0.00 | 231.10 | 6.68 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | 0.031 | 0.06 |
| 1596 | 0.00 | 231.10 | 6.68 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | 0.031 | 0.06 |
| 1600 | 0.00 | 231.09 | 6.68 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | 0.031 | 0.06 |
| 1604 | 0.00 | 231.09 | 6.68 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | 0.031 | 0.06 |
| 1608 | 0.00 | 231.08 | 6.68 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | 0.031 | 0.06 |
| 1612 | 0.00 | 231.08 | 6.68 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | 0.031 | 0.06 |
| 1616 | 0.00 | 231.08 | 6.68 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | 0.031 | 0.06 |
| 1620 | 0.00 | 231.07 | 6.68 | 0.02 | ---- | ---- | ---- | ---- | ---- | ---- | 0.031 | 0.06 |
| 1624 | 0.00 | 231.07 | 6.68 | 0.02 | ---- | ---- | ---- | ---- | ---- | ---- | 0.031 | 0.05 |
| 1628 | 0.00 | 231.07 | 6.68 | 0.02 | ---- | ---- | ---- | ---- | ---- | ---- | 0.031 | 0.05 |
| 1632 | 0.00 | 231.07 | 6.68 | 0.02 | ---- | ---- | ---- | ---- | ---- | ---- | 0.031 | 0.05 |
| 1636 | 0.00 | 231.06 | 6.68 | 0.02 | ---- | ---- | ---- | ---- | ---- | ---- | 0.031 | 0.05 |
| 1640 | 0.00 | 231.06 | 6.68 | 0.02 | ---- | ---- | ---- | ---- | ---- | ---- | 0.031 | 0.05 |
| 1644 | 0.00 | 231.06 | 6.68 | 0.02 | ---- | ---- | ---- | ---- | ---- | ---- | 0.031 | 0.05 |
| 1648 | 0.00 | 231.05 | 6.68 | 0.02 | ---- | ---- | ---- | ---- | ---- | ---- | 0.031 | 0.05 |
| 1652 | 0.00 | 231.05 | 6.68 | 0.02 | ---- | ---- | ---- | ---- | ---- | ---- | 0.031 | 0.05 |
| 1656 | 0.00 | 231.05 | 6.68 | 0.02 | ---- | ---- | ---- | ---- | ---- | ---- | 0.031 | 0.05 |
| 1660 | 0.00 | 231.05 | 6.68 | 0.01 | ---- | ---- | ---- | ---- | ---- | ---- | 0.031 | 0.05 |
| 1664 | 0.00 | 231.04 | 6.68 | 0.01 | ---- | ---- | ---- | ---- | ---- | ---- | 0.031 | 0.04 |
| 1668 | 0.00 | 231.04 | 6.68 | 0.01 | ---- | ---- | ---- | ---- | ---- | ---- | 0.031 | 0.04 |
| 1672 | 0.00 | 231.04 | 6.68 | 0.01 | ---- | ---- | ---- | ---- | ---- | ---- | 0.031 | 0.04 |
| 1676 | 0.00 | 231.03 | 6.68 | 0.01 | ---- | ---- | ---- | ---- | ---- | ---- | 0.031 | 0.04 |
| 1680 | 0.00 | 231.03 | 6.68 | 0.01 | ---- | ---- | ---- | ---- | ---- | ---- | 0.031 | 0.04 |
| 1684 | 0.00 | 231.03 | 6.68 | 0.01 | ---- | ---- | ---- | ---- | ---- | ---- | 0.031 | 0.04 |

...End

Reservoir Report

Reservoir No. 2 - Detention Basin 2

Hydraflow Hydrographs by Intelisolve

Pond Data

Pond storage is based on known contour areas. Average end area method used.

Stage / Storage Table

| Stage (ft) | Elevation (ft) | Contour area (sqft) | Incr. Storage (cuft) | Total storage (cuft) |
|------------|----------------|---------------------|----------------------|----------------------|
| 0.00 | 229.33 | 00 | 0 | 0 |
| 0.67 | 230.00 | 2,454 | 822 | 822 |
| 2.67 | 232.00 | 5,689 | 8,143 | 8,965 |
| 4.67 | 234.00 | 6,522 | 12,211 | 21,176 |
| 6.67 | 236.00 | 7,413 | 13,935 | 35,111 |
| 8.67 | 238.00 | 9,192 | 16,605 | 51,716 |

Culvert / Orifice Structures

| | [A] | [B] | [C] | [D] |
|---------------|----------|--------|------|------|
| Rise in | = 6.0 | 3.0 | 0.0 | 0.0 |
| Span in | = 6.0 | 3.0 | 0.0 | 0.0 |
| No. Barrels | = 10 | 1 | 0 | 0 |
| Invert El. ft | = 228.40 | 231.00 | 0.00 | 0.00 |
| Length ft | = 40.0 | 1.0 | 0.0 | 0.0 |
| Slope % | = 1.00 | 0.00 | 0.00 | 0.00 |
| N-Value | = .013 | .013 | .000 | .000 |
| Orif. Coeff. | = 0.60 | 0.60 | 0.00 | 0.00 |
| Multi-Stage | = n/a | Yes | No | No |

Weir Structures

| | [A] | [B] | [C] | [D] |
|--------------|----------|--------|--------|------|
| Crest Len ft | = 0.66 | 20.00 | 16.00 | 0.00 |
| Crest El. ft | = 232.00 | 236.00 | 235.50 | 0.00 |
| Weir Coeff. | = 3.33 | 2.60 | 3.33 | 0.00 |
| Weir Type | = Rect | Broad | Rect | --- |
| Multi-Stage | = Yes | No | Yes | No |

Exfiltration Rate = 0.32 in/hr/sqft Tailwater Elev. = 0.00 ft

Stage / Storage / Discharge Table

Note: All outflows have been analyzed under inlet and outlet control.

| Stage ft | Storage cuft | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Total cfs |
|----------|--------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-----------|
| 0.00 | 0 | 229.33 | 0.00 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.000 | 0.00 |
| 0.07 | 82 | 229.40 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.002 | 0.00 |
| 0.13 | 164 | 229.46 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.004 | 0.00 |
| 0.20 | 247 | 229.53 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.005 | 0.01 |
| 0.27 | 329 | 229.60 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.007 | 0.01 |
| 0.34 | 411 | 229.67 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.009 | 0.01 |
| 0.40 | 493 | 229.73 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.011 | 0.01 |
| 0.47 | 575 | 229.80 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.013 | 0.01 |
| 0.54 | 658 | 229.87 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.015 | 0.01 |
| 0.60 | 740 | 229.93 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.016 | 0.02 |
| 0.67 | 822 | 230.00 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.018 | 0.02 |
| 0.87 | 1,636 | 230.20 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.021 | 0.02 |
| 1.07 | 2,451 | 230.40 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.023 | 0.02 |
| 1.27 | 3,265 | 230.60 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.025 | 0.03 |
| 1.47 | 4,079 | 230.80 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.028 | 0.03 |
| 1.67 | 4,894 | 231.00 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.030 | 0.03 |
| 1.87 | 5,708 | 231.20 | 6.68 | 0.06 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.033 | 0.10 |
| 2.07 | 6,522 | 231.40 | 6.68 | 0.12 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.035 | 0.16 |
| 2.27 | 7,336 | 231.60 | 6.68 | 0.16 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.037 | 0.20 |
| 2.47 | 8,151 | 231.80 | 6.68 | 0.19 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.040 | 0.23 |
| 2.67 | 8,965 | 232.00 | 6.68 | 0.22 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.042 | 0.26 |
| 2.87 | 10,186 | 232.20 | 6.68 | 0.25 | --- | --- | 0.20 | 0.00 | 0.00 | --- | 0.043 | 0.48 |
| 3.07 | 11,407 | 232.40 | 6.68 | 0.27 | --- | --- | 0.56 | 0.00 | 0.00 | --- | 0.043 | 0.87 |
| 3.27 | 12,628 | 232.60 | 6.68 | 0.29 | --- | --- | 1.02 | 0.00 | 0.00 | --- | 0.044 | 1.35 |
| 3.47 | 13,849 | 232.80 | 6.68 | 0.31 | --- | --- | 1.57 | 0.00 | 0.00 | --- | 0.045 | 1.92 |
| 3.67 | 15,071 | 233.00 | 6.68 | 0.32 | --- | --- | 2.20 | 0.00 | 0.00 | --- | 0.045 | 2.57 |
| 3.87 | 16,292 | 233.20 | 6.68 | 0.34 | --- | --- | 2.89 | 0.00 | 0.00 | --- | 0.046 | 3.28 |
| 4.07 | 17,513 | 233.40 | 6.68 | 0.36 | --- | --- | 3.64 | 0.00 | 0.00 | --- | 0.046 | 4.04 |
| 4.27 | 18,734 | 233.60 | 6.68 | 0.37 | --- | --- | 4.45 | 0.00 | 0.00 | --- | 0.047 | 4.87 |
| 4.47 | 19,955 | 233.80 | 6.68 | 0.39 | --- | --- | 5.31 | 0.00 | 0.00 | --- | 0.048 | 5.74 |
| 4.67 | 21,176 | 234.00 | 6.68 | 0.40 | --- | --- | 6.22 | 0.00 | 0.00 | --- | 0.048 | 6.67 |
| 4.87 | 22,570 | 234.20 | 7.59 | 0.41 | --- | --- | 7.17 | 0.00 | 0.00 | --- | 0.049 | 7.64 |

Continues on next page...

Detention Basin 2
Stage / Storage / Discharge Table

| Stage ft | Storage cuft | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Total cfs |
|-------------|-----------------|-----------------|--------------|--------------|--------------|--------------|-------------|-------------|-------------|-------------|--------------|--------------|
| 5.07 | 23,963 | 234.40 | 8.60 | 0.43 | --- | --- | 8.17 | 0.00 | 0.00 | --- | 0.050 | 8.65 |
| 5.27 | 25,357 | 234.60 | 9.65 | 0.44 | --- | --- | 9.21 | 0.00 | 0.00 | --- | 0.050 | 9.70 |
| 5.47 | 26,750 | 234.80 | 10.75 | 0.45 | --- | --- | 10.30 | 0.00 | 0.00 | --- | 0.051 | 10.80 |
| 5.67 | 28,144 | 235.00 | 11.89 | 0.47 | --- | --- | 11.42 | 0.00 | 0.00 | --- | 0.052 | 11.94 |
| 5.87 | 29,537 | 235.20 | 13.03 | 0.44 | --- | --- | 12.58 | 0.00 | 0.00 | --- | 0.052 | 13.08 |
| 6.07 | 30,931 | 235.40 | 14.12 | 0.42 | --- | --- | 13.70 | 0.00 | 0.00 | --- | 0.053 | 14.17 |
| 6.27 | 32,324 | 235.60 | 15.89 | 0.37 | --- | --- | 13.84 | 0.00 | 1.68 | --- | 0.054 | 15.94 |
| 6.47 | 33,718 | 235.80 | 18.81 | 0.20 | --- | --- | 9.85 | 0.00 | 8.75 | --- | 0.054 | 18.86 |
| 6.67 | 35,111 | 236.00 | 19.86 | 0.10 | --- | --- | 5.97 | 0.00 | 13.80 | --- | 0.055 | 19.92 |
| 6.87 | 36,772 | 236.20 | 20.25 | 0.07 | --- | --- | 4.74 | 4.65 | 15.44 | --- | 0.056 | 24.95 |
| 7.07 | 38,432 | 236.40 | 20.56 | 0.05 | --- | --- | 4.01 | 13.15 | 16.50 | --- | 0.058 | 33.77 |
| 7.27 | 40,093 | 236.60 | 20.84 | 0.04 | --- | --- | 3.52 | 24.17 | 17.27 | --- | 0.059 | 45.05 |
| 7.47 | 41,753 | 236.80 | 21.10 | 0.03 | --- | --- | 3.17 | 37.21 | 17.88 | --- | 0.060 | 58.35 |
| 7.67 | 43,414 | 237.00 | 21.36 | 0.03 | --- | --- | 2.91 | 52.00 | 18.41 | --- | 0.061 | 73.40 |
| 7.87 | 45,074 | 237.20 | 21.62 | 0.02 | --- | --- | 2.71 | 68.35 | 18.85 | --- | 0.063 | 90.00 |
| 8.07 | 46,735 | 237.40 | 21.87 | 0.02 | --- | --- | 2.54 | 86.14 | 19.22 | --- | 0.064 | 107.99 |
| 8.27 | 48,395 | 237.60 | 22.12 | 0.02 | --- | --- | 2.41 | 105.24 | 19.56 | --- | 0.065 | 127.29 |
| 8.47 | 50,056 | 237.80 | 22.36 | 0.02 | --- | --- | 2.31 | 125.57 | 19.95 | --- | 0.067 | 147.91 |
| 8.67 | 51,716 | 238.00 | 22.60 | 0.01 | --- | --- | 2.21 | 147.08 | 20.20 | --- | 0.068 | 169.58 |

...End

Hydrograph Report

Hyd. No. 13

Basin 3 Out

| | | | |
|-----------------|-------------|----------------|-------------------|
| Hydrograph type | = Reservoir | Peak discharge | = 0.45 cfs |
| Storm frequency | = 2 yrs | Time interval | = 2 min |
| Inflow hyd. No. | = 10 | Reservoir name | = Basin 3 (Hotel) |
| Max. Elevation | = 222.57 ft | Max. Storage | = 9,939 cuft |

Storage Indication method used.

Outflow hydrograph volume = 20,626 cuft

Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 564 | 0.06 | 219.06 | 6.83 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 568 | 0.07 | 219.07 | 7.39 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 572 | 0.07 | 219.07 | 7.97 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |
| 576 | 0.08 | 219.08 | 8.57 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |
| 580 | 0.08 | 219.09 | 9.19 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |
| 584 | 0.09 | 219.09 | 9.83 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 588 | 0.09 | 219.10 | 10.48 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 592 | 0.10 | 219.10 | 10.70 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 596 | 0.10 | 219.11 | 10.70 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 600 | 0.11 | 219.12 | 10.70 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 604 | 0.11 | 219.13 | 10.70 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 608 | 0.12 | 219.14 | 10.70 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 612 | 0.13 | 219.15 | 10.70 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 616 | 0.14 | 219.17 | 10.70 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 620 | 0.15 | 219.18 | 10.70 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 624 | 0.15 | 219.20 | 10.70 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 628 | 0.16 | 219.21 | 10.70 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.11 |
| 632 | 0.17 | 219.23 | 10.70 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.11 |
| 636 | 0.18 | 219.26 | 10.70 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.12 |
| 640 | 0.19 | 219.28 | 10.70 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.12 |
| 644 | 0.20 | 219.30 | 10.70 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 648 | 0.22 | 219.33 | 10.70 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 652 | 0.23 | 219.36 | 10.70 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 656 | 0.24 | 219.39 | 10.70 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 660 | 0.25 | 219.42 | 10.70 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 664 | 0.26 | 219.45 | 10.70 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |
| 668 | 0.29 | 219.49 | 10.70 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 672 | 0.31 | 219.54 | 10.70 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 676 | 0.35 | 219.59 | 10.70 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 680 | 0.38 | 219.65 | 10.70 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 684 | 0.42 | 219.72 | 10.70 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 688 | 0.45 | 219.80 | 10.70 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 692 | 0.50 | 219.88 | 10.70 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 696 | 0.61 | 219.99 | 10.70 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 700 | 0.83 | 220.03 | 10.70 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 704 | 1.13 | 220.09 | 10.70 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 708 | 1.48 | 220.17 | 10.70 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 712 | 1.87 | 220.28 | 10.70 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |

Continues on next page...

Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 716 | 2.37 | 220.43 | 10.70 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 720 | 3.63 | 220.63 | 10.70 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 724 | 5.58 | 220.96 | 10.70 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 728 | 5.81 | 221.39 | 10.70 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 732 | 4.51 | 221.77 | 10.70 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 736 | 3.33 | 222.02 | 10.70 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.41 |
| 740 | 2.75 | 222.14 | 10.70 | 0.42 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.42 |
| 744 | 2.34 | 222.23 | 10.70 | 0.42 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.42 |
| 748 | 1.90 | 222.31 | 10.70 | 0.43 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.43 |
| 752 | 1.46 | 222.36 | 10.70 | 0.43 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.43 |
| 756 | 1.11 | 222.40 | 10.70 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.44 |
| 760 | 0.94 | 222.43 | 10.70 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.44 |
| 764 | 0.87 | 222.45 | 10.70 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.44 |
| 768 | 0.82 | 222.47 | 10.70 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.44 |
| 772 | 0.78 | 222.48 | 10.70 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.44 |
| 776 | 0.73 | 222.50 | 10.70 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.44 |
| 780 | 0.68 | 222.51 | 10.70 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.44 |
| 784 | 0.64 | 222.52 | 10.70 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.44 |
| 788 | 0.61 | 222.52 | 10.70 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.44 |
| 792 | 0.59 | 222.53 | 10.70 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.44 |
| 796 | 0.58 | 222.54 | 10.70 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.44 |
| 800 | 0.56 | 222.54 | 10.70 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.44 |
| 804 | 0.55 | 222.55 | 10.70 | 0.45 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.45 |
| 808 | 0.54 | 222.55 | 10.70 | 0.45 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.45 |
| 812 | 0.53 | 222.56 | 10.70 | 0.45 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.45 |
| 816 | 0.51 | 222.56 | 10.70 | 0.45 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.45 |
| 820 | 0.50 | 222.56 | 10.70 | 0.45 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.45 |
| 824 | 0.49 | 222.57 | 10.70 | 0.45 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.45 |
| 828 | 0.48 | 222.57 | 10.70 | 0.45 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.45 |
| 832 | 0.46 | 222.57 | 10.70 | 0.45 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.45 |
| 836 | 0.45 | 222.57 | 10.70 | 0.45 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.45 |
| 840 | 0.44 | 222.57 | 10.70 | 0.45 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.45 |
| 844 | 0.43 | 222.57 | 10.70 | 0.45 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.45 |
| 848 | 0.42 | 222.57 | 10.70 | 0.45 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.45 |
| 852 | 0.41 | 222.56 | 10.70 | 0.45 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.45 |
| 856 | 0.40 | 222.56 | 10.70 | 0.45 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.45 |
| 860 | 0.40 | 222.56 | 10.70 | 0.45 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.45 |
| 864 | 0.39 | 222.56 | 10.70 | 0.45 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.45 |
| 868 | 0.38 | 222.56 | 10.70 | 0.45 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.45 |
| 872 | 0.38 | 222.55 | 10.70 | 0.45 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.45 |
| 876 | 0.37 | 222.55 | 10.70 | 0.45 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.45 |
| 880 | 0.37 | 222.55 | 10.70 | 0.45 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.45 |
| 884 | 0.36 | 222.54 | 10.70 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.44 |
| 888 | 0.35 | 222.54 | 10.70 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.44 |
| 892 | 0.35 | 222.54 | 10.70 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.44 |
| 896 | 0.34 | 222.53 | 10.70 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.44 |
| 900 | 0.34 | 222.53 | 10.70 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.44 |
| 904 | 0.33 | 222.52 | 10.70 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.44 |
| 908 | 0.32 | 222.52 | 10.70 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.44 |
| 912 | 0.32 | 222.51 | 10.70 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.44 |
| 916 | 0.31 | 222.50 | 10.70 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.44 |

Continues on next page...

Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 920 | 0.30 | 222.50 | 10.70 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.44 |
| 924 | 0.30 | 222.49 | 10.70 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.44 |
| 928 | 0.29 | 222.49 | 10.70 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.44 |
| 932 | 0.28 | 222.48 | 10.70 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.44 |
| 936 | 0.28 | 222.47 | 10.70 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.44 |
| 940 | 0.27 | 222.46 | 10.70 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.44 |
| 944 | 0.26 | 222.46 | 10.70 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.44 |
| 948 | 0.26 | 222.45 | 10.70 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.44 |
| 952 | 0.25 | 222.44 | 10.70 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.44 |
| 956 | 0.25 | 222.43 | 10.70 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.44 |
| 960 | 0.24 | 222.42 | 10.70 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.44 |
| 964 | 0.23 | 222.41 | 10.70 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.44 |
| 968 | 0.23 | 222.40 | 10.70 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.44 |
| 972 | 0.22 | 222.40 | 10.70 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.44 |
| 976 | 0.22 | 222.39 | 10.70 | 0.43 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.43 |
| 980 | 0.22 | 222.38 | 10.70 | 0.43 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.43 |
| 984 | 0.22 | 222.37 | 10.70 | 0.43 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.43 |
| 988 | 0.21 | 222.36 | 10.70 | 0.43 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.43 |
| 992 | 0.21 | 222.35 | 10.70 | 0.43 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.43 |
| 996 | 0.21 | 222.34 | 10.70 | 0.43 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.43 |
| 1000 | 0.20 | 222.33 | 10.70 | 0.43 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.43 |
| 1004 | 0.20 | 222.32 | 10.70 | 0.43 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.43 |
| 1008 | 0.20 | 222.31 | 10.70 | 0.43 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.43 |
| 1012 | 0.20 | 222.30 | 10.70 | 0.43 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.43 |
| 1016 | 0.19 | 222.29 | 10.70 | 0.43 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.43 |
| 1020 | 0.19 | 222.28 | 10.70 | 0.43 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.43 |
| 1024 | 0.19 | 222.26 | 10.70 | 0.43 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.43 |
| 1028 | 0.18 | 222.25 | 10.70 | 0.43 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.43 |
| 1032 | 0.18 | 222.24 | 10.70 | 0.43 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.43 |
| 1036 | 0.18 | 222.23 | 10.70 | 0.42 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.42 |
| 1040 | 0.18 | 222.22 | 10.70 | 0.42 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.42 |
| 1044 | 0.17 | 222.21 | 10.70 | 0.42 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.42 |
| 1048 | 0.17 | 222.20 | 10.70 | 0.42 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.42 |
| 1052 | 0.17 | 222.19 | 10.70 | 0.42 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.42 |
| 1056 | 0.16 | 222.18 | 10.70 | 0.42 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.42 |
| 1060 | 0.16 | 222.16 | 10.70 | 0.42 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.42 |
| 1064 | 0.16 | 222.15 | 10.70 | 0.42 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.42 |
| 1068 | 0.16 | 222.14 | 10.70 | 0.42 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.42 |
| 1072 | 0.15 | 222.13 | 10.70 | 0.42 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.42 |
| 1076 | 0.15 | 222.12 | 10.70 | 0.42 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.42 |
| 1080 | 0.15 | 222.11 | 10.70 | 0.42 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.42 |
| 1084 | 0.14 | 222.09 | 10.70 | 0.42 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.42 |
| 1088 | 0.14 | 222.08 | 10.70 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.41 |
| 1092 | 0.14 | 222.07 | 10.70 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.41 |
| 1096 | 0.14 | 222.06 | 10.70 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.41 |
| 1100 | 0.14 | 222.04 | 10.70 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.41 |
| 1104 | 0.14 | 222.03 | 10.70 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.41 |
| 1108 | 0.14 | 222.02 | 10.70 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.41 |
| 1112 | 0.14 | 222.01 | 10.70 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.41 |
| 1116 | 0.14 | 221.99 | 10.70 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.41 |
| 1120 | 0.14 | 221.97 | 10.70 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.41 |

Continues on next page...

Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 1124 | 0.13 | 221.95 | 10.70 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.41 |
| 1128 | 0.13 | 221.93 | 10.70 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 1132 | 0.13 | 221.91 | 10.70 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 1136 | 0.13 | 221.89 | 10.70 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 1140 | 0.13 | 221.87 | 10.70 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 1144 | 0.13 | 221.85 | 10.70 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 1148 | 0.13 | 221.83 | 10.70 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 1152 | 0.13 | 221.80 | 10.70 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 1156 | 0.13 | 221.78 | 10.70 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1160 | 0.13 | 221.76 | 10.70 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1164 | 0.13 | 221.74 | 10.70 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1168 | 0.13 | 221.72 | 10.70 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1172 | 0.12 | 221.70 | 10.70 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1176 | 0.12 | 221.68 | 10.70 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1180 | 0.12 | 221.66 | 10.70 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1184 | 0.12 | 221.64 | 10.70 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1188 | 0.12 | 221.62 | 10.70 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1192 | 0.12 | 221.60 | 10.70 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1196 | 0.12 | 221.58 | 10.70 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1200 | 0.12 | 221.56 | 10.70 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1204 | 0.12 | 221.54 | 10.70 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1208 | 0.12 | 221.52 | 10.70 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1212 | 0.12 | 221.50 | 10.70 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1216 | 0.11 | 221.48 | 10.70 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1220 | 0.11 | 221.46 | 10.70 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1224 | 0.11 | 221.44 | 10.70 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1228 | 0.11 | 221.42 | 10.70 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1232 | 0.11 | 221.40 | 10.70 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1236 | 0.11 | 221.38 | 10.70 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1240 | 0.11 | 221.36 | 10.70 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1244 | 0.11 | 221.34 | 10.70 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1248 | 0.11 | 221.32 | 10.70 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1252 | 0.11 | 221.30 | 10.70 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1256 | 0.11 | 221.28 | 10.70 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1260 | 0.11 | 221.26 | 10.70 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1264 | 0.10 | 221.24 | 10.70 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1268 | 0.10 | 221.22 | 10.70 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1272 | 0.10 | 221.20 | 10.70 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1276 | 0.10 | 221.19 | 10.70 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1280 | 0.10 | 221.17 | 10.70 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1284 | 0.10 | 221.15 | 10.70 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1288 | 0.10 | 221.13 | 10.70 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1292 | 0.10 | 221.11 | 10.70 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1296 | 0.10 | 221.09 | 10.70 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1300 | 0.10 | 221.07 | 10.70 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1304 | 0.10 | 221.05 | 10.70 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1308 | 0.09 | 221.03 | 10.70 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1312 | 0.09 | 221.01 | 10.70 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1316 | 0.09 | 221.00 | 10.70 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1320 | 0.09 | 220.98 | 10.70 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1324 | 0.13 | 220.96 | 10.70 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |

Continues on next page...

Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 1328 | 0.14 | 220.94 | 10.70 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1332 | 0.12 | 220.93 | 10.70 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1336 | 0.10 | 220.91 | 10.70 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1340 | 0.10 | 220.89 | 10.70 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1344 | 0.09 | 220.88 | 10.70 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1348 | 0.09 | 220.86 | 10.70 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1352 | 0.09 | 220.84 | 10.70 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1356 | 0.09 | 220.82 | 10.70 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1360 | 0.09 | 220.81 | 10.70 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1364 | 0.09 | 220.79 | 10.70 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1368 | 0.09 | 220.77 | 10.70 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1372 | 0.09 | 220.75 | 10.70 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1376 | 0.09 | 220.74 | 10.70 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1380 | 0.09 | 220.72 | 10.70 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1384 | 0.09 | 220.70 | 10.70 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1388 | 0.09 | 220.68 | 10.70 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1392 | 0.09 | 220.67 | 10.70 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1396 | 0.09 | 220.65 | 10.70 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1400 | 0.09 | 220.63 | 10.70 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1404 | 0.08 | 220.62 | 10.70 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1408 | 0.08 | 220.60 | 10.70 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1412 | 0.08 | 220.58 | 10.70 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1416 | 0.08 | 220.57 | 10.70 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1420 | 0.08 | 220.55 | 10.70 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1424 | 0.08 | 220.53 | 10.70 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1428 | 0.08 | 220.52 | 10.70 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1432 | 0.08 | 220.50 | 10.70 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1436 | 0.08 | 220.48 | 10.70 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1440 | 0.08 | 220.47 | 10.70 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1444 | 0.06 | 220.45 | 10.70 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 1448 | 0.02 | 220.43 | 10.70 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 1452 | 0.00 | 220.41 | 10.70 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 1456 | 0.00 | 220.39 | 10.70 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 1460 | 0.00 | 220.37 | 10.70 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 1464 | 0.00 | 220.35 | 10.70 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 1468 | 0.00 | 220.33 | 10.70 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 1472 | 0.00 | 220.31 | 10.70 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 1476 | 0.00 | 220.28 | 10.70 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 1480 | 0.00 | 220.26 | 10.70 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 1484 | 0.00 | 220.24 | 10.70 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 1488 | 0.00 | 220.22 | 10.70 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 1492 | 0.00 | 220.20 | 10.70 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 1496 | 0.00 | 220.18 | 10.70 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 1500 | 0.00 | 220.16 | 10.70 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 1504 | 0.00 | 220.14 | 10.70 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 1508 | 0.00 | 220.12 | 10.70 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 1512 | 0.00 | 220.10 | 10.70 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 1516 | 0.00 | 220.08 | 10.70 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 1520 | 0.00 | 220.07 | 10.70 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 1524 | 0.00 | 220.05 | 10.70 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 1528 | 0.00 | 220.03 | 10.70 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |

Continues on next page...

Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 1532 | 0.00 | 220.01 | 10.70 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 1536 | 0.00 | 219.96 | 10.70 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 1540 | 0.00 | 219.89 | 10.70 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 1544 | 0.00 | 219.81 | 10.70 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 1548 | 0.00 | 219.74 | 10.70 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 1552 | 0.00 | 219.67 | 10.70 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 1556 | 0.00 | 219.61 | 10.70 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 1560 | 0.00 | 219.55 | 10.70 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 1564 | 0.00 | 219.49 | 10.70 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 1568 | 0.00 | 219.43 | 10.70 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |
| 1572 | 0.00 | 219.38 | 10.70 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 1576 | 0.00 | 219.33 | 10.70 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 1580 | 0.00 | 219.29 | 10.70 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 1584 | 0.00 | 219.25 | 10.70 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.12 |
| 1588 | 0.00 | 219.21 | 10.70 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.11 |
| 1592 | 0.00 | 219.17 | 10.70 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 1596 | 0.00 | 219.14 | 10.70 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 1600 | 0.00 | 219.11 | 10.70 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 1604 | 0.00 | 219.09 | 9.50 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 1608 | 0.00 | 219.07 | 7.36 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |

...End

Reservoir Report

Reservoir No. 3 - Basin 3 (Hotel)

Hydraflow Hydrographs by Intelisoive

Pond Data

Pond storage is based on known contour areas. Average end area method used.

Stage / Storage Table

| Stage (ft) | Elevation (ft) | Contour area (sqft) | Incr. Storage (cuft) | Total storage (cuft) |
|------------|----------------|---------------------|----------------------|----------------------|
| 0.00 | 219.00 | 00 | 0 | 0 |
| 1.00 | 220.00 | 1,406 | 703 | 703 |
| 3.00 | 222.00 | 4,776 | 6,182 | 6,885 |
| 5.00 | 224.00 | 5,971 | 10,747 | 17,632 |
| 7.00 | 226.00 | 7,278 | 13,249 | 30,881 |
| 9.00 | 228.00 | 8,709 | 15,987 | 46,868 |
| 9.50 | 228.50 | 9,086 | 4,449 | 51,317 |

Culvert / Orifice Structures

| | [A] | [B] | [C] | [D] |
|---------------|----------|--------|--------|------|
| Rise in | = 24.0 | 3.0 | 12.0 | 0.0 |
| Span in | = 24.0 | 3.0 | 12.0 | 0.0 |
| No. Barrels | = 1 | 1 | 1 | 0 |
| Invert El. ft | = 217.50 | 217.90 | 224.00 | 0.00 |
| Length ft | = 48.0 | 1.0 | 1.0 | 0.0 |
| Slope % | = 10.00 | 0.00 | 0.00 | 0.00 |
| N-Value | = .013 | .013 | .013 | .000 |
| Orif. Coeff. | = 0.60 | 0.60 | 0.60 | 0.00 |
| Multi-Stage | = n/a | Yes | Yes | No |

Weir Structures

| | [A] | [B] | [C] | [D] |
|--------------|----------|--------|--------|--------|
| Crest Len ft | = 1.00 | 2.00 | 16.00 | 90.00 |
| Crest El. ft | = 225.25 | 226.00 | 227.00 | 227.00 |
| Weir Coeff. | = 3.33 | 3.33 | 3.33 | 2.60 |
| Weir Type | = Rect | Rect | Rect | Broad |
| Multi-Stage | = Yes | Yes | Yes | Yes |

Exfiltration Rate = 0.00 in/hr/sqft Tailwater Elev. = 0.00 ft

Note: All outflows have been analyzed under inlet and outlet control.

Stage / Storage / Discharge Table

| Stage ft | Storage cuft | Elevation ft | Civ A cfs | Civ B cfs | Civ C cfs | Civ D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Total cfs |
|----------|--------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-----------|
| 0.00 | 0 | 219.00 | 0.00 | 0.00 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.00 |
| 0.10 | 70 | 219.10 | 10.70 | 0.07 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.07 |
| 0.20 | 141 | 219.20 | 10.70 | 0.11 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.11 |
| 0.30 | 211 | 219.30 | 10.70 | 0.13 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.13 |
| 0.40 | 281 | 219.40 | 10.70 | 0.15 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.15 |
| 0.50 | 352 | 219.50 | 10.70 | 0.17 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.17 |
| 0.60 | 422 | 219.60 | 10.70 | 0.18 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.18 |
| 0.70 | 492 | 219.70 | 10.70 | 0.20 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.20 |
| 0.80 | 562 | 219.80 | 10.70 | 0.21 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.21 |
| 0.90 | 633 | 219.90 | 10.70 | 0.22 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.22 |
| 1.00 | 703 | 220.00 | 10.70 | 0.24 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.24 |
| 1.20 | 1,321 | 220.20 | 10.70 | 0.26 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.26 |
| 1.40 | 1,939 | 220.40 | 10.70 | 0.28 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.28 |
| 1.60 | 2,558 | 220.60 | 10.70 | 0.30 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.30 |
| 1.80 | 3,176 | 220.80 | 10.70 | 0.32 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.32 |
| 2.00 | 3,794 | 221.00 | 10.70 | 0.33 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.33 |
| 2.20 | 4,412 | 221.20 | 10.70 | 0.35 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.35 |
| 2.40 | 5,030 | 221.40 | 10.70 | 0.37 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.37 |
| 2.60 | 5,649 | 221.60 | 10.70 | 0.38 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.38 |
| 2.80 | 6,267 | 221.80 | 10.70 | 0.40 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.40 |
| 3.00 | 6,885 | 222.00 | 10.70 | 0.41 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.41 |
| 3.20 | 7,960 | 222.20 | 10.70 | 0.42 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.42 |
| 3.40 | 9,034 | 222.40 | 10.70 | 0.44 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.44 |
| 3.60 | 10,109 | 222.60 | 10.70 | 0.45 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.45 |
| 3.80 | 11,184 | 222.80 | 10.70 | 0.46 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.46 |
| 4.00 | 12,259 | 223.00 | 10.70 | 0.47 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.47 |
| 4.20 | 13,333 | 223.20 | 10.70 | 0.48 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.48 |
| 4.40 | 14,408 | 223.40 | 10.70 | 0.50 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.50 |
| 4.60 | 15,483 | 223.60 | 10.70 | 0.51 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.51 |
| 4.80 | 16,557 | 223.80 | 10.70 | 0.52 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.52 |
| 5.00 | 17,632 | 224.00 | 10.70 | 0.53 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.53 |

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Stage / Storage / Discharge Table

| Stage ft | Storage cuft | Elevation ft | Civ A cfs | Civ B cfs | Civ C cfs | Civ D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Total cfs |
|-------------|-----------------|-----------------|--------------|--------------|--------------|--------------|-------------|-------------|-------------|-------------|--------------|--------------|
| 5.20 | 18,957 | 224.20 | 10.70 | 0.54 | 0.18 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.72 |
| 5.40 | 20,282 | 224.40 | 10.70 | 0.55 | 0.64 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 1.19 |
| 5.60 | 21,607 | 224.60 | 10.70 | 0.56 | 1.34 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 1.90 |
| 5.80 | 22,932 | 224.80 | 10.70 | 0.57 | 2.07 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 2.64 |
| 6.00 | 24,257 | 225.00 | 10.70 | 0.58 | 2.67 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 3.25 |
| 6.20 | 25,581 | 225.20 | 10.70 | 0.59 | 3.16 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 3.75 |
| 6.40 | 26,906 | 225.40 | 10.70 | 0.60 | 3.59 | --- | 0.19 | 0.00 | 0.00 | 0.00 | --- | 4.38 |
| 6.60 | 28,231 | 225.60 | 10.70 | 0.61 | 3.97 | --- | 0.69 | 0.00 | 0.00 | 0.00 | --- | 5.26 |
| 6.80 | 29,556 | 225.80 | 10.70 | 0.62 | 4.31 | --- | 1.36 | 0.00 | 0.00 | 0.00 | --- | 6.29 |
| 7.00 | 30,881 | 226.00 | 10.70 | 0.63 | 4.63 | --- | 2.16 | 0.00 | 0.00 | 0.00 | --- | 7.42 |
| 7.20 | 32,480 | 226.20 | 10.70 | 0.63 | 4.93 | --- | 3.08 | 0.60 | 0.00 | 0.00 | --- | 9.24 |
| 7.40 | 34,078 | 226.40 | 11.69 | 0.64 | 5.21 | --- | 4.11 | 1.68 | 0.00 | 0.00 | --- | 11.64 |
| 7.60 | 35,677 | 226.60 | 14.47 | 0.63 | 5.48 | --- | 5.22 | 3.10 | 0.00 | 0.00 | --- | 14.43 |
| 7.80 | 37,276 | 226.80 | 17.55 | 0.62 | 5.73 | --- | 6.43 | 4.77 | 0.00 | 0.00 | --- | 17.55 |
| 8.00 | 38,875 | 227.00 | 20.95 | 0.61 | 5.98 | --- | 7.71 | 6.66 | 0.00 | 0.00 | --- | 20.95 |
| 8.20 | 40,473 | 227.20 | 42.98 | 0.19 | 2.99 | --- | 6.61 | 7.50 | 4.76 | 20.93 | --- | 42.98 |
| 8.40 | 42,072 | 227.40 | 45.00 | 0.05 | 0.84 | --- | 2.87 | 3.56 | 6.98 | 30.65 | --- | 44.96 |
| 8.60 | 43,671 | 227.60 | 45.58 | 0.03 | 0.50 | --- | 2.13 | 2.78 | 7.43 | 32.62 | --- | 45.49 |
| 8.80 | 45,269 | 227.80 | 46.10 | 0.02 | 0.35 | --- | 1.75 | 2.38 | 7.69 | 33.77 | --- | 45.95 |
| 9.00 | 46,868 | 228.00 | 46.61 | 0.02 | 0.26 | --- | 1.53 | 2.14 | 7.90 | 34.69 | --- | 46.53 |
| 9.05 | 47,313 | 228.05 | 46.73 | 0.02 | 0.24 | --- | 1.48 | 2.09 | 7.91 | 34.75 | --- | 46.48 |
| 9.10 | 47,758 | 228.10 | 46.85 | 0.01 | 0.23 | --- | 1.43 | 2.04 | 7.92 | 34.79 | --- | 46.41 |
| 9.15 | 48,203 | 228.15 | 46.98 | 0.01 | 0.21 | --- | 1.39 | 2.00 | 7.95 | 34.93 | --- | 46.50 |
| 9.20 | 48,648 | 228.20 | 47.10 | 0.01 | 0.20 | --- | 1.37 | 1.97 | 8.02 | 35.22 | --- | 46.79 |
| 9.25 | 49,092 | 228.25 | 47.22 | 0.01 | 0.19 | --- | 1.33 | 1.94 | 8.04 | 35.33 | --- | 46.85 |
| 9.30 | 49,537 | 228.30 | 47.34 | 0.01 | 0.18 | --- | 1.30 | 1.89 | 8.01 | 35.19 | --- | 46.59 |
| 9.35 | 49,982 | 228.35 | 47.46 | 0.01 | 0.17 | --- | 1.27 | 1.87 | 8.07 | 35.43 | --- | 46.82 |
| 9.40 | 50,427 | 228.40 | 47.58 | 0.01 | 0.16 | --- | 1.25 | 1.84 | 8.07 | 35.43 | --- | 46.76 |
| 9.45 | 50,872 | 228.45 | 47.70 | 0.01 | 0.16 | --- | 1.24 | 1.84 | 8.21 | 36.07 | --- | 47.54 |
| 9.50 | 51,317 | 228.50 | 47.83 | 0.01 | 0.15 | --- | 1.20 | 1.79 | 8.08 | 35.50 | --- | 46.73 |

...End

Hydrograph Report

Hyd. No. 14

Hydrograph type = Combine
Storm frequency = 2 yrs
Inflow hyds. = 11, 12, 13

Peak discharge = 1.10 cfs
Time interval = 2 min

Hydrograph Volume = 47,272 cuft

Hydrograph Discharge Table

| Time (min) | Hyd. 11 + (cfs) | Hyd. 12 + (cfs) | Hyd. 13 = (cfs) | Outflow (cfs) |
|------------|-----------------|-----------------|-----------------|---------------|
| 612 | 0.01 | 0.01 | 0.09 | 0.11 |
| 616 | 0.01 | 0.01 | 0.10 | 0.12 |
| 620 | 0.01 | 0.01 | 0.10 | 0.12 |
| 624 | 0.01 | 0.01 | 0.10 | 0.13 |
| 628 | 0.01 | 0.01 | 0.11 | 0.14 |
| 632 | 0.01 | 0.01 | 0.11 | 0.14 |
| 636 | 0.02 | 0.02 | 0.12 | 0.15 |
| 640 | 0.02 | 0.02 | 0.12 | 0.16 |
| 644 | 0.02 | 0.02 | 0.13 | 0.17 |
| 648 | 0.02 | 0.02 | 0.14 | 0.17 |
| 652 | 0.02 | 0.02 | 0.14 | 0.18 |
| 656 | 0.02 | 0.02 | 0.15 | 0.19 |
| 660 | 0.02 | 0.02 | 0.15 | 0.20 |
| 664 | 0.03 | 0.02 | 0.16 | 0.20 |
| 668 | 0.03 | 0.02 | 0.17 | 0.21 |
| 672 | 0.03 | 0.02 | 0.17 | 0.22 |
| 676 | 0.03 | 0.02 | 0.18 | 0.23 |
| 680 | 0.03 | 0.02 | 0.19 | 0.24 |
| 684 | 0.03 | 0.02 | 0.20 | 0.25 |
| 688 | 0.04 | 0.02 | 0.21 | 0.27 |
| 692 | 0.04 | 0.02 | 0.22 | 0.28 |
| 696 | 0.04 | 0.02 | 0.24 | 0.30 |
| 700 | 0.05 | 0.02 | 0.24 | 0.31 |
| 704 | 0.05 | 0.02 | 0.25 | 0.32 |
| 708 | 0.06 | 0.02 | 0.26 | 0.34 |
| 712 | 0.07 | 0.02 | 0.27 | 0.36 |
| 716 | 0.08 | 0.02 | 0.28 | 0.39 |
| 720 | 0.10 | 0.02 | 0.30 | 0.42 |
| 724 | 0.12 | 0.03 | 0.33 | 0.48 |
| 728 | 0.14 | 0.03 | 0.37 | 0.54 |
| 732 | 0.16 | 0.08 | 0.39 | 0.64 |
| 736 | 0.18 | 0.15 | 0.41 | 0.74 |
| 740 | 0.19 | 0.19 | 0.42 | 0.80 |
| 744 | 0.20 | 0.22 | 0.42 | 0.84 |
| 748 | 0.21 | 0.24 | 0.43 | 0.87 |
| 752 | 0.21 | 0.25 | 0.43 | 0.89 |
| 756 | 0.21 | 0.26 | 0.44 | 0.91 |
| 760 | 0.22 | 0.28 | 0.44 | 0.94 |

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Hydrograph Discharge Table

| Time (min) | Hyd. 11 + (cfs) | Hyd. 12 + (cfs) | Hyd. 13 = (cfs) | Outflow (cfs) |
|---------------|--------------------|--------------------|--------------------|------------------|
| 764 | 0.22 | 0.31 | 0.44 | 0.98 |
| 768 | 0.22 | 0.33 | 0.44 | 1.01 |
| 772 | 0.22 | 0.34 | 0.44 | 1.04 |
| 776 | 0.22 | 0.35 | 0.44 | 1.05 |
| 780 | 0.22 | 0.36 | 0.44 | 1.07 |
| 784 | 0.22 | 0.37 | 0.44 | 1.08 |
| 788 | 0.23 | 0.38 | 0.44 | 1.09 |
| 792 | 0.23 | 0.38 | 0.44 | 1.09 |
| 796 | 0.23 | 0.39 | 0.44 | 1.09 |
| 800 | 0.23 | 0.39 | 0.44 | 1.10 |
| 804 | 0.23 | 0.39 | 0.45 | 1.10 |
| 808 | 0.23 | 0.39 | 0.45 | 1.10 |
| 812 | 0.23 | 0.39 | 0.45 | 1.10 << |
| 816 | 0.23 | 0.39 | 0.45 | 1.10 |
| 820 | 0.23 | 0.40 | 0.45 | 1.10 |
| 824 | 0.23 | 0.40 | 0.45 | 1.10 |
| 828 | 0.23 | 0.39 | 0.45 | 1.10 |
| 832 | 0.23 | 0.39 | 0.45 | 1.09 |
| 836 | 0.23 | 0.39 | 0.45 | 1.09 |
| 840 | 0.23 | 0.39 | 0.45 | 1.09 |
| 844 | 0.23 | 0.39 | 0.45 | 1.08 |
| 848 | 0.23 | 0.39 | 0.45 | 1.08 |
| 852 | 0.23 | 0.38 | 0.45 | 1.07 |
| 856 | 0.23 | 0.38 | 0.45 | 1.07 |
| 860 | 0.23 | 0.38 | 0.45 | 1.07 |
| 864 | 0.23 | 0.38 | 0.45 | 1.06 |
| 868 | 0.23 | 0.37 | 0.45 | 1.06 |
| 872 | 0.23 | 0.37 | 0.45 | 1.05 |
| 876 | 0.23 | 0.37 | 0.45 | 1.05 |
| 880 | 0.23 << | 0.36 | 0.45 | 1.04 |
| 884 | 0.23 | 0.36 | 0.44 | 1.04 |
| 888 | 0.23 | 0.36 | 0.44 | 1.03 |
| 892 | 0.23 | 0.35 | 0.44 | 1.02 |
| 896 | 0.23 | 0.35 | 0.44 | 1.02 |
| 900 | 0.23 | 0.35 | 0.44 | 1.01 |
| 904 | 0.23 | 0.34 | 0.44 | 1.01 |
| 908 | 0.23 | 0.34 | 0.44 | 1.00 |
| 912 | 0.23 | 0.33 | 0.44 | 1.00 |
| 916 | 0.23 | 0.33 | 0.44 | 0.99 |
| 920 | 0.23 | 0.33 | 0.44 | 0.99 |
| 924 | 0.23 | 0.32 | 0.44 | 0.98 |
| 928 | 0.23 | 0.32 | 0.44 | 0.98 |
| 932 | 0.23 | 0.31 | 0.44 | 0.97 |
| 936 | 0.23 | 0.31 | 0.44 | 0.97 |
| 940 | 0.23 | 0.31 | 0.44 | 0.96 |
| 944 | 0.23 | 0.30 | 0.44 | 0.95 |
| 948 | 0.23 | 0.30 | 0.44 | 0.95 |
| 952 | 0.23 | 0.29 | 0.44 | 0.94 |
| 956 | 0.23 | 0.29 | 0.44 | 0.94 |
| 960 | 0.23 | 0.29 | 0.44 | 0.93 |
| 964 | 0.23 | 0.28 | 0.44 | 0.93 |

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Hydrograph Discharge Table

| Time (min) | Hyd. 11 + (cfs) | Hyd. 12 + (cfs) | Hyd. 13 = (cfs) | Outflow (cfs) |
|---------------|--------------------|--------------------|--------------------|------------------|
| 968 | 0.23 | 0.28 | 0.44 | 0.93 |
| 972 | 0.23 | 0.27 | 0.44 | 0.92 |
| 976 | 0.23 | 0.27 | 0.43 | 0.92 |
| 980 | 0.23 | 0.26 | 0.43 | 0.92 |
| 984 | 0.23 | 0.26 | 0.43 | 0.92 |
| 988 | 0.23 | 0.26 | 0.43 | 0.92 |
| 992 | 0.23 | 0.26 | 0.43 | 0.92 |
| 996 | 0.23 | 0.26 | 0.43 | 0.91 |
| 1000 | 0.23 | 0.26 | 0.43 | 0.91 |
| 1004 | 0.22 | 0.26 | 0.43 | 0.91 |
| 1008 | 0.22 | 0.26 | 0.43 | 0.91 |
| 1012 | 0.22 | 0.26 | 0.43 | 0.91 |
| 1016 | 0.22 | 0.26 | 0.43 | 0.90 |
| 1020 | 0.22 | 0.25 | 0.43 | 0.90 |
| 1024 | 0.22 | 0.25 | 0.43 | 0.90 |
| 1028 | 0.22 | 0.25 | 0.43 | 0.90 |
| 1032 | 0.22 | 0.25 | 0.43 | 0.90 |
| 1036 | 0.22 | 0.25 | 0.42 | 0.89 |
| 1040 | 0.22 | 0.25 | 0.42 | 0.89 |
| 1044 | 0.22 | 0.25 | 0.42 | 0.89 |
| 1048 | 0.22 | 0.25 | 0.42 | 0.89 |
| 1052 | 0.22 | 0.25 | 0.42 | 0.89 |
| 1056 | 0.22 | 0.25 | 0.42 | 0.88 |
| 1060 | 0.22 | 0.24 | 0.42 | 0.88 |
| 1064 | 0.22 | 0.24 | 0.42 | 0.88 |
| 1068 | 0.22 | 0.24 | 0.42 | 0.88 |
| 1072 | 0.22 | 0.24 | 0.42 | 0.87 |
| 1076 | 0.22 | 0.24 | 0.42 | 0.87 |
| 1080 | 0.22 | 0.24 | 0.42 | 0.87 |
| 1084 | 0.21 | 0.24 | 0.42 | 0.87 |
| 1088 | 0.21 | 0.24 | 0.41 | 0.86 |
| 1092 | 0.21 | 0.24 | 0.41 | 0.86 |
| 1096 | 0.21 | 0.24 | 0.41 | 0.86 |
| 1100 | 0.21 | 0.23 | 0.41 | 0.86 |
| 1104 | 0.21 | 0.23 | 0.41 | 0.85 |
| 1108 | 0.21 | 0.23 | 0.41 | 0.85 |
| 1112 | 0.21 | 0.23 | 0.41 | 0.85 |
| 1116 | 0.21 | 0.23 | 0.41 | 0.84 |
| 1120 | 0.21 | 0.23 | 0.41 | 0.84 |
| 1124 | 0.21 | 0.23 | 0.41 | 0.84 |
| 1128 | 0.21 | 0.23 | 0.40 | 0.84 |
| 1132 | 0.21 | 0.22 | 0.40 | 0.83 |
| 1136 | 0.21 | 0.22 | 0.40 | 0.83 |
| 1140 | 0.21 | 0.22 | 0.40 | 0.83 |
| 1144 | 0.21 | 0.22 | 0.40 | 0.82 |
| 1148 | 0.21 | 0.22 | 0.40 | 0.82 |
| 1152 | 0.20 | 0.22 | 0.40 | 0.82 |
| 1156 | 0.20 | 0.22 | 0.39 | 0.81 |
| 1160 | 0.20 | 0.22 | 0.39 | 0.81 |
| 1164 | 0.20 | 0.21 | 0.39 | 0.81 |
| 1168 | 0.20 | 0.21 | 0.39 | 0.80 |

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Hydrograph Discharge Table

| Time (min) | Hyd. 11 + (cfs) | Hyd. 12 + (cfs) | Hyd. 13 = (cfs) | Outflow (cfs) |
|---------------|--------------------|--------------------|--------------------|------------------|
| 1172 | 0.20 | 0.21 | 0.39 | 0.80 |
| 1176 | 0.20 | 0.21 | 0.39 | 0.80 |
| 1180 | 0.20 | 0.21 | 0.39 | 0.79 |
| 1184 | 0.20 | 0.21 | 0.38 | 0.79 |
| 1188 | 0.20 | 0.21 | 0.38 | 0.79 |
| 1192 | 0.20 | 0.21 | 0.38 | 0.78 |
| 1196 | 0.20 | 0.21 | 0.38 | 0.78 |
| 1200 | 0.20 | 0.20 | 0.38 | 0.78 |
| 1204 | 0.20 | 0.20 | 0.38 | 0.77 |
| 1208 | 0.20 | 0.20 | 0.38 | 0.77 |
| 1212 | 0.20 | 0.20 | 0.37 | 0.77 |
| 1216 | 0.19 | 0.20 | 0.37 | 0.76 |
| 1220 | 0.19 | 0.20 | 0.37 | 0.76 |
| 1224 | 0.19 | 0.20 | 0.37 | 0.76 |
| 1228 | 0.19 | 0.20 | 0.37 | 0.75 |
| 1232 | 0.19 | 0.19 | 0.37 | 0.75 |
| 1236 | 0.19 | 0.19 | 0.36 | 0.75 |
| 1240 | 0.19 | 0.19 | 0.36 | 0.74 |
| 1244 | 0.19 | 0.19 | 0.36 | 0.74 |
| 1248 | 0.19 | 0.19 | 0.36 | 0.74 |
| 1252 | 0.19 | 0.19 | 0.36 | 0.73 |
| 1256 | 0.19 | 0.19 | 0.36 | 0.73 |
| 1260 | 0.19 | 0.19 | 0.36 | 0.73 |
| 1264 | 0.19 | 0.18 | 0.35 | 0.72 |
| 1268 | 0.19 | 0.18 | 0.35 | 0.72 |
| 1272 | 0.19 | 0.18 | 0.35 | 0.72 |
| 1276 | 0.18 | 0.18 | 0.35 | 0.71 |
| 1280 | 0.18 | 0.18 | 0.35 | 0.71 |
| 1284 | 0.18 | 0.18 | 0.35 | 0.71 |
| 1288 | 0.18 | 0.18 | 0.34 | 0.70 |
| 1292 | 0.18 | 0.18 | 0.34 | 0.70 |
| 1296 | 0.18 | 0.17 | 0.34 | 0.69 |
| 1300 | 0.18 | 0.17 | 0.34 | 0.69 |
| 1304 | 0.18 | 0.17 | 0.34 | 0.69 |
| 1308 | 0.18 | 0.17 | 0.34 | 0.68 |
| 1312 | 0.18 | 0.17 | 0.34 | 0.68 |
| 1316 | 0.18 | 0.17 | 0.33 | 0.68 |
| 1320 | 0.18 | 0.17 | 0.33 | 0.67 |
| 1324 | 0.18 | 0.17 | 0.33 | 0.67 |
| 1328 | 0.18 | 0.16 | 0.33 | 0.67 |
| 1332 | 0.18 | 0.16 | 0.33 | 0.67 |
| 1336 | 0.18 | 0.16 | 0.33 | 0.66 |
| 1340 | 0.17 | 0.16 | 0.33 | 0.66 |
| 1344 | 0.17 | 0.16 | 0.32 | 0.66 |
| 1348 | 0.17 | 0.16 | 0.32 | 0.65 |
| 1352 | 0.17 | 0.16 | 0.32 | 0.65 |
| 1356 | 0.17 | 0.16 | 0.32 | 0.65 |
| 1360 | 0.17 | 0.16 | 0.32 | 0.64 |
| 1364 | 0.17 | 0.15 | 0.32 | 0.64 |
| 1368 | 0.17 | 0.15 | 0.31 | 0.63 |
| 1372 | 0.17 | 0.15 | 0.31 | 0.63 |

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Hydrograph Discharge Table

| Time (min) | Hyd. 11 + (cfs) | Hyd. 12 + (cfs) | Hyd. 13 = (cfs) | Outflow (cfs) |
|---------------|--------------------|--------------------|--------------------|------------------|
| 1376 | 0.17 | 0.15 | 0.31 | 0.63 |
| 1380 | 0.17 | 0.15 | 0.31 | 0.62 |
| 1384 | 0.17 | 0.15 | 0.31 | 0.62 |
| 1388 | 0.17 | 0.15 | 0.31 | 0.62 |
| 1392 | 0.17 | 0.14 | 0.31 | 0.61 |
| 1396 | 0.17 | 0.14 | 0.30 | 0.61 |
| 1400 | 0.17 | 0.14 | 0.30 | 0.61 |
| 1404 | 0.16 | 0.14 | 0.30 | 0.60 |
| 1408 | 0.16 | 0.14 | 0.30 | 0.60 |
| 1412 | 0.16 | 0.14 | 0.30 | 0.60 |
| 1416 | 0.16 | 0.14 | 0.30 | 0.59 |
| 1420 | 0.16 | 0.13 | 0.29 | 0.59 |
| 1424 | 0.16 | 0.13 | 0.29 | 0.58 |
| 1428 | 0.16 | 0.13 | 0.29 | 0.58 |
| 1432 | 0.16 | 0.13 | 0.29 | 0.58 |
| 1436 | 0.16 | 0.13 | 0.29 | 0.57 |
| 1440 | 0.16 | 0.13 | 0.29 | 0.57 |
| 1444 | 0.16 | 0.13 | 0.28 | 0.57 |
| 1448 | 0.16 | 0.13 | 0.28 | 0.56 |
| 1452 | 0.16 | 0.12 | 0.28 | 0.56 |
| 1456 | 0.15 | 0.12 | 0.28 | 0.55 |
| 1460 | 0.15 | 0.12 | 0.28 | 0.55 |
| 1464 | 0.15 | 0.12 | 0.27 | 0.54 |
| 1468 | 0.15 | 0.12 | 0.27 | 0.54 |
| 1472 | 0.15 | 0.11 | 0.27 | 0.53 |
| 1476 | 0.15 | 0.11 | 0.27 | 0.53 |
| 1480 | 0.15 | 0.11 | 0.27 | 0.52 |
| 1484 | 0.15 | 0.11 | 0.26 | 0.52 |
| 1488 | 0.15 | 0.11 | 0.26 | 0.51 |
| 1492 | 0.14 | 0.10 | 0.26 | 0.51 |
| 1496 | 0.14 | 0.10 | 0.26 | 0.50 |
| 1500 | 0.14 | 0.10 | 0.25 | 0.50 |
| 1504 | 0.14 | 0.10 | 0.25 | 0.49 |
| 1508 | 0.14 | 0.10 | 0.25 | 0.49 |
| 1512 | 0.14 | 0.09 | 0.25 | 0.48 |
| 1516 | 0.14 | 0.09 | 0.25 | 0.48 |
| 1520 | 0.14 | 0.09 | 0.24 | 0.47 |
| 1524 | 0.14 | 0.09 | 0.24 | 0.47 |
| 1528 | 0.14 | 0.09 | 0.24 | 0.46 |
| 1532 | 0.14 | 0.09 | 0.24 | 0.46 |
| 1536 | 0.13 | 0.08 | 0.23 | 0.45 |
| 1540 | 0.13 | 0.08 | 0.22 | 0.44 |
| 1544 | 0.13 | 0.08 | 0.21 | 0.42 |
| 1548 | 0.13 | 0.08 | 0.20 | 0.41 |
| 1552 | 0.13 | 0.08 | 0.19 | 0.40 |
| 1556 | 0.13 | 0.08 | 0.18 | 0.39 |
| 1560 | 0.13 | 0.07 | 0.17 | 0.38 |
| 1564 | 0.13 | 0.07 | 0.17 | 0.36 |
| 1568 | 0.13 | 0.07 | 0.16 | 0.35 |
| 1572 | 0.13 | 0.07 | 0.15 | 0.34 |
| 1576 | 0.13 | 0.07 | 0.14 | 0.33 |

Continues on next page...

Hydrograph Discharge Table

| Time (min) | Hyd. 11 + (cfs) | Hyd. 12 + (cfs) | Hyd. 13 = (cfs) | Outflow (cfs) |
|---------------|--------------------|--------------------|--------------------|------------------|
| 1580 | 0.12 | 0.07 | 0.13 | 0.32 |
| 1584 | 0.12 | 0.07 | 0.12 | 0.31 |
| 1588 | 0.12 | 0.06 | 0.11 | 0.29 |
| 1592 | 0.12 | 0.06 | 0.10 | 0.28 |
| 1596 | 0.12 | 0.06 | 0.09 | 0.27 |
| 1600 | 0.12 | 0.06 | 0.08 | 0.26 |
| 1604 | 0.12 | 0.06 | 0.07 | 0.24 |
| 1608 | 0.12 | 0.06 | 0.05 | 0.22 |
| 1612 | 0.11 | 0.06 | 0.04 | 0.21 |
| 1616 | 0.11 | 0.06 | 0.03 | 0.20 |
| 1620 | 0.11 | 0.06 | 0.02 | 0.19 |
| 1624 | 0.11 | 0.05 | 0.02 | 0.18 |
| 1628 | 0.11 | 0.05 | 0.01 | 0.18 |
| 1632 | 0.11 | 0.05 | 0.01 | 0.17 |
| 1636 | 0.11 | 0.05 | 0.01 | 0.17 |
| 1640 | 0.11 | 0.05 | 0.01 | 0.16 |
| 1644 | 0.10 | 0.05 | 0.01 | 0.16 |
| 1648 | 0.10 | 0.05 | 0.00 | 0.16 |
| 1652 | 0.10 | 0.05 | 0.00 | 0.15 |
| 1656 | 0.10 | 0.05 | 0.00 | 0.15 |
| 1660 | 0.10 | 0.05 | 0.00 | 0.15 |
| 1664 | 0.10 | 0.04 | 0.00 | 0.14 |
| 1668 | 0.10 | 0.04 | 0.00 | 0.14 |
| 1672 | 0.10 | 0.04 | 0.00 | 0.14 |
| 1676 | 0.10 | 0.04 | 0.00 | 0.14 |
| 1680 | 0.10 | 0.04 | 0.00 | 0.14 |
| 1684 | 0.09 | 0.04 | 0.00 | 0.13 |
| 1688 | 0.09 | 0.04 | 0.00 | 0.13 |
| 1692 | 0.09 | 0.04 | 0.00 | 0.13 |
| 1696 | 0.09 | 0.04 | 0.00 | 0.13 |
| 1700 | 0.09 | 0.04 | 0.00 | 0.13 |
| 1704 | 0.09 | 0.04 | 0.00 | 0.13 |
| 1708 | 0.09 | 0.04 | 0.00 | 0.12 |
| 1712 | 0.09 | 0.04 | 0.00 | 0.12 |
| 1716 | 0.09 | 0.03 | 0.00 | 0.12 |
| 1720 | 0.09 | 0.03 | 0.00 | 0.12 |
| 1724 | 0.08 | 0.03 | 0.00 | 0.12 |
| 1728 | 0.08 | 0.03 | 0.00 | 0.12 |
| 1732 | 0.08 | 0.03 | 0.00 | 0.11 |
| 1736 | 0.08 | 0.03 | 0.00 | 0.11 |
| 1740 | 0.08 | 0.03 | 0.00 | 0.11 |
| 1744 | 0.08 | 0.03 | 0.00 | 0.11 |

...End

Hydrograph Summary Report

| Hyd. No. | Hydrograph type (origin) | Peak flow (cfs) | Time interval (min) | Time to peak (min) | Volume (cuft) | Inflow hyd(s) | Maximum elevation (ft) | Maximum storage (cuft) | Hydrograph description |
|----------|--------------------------|-----------------|---------------------|--------------------|---------------|---------------|------------------------|------------------------|------------------------|
| 1 | SCS Runoff | 8.97 | 2 | 732 | 40,073 | --- | ---- | ---- | Predevelopment |
| 2 | SCS Runoff | 6.21 | 2 | 728 | 23,955 | --- | ---- | ---- | Post Subarea 1a |
| 3 | SCS Runoff | 0.40 | 2 | 724 | 1,305 | --- | ---- | ---- | Post Subarea 1b |
| 4 | SCS Runoff | 7.26 | 2 | 730 | 30,126 | --- | ---- | ---- | Post Subarea 2a |
| 5 | SCS Runoff | 0.38 | 2 | 724 | 1,258 | --- | ---- | ---- | Post Subarea 2b |
| 6 | SCS Runoff | 11.18 | 2 | 726 | 38,512 | --- | ---- | ---- | Post Subarea 3a |
| 7 | SCS Runoff | 0.50 | 2 | 724 | 1,631 | --- | ---- | ---- | Post Subarea 3b |
| 8 | Combine | 6.52 | 2 | 728 | 25,260 | 2, 3, | ---- | ---- | Basin 1 In |
| 9 | Combine | 7.51 | 2 | 730 | 31,384 | 4, 5, | ---- | ---- | Basin 2 In |
| 10 | Combine | 11.65 | 2 | 726 | 40,143 | 6, 7, | ---- | ---- | Basin 3 In |
| 11 | Reservoir | 0.35 | 2 | 914 | 24,998 | 8 | 242.34 | 26,745 | Basin 1 Out |
| 12 | Reservoir | 2.53 | 2 | 754 | 28,194 | 9 | 232.99 | 14,998 | Basin 2 Out |
| 13 | Reservoir | 1.15 | 2 | 784 | 40,143 | 10 | 224.38 | 20,176 | Basin 3 Out |
| 14 | Combine | 4.21 | 2 | 754 | 93,343 | 11, 12, 13 | ---- | ---- | |

Proj. file: ansuya.basin.9-30-04.gpw Return Period: 10 yr Run date: 10-08-2004

Hydrograph Report

Hyd. No. 1

Predevelopment

| | | | |
|-----------------|--------------|--------------------|------------|
| Hydrograph type | = SCS Runoff | Peak discharge | = 8.97 cfs |
| Storm frequency | = 10 yrs | Time interval | = 2 min |
| Drainage area | = 8.27 ac | Curve number | = 61 |
| Basin Slope | = 0.0 % | Hydraulic length | = 0 ft |
| Tc method | = USER | Time of conc. (Tc) | = 14.4 min |
| Total precip. | = 5.00 in | Distribution | = Type III |
| Storm duration | = 24 hrs | Shape factor | = 484 |

Hydrograph Volume = 40,073 cuft

Hydrograph Discharge Table

| Time (min) | Outflow (cfs) | Time (min) | Outflow (cfs) | Time (min) | Outflow (cfs) |
|------------|---------------|------------|---------------|------------|---------------|
| 702 | 0.47 | 838 | 1.12 | 974 | 0.58 |
| 706 | 0.75 | 842 | 1.09 | 978 | 0.57 |
| 710 | 1.16 | 846 | 1.06 | 982 | 0.56 |
| 714 | 1.73 | 850 | 1.04 | 986 | 0.56 |
| 718 | 2.64 | 854 | 1.02 | 990 | 0.55 |
| 722 | 4.47 | 858 | 1.00 | 994 | 0.54 |
| 726 | 6.96 | 862 | 0.99 | 998 | 0.54 |
| 730 | 8.73 | 866 | 0.98 | 1002 | 0.53 |
| 734 | 8.86 | 870 | 0.96 | 1006 | 0.52 |
| 738 | 8.12 | 874 | 0.95 | 1010 | 0.52 |
| 742 | 6.94 | 878 | 0.93 | 1014 | 0.51 |
| 746 | 5.71 | 882 | 0.92 | 1018 | 0.50 |
| 750 | 4.77 | 886 | 0.91 | 1022 | 0.50 |
| 754 | 3.91 | 890 | 0.89 | 1026 | 0.49 |
| 758 | 3.13 | 894 | 0.88 | 1030 | 0.48 |
| 762 | 2.56 | 898 | 0.86 | 1034 | 0.47 |
| 766 | 2.20 | 902 | 0.85 | 1038 | 0.47 |
| 770 | 1.99 | 906 | 0.84 | 1042 | 0.46 |
| 774 | 1.87 | 910 | 0.82 | 1046 | 0.45 |
| 778 | 1.77 | 914 | 0.81 | | |
| 782 | 1.67 | 918 | 0.79 | | |
| 786 | 1.57 | 922 | 0.78 | ...End | |
| 790 | 1.49 | 926 | 0.76 | | |
| 794 | 1.43 | 930 | 0.75 | | |
| 798 | 1.39 | 934 | 0.73 | | |
| 802 | 1.36 | 938 | 0.71 | | |
| 806 | 1.33 | 942 | 0.70 | | |
| 810 | 1.31 | 946 | 0.68 | | |
| 814 | 1.28 | 950 | 0.67 | | |
| 818 | 1.26 | 954 | 0.65 | | |
| 822 | 1.23 | 958 | 0.64 | | |
| 826 | 1.20 | 962 | 0.62 | | |
| 830 | 1.18 | 966 | 0.60 | | |
| 834 | 1.15 | 970 | 0.59 | | |

Hydrograph Report

Hyd. No. 2

Post Subarea 1a

| | | | |
|-----------------|--------------|--------------------|------------|
| Hydrograph type | = SCS Runoff | Peak discharge | = 6.21 cfs |
| Storm frequency | = 10 yrs | Time interval | = 2 min |
| Drainage area | = 1.90 ac | Curve number | = 85 |
| Basin Slope | = 0.0 % | Hydraulic length | = 0 ft |
| Tc method | = USER | Time of conc. (Tc) | = 10.6 min |
| Total precip. | = 5.00 in | Distribution | = Type III |
| Storm duration | = 24 hrs | Shape factor | = 484 |

Hydrograph Volume = 23,955 cuft

Hydrograph Discharge Table

| Time -- Outflow (min cfs) | Time -- Outflow (min cfs) | Time -- Outflow (min cfs) |
|------------------------------|------------------------------|------------------------------|
| 642 0.31 | 778 0.78 | 914 0.33 |
| 646 0.32 | 782 0.73 | 918 0.32 |
| 650 0.34 | 786 0.68 | 922 0.31 |
| 654 0.35 | 790 0.65 | |
| 658 0.36 | 794 0.62 | |
| 662 0.38 | 798 0.61 | ...End |
| 666 0.40 | 802 0.59 | |
| 670 0.42 | 806 0.58 | |
| 674 0.46 | 810 0.57 | |
| 678 0.50 | 814 0.55 | |
| 682 0.54 | 818 0.54 | |
| 686 0.59 | 822 0.53 | |
| 690 0.63 | 826 0.51 | |
| 694 0.70 | 830 0.50 | |
| 698 0.84 | 834 0.49 | |
| 702 1.10 | 838 0.47 | |
| 706 1.46 | 842 0.46 | |
| 710 1.88 | 846 0.45 | |
| 714 2.34 | 850 0.43 | |
| 718 3.02 | 854 0.43 | |
| 722 4.42 | 858 0.42 | |
| 726 5.92 | 862 0.41 | |
| 730 6.11 | 866 0.41 | |
| 734 5.26 | 870 0.40 | |
| 738 4.15 | 874 0.39 | |
| 742 3.20 | 878 0.39 | |
| 746 2.62 | 882 0.38 | |
| 750 2.14 | 886 0.37 | |
| 754 1.67 | 890 0.37 | |
| 758 1.30 | 894 0.36 | |
| 762 1.07 | 898 0.35 | |
| 766 0.95 | 902 0.35 | |
| 770 0.88 | 906 0.34 | |
| 774 0.83 | 910 0.33 | |

Hydrograph Report

Hyd. No. 3

Post Subarea 1b

Hydrograph type = SCS Runoff
Storm frequency = 10 yrs
Drainage area = 0.28 ac
Basin Slope = 0.0 %
Tc method = USER
Total precip. = 5.00 in
Storm duration = 24 hrs

Peak discharge = 0.40 cfs
Time interval = 2 min
Curve number = 61
Hydraulic length = 0 ft
Time of conc. (Tc) = 6 min
Distribution = Type III
Shape factor = 484

Hydrograph Volume = 1,305 cuft

Hydrograph Discharge Table

| Time -- Outflow (min cfs) | Time -- Outflow (min cfs) |
|------------------------------|------------------------------|
| 700 0.02 | 836 0.04 |
| 704 0.04 | 840 0.03 |
| 708 0.06 | 844 0.03 |
| 712 0.08 | 848 0.03 |
| 716 0.12 | 852 0.03 |
| 720 0.25 | 856 0.03 |
| 724 0.40 << | 860 0.03 |
| 728 0.32 | 864 0.03 |
| 732 0.23 | 868 0.03 |
| 736 0.20 | 872 0.03 |
| 740 0.18 | 876 0.03 |
| 744 0.15 | 880 0.03 |
| 748 0.12 | 884 0.03 |
| 752 0.09 | 888 0.03 |
| 756 0.07 | 892 0.03 |
| 760 0.07 | 896 0.03 |
| 764 0.06 | 900 0.03 |
| 768 0.06 | 904 0.03 |
| 772 0.06 | 908 0.03 |
| 776 0.05 | 912 0.03 |
| 780 0.05 | 916 0.03 |
| 784 0.05 | 920 0.02 |
| 788 0.05 | 924 0.02 |
| 792 0.04 | 928 0.02 |
| 796 0.04 | 932 0.02 |
| 800 0.04 | 936 0.02 |
| 804 0.04 | 940 0.02 |
| 808 0.04 | 944 0.02 |
| 812 0.04 | 948 0.02 |
| 816 0.04 | 952 0.02 |
| 820 0.04 | 956 0.02 |
| 824 0.04 | |
| 828 0.04 | |
| 832 0.04 | ...End |

Hydrograph Report

Hyd. No. 4

Post Subarea 2a

| | | | |
|-----------------|--------------|--------------------|------------|
| Hydrograph type | = SCS Runoff | Peak discharge | = 7.26 cfs |
| Storm frequency | = 10 yrs | Time interval | = 2 min |
| Drainage area | = 2.32 ac | Curve number | = 88 |
| Basin Slope | = 0.0 % | Hydraulic length | = 0 ft |
| Tc method | = USER | Time of conc. (Tc) | = 14.5 min |
| Total precip. | = 5.00 in | Distribution | = Type III |
| Storm duration | = 24 hrs | Shape factor | = 484 |

Hydrograph Volume = 30,126 cuft

Hydrograph Discharge Table

| Time (min) | Outflow (cfs) | Time (min) | Outflow (cfs) | Time (min) | Outflow (cfs) |
|------------|---------------|------------|---------------|------------|---------------|
| 626 | 0.36 | 762 | 1.46 | 898 | 0.43 |
| 630 | 0.38 | 766 | 1.24 | 902 | 0.42 |
| 634 | 0.39 | 770 | 1.11 | 906 | 0.41 |
| 638 | 0.41 | 774 | 1.04 | 910 | 0.40 |
| 642 | 0.43 | 778 | 0.97 | 914 | 0.39 |
| 646 | 0.44 | 782 | 0.91 | 918 | 0.39 |
| 650 | 0.46 | 786 | 0.85 | 922 | 0.38 |
| 654 | 0.48 | 790 | 0.80 | 926 | 0.37 |
| 658 | 0.49 | 794 | 0.77 | | |
| 662 | 0.51 | 798 | 0.74 | | |
| 666 | 0.53 | 802 | 0.72 | ...End | |
| 670 | 0.56 | 806 | 0.71 | | |
| 674 | 0.60 | 810 | 0.69 | | |
| 678 | 0.65 | 814 | 0.67 | | |
| 682 | 0.70 | 818 | 0.66 | | |
| 686 | 0.76 | 822 | 0.64 | | |
| 690 | 0.81 | 826 | 0.62 | | |
| 694 | 0.89 | 830 | 0.61 | | |
| 698 | 1.04 | 834 | 0.59 | | |
| 702 | 1.30 | 838 | 0.57 | | |
| 706 | 1.69 | 842 | 0.56 | | |
| 710 | 2.18 | 846 | 0.54 | | |
| 714 | 2.73 | 850 | 0.53 | | |
| 718 | 3.47 | 854 | 0.52 | | |
| 722 | 4.82 | 858 | 0.51 | | |
| 726 | 6.45 | 862 | 0.50 | | |
| 730 | 7.26 << | 866 | 0.49 | | |
| 734 | 6.79 | 870 | 0.48 | | |
| 738 | 5.78 | 874 | 0.47 | | |
| 742 | 4.60 | 878 | 0.47 | | |
| 746 | 3.57 | 882 | 0.46 | | |
| 750 | 2.88 | 886 | 0.45 | | |
| 754 | 2.31 | 890 | 0.44 | | |
| 758 | 1.82 | 894 | 0.43 | | |

Hydrograph Report

Hyd. No. 5

Post Subarea 2b

Hydrograph type = SCS Runoff
Storm frequency = 10 yrs
Drainage area = 0.27 ac
Basin Slope = 0.0 %
Tc method = USER
Total precip. = 5.00 in
Storm duration = 24 hrs

Peak discharge = 0.38 cfs
Time interval = 2 min
Curve number = 61
Hydraulic length = 0 ft
Time of conc. (Tc) = 6 min
Distribution = Type III
Shape factor = 484

Hydrograph Volume = 1,258 cuft

Hydrograph Discharge Table

| Time -- Outflow (min cfs) | Time -- Outflow (min cfs) |
|------------------------------|------------------------------|
| 700 0.02 | 836 0.03 |
| 704 0.04 | 840 0.03 |
| 708 0.06 | 844 0.03 |
| 712 0.08 | 848 0.03 |
| 716 0.12 | 852 0.03 |
| 720 0.24 | 856 0.03 |
| 724 0.38 << | 860 0.03 |
| 728 0.31 | 864 0.03 |
| 732 0.22 | 868 0.03 |
| 736 0.19 | 872 0.03 |
| 740 0.17 | 876 0.03 |
| 744 0.14 | 880 0.03 |
| 748 0.11 | 884 0.03 |
| 752 0.08 | 888 0.03 |
| 756 0.07 | 892 0.03 |
| 760 0.06 | 896 0.03 |
| 764 0.06 | 900 0.03 |
| 768 0.06 | 904 0.03 |
| 772 0.05 | 908 0.03 |
| 776 0.05 | 912 0.02 |
| 780 0.05 | 916 0.02 |
| 784 0.05 | 920 0.02 |
| 788 0.04 | 924 0.02 |
| 792 0.04 | 928 0.02 |
| 796 0.04 | 932 0.02 |
| 800 0.04 | 936 0.02 |
| 804 0.04 | 940 0.02 |
| 808 0.04 | 944 0.02 |
| 812 0.04 | 948 0.02 |
| 816 0.04 | 952 0.02 |
| 820 0.04 | 956 0.02 |
| 824 0.04 | |
| 828 0.04 | |
| 832 0.03 | ...End |

Hydrograph Report

Hyd. No. 6

Post Subarea 3a

| | | | |
|-----------------|--------------|--------------------|-------------|
| Hydrograph type | = SCS Runoff | Peak discharge | = 11.18 cfs |
| Storm frequency | = 10 yrs | Time interval | = 2 min |
| Drainage area | = 3.15 ac | Curve number | = 85 |
| Basin Slope | = 0.0 % | Hydraulic length | = 0 ft |
| Tc method | = USER | Time of conc. (Tc) | = 7.5 min |
| Total precip. | = 5.00 in | Distribution | = Type III |
| Storm duration | = 24 hrs | Shape factor | = 484 |

Hydrograph Volume = 38,512 cuft

Hydrograph Discharge Table

| Time -- Outflow (min cfs) | Time -- Outflow (min cfs) |
|------------------------------|------------------------------|
| 652 0.57 | 788 1.03 |
| 656 0.59 | 792 0.99 |
| 660 0.61 | 796 0.97 |
| 664 0.64 | 800 0.95 |
| 668 0.68 | 804 0.93 |
| 672 0.74 | 808 0.91 |
| 676 0.81 | 812 0.89 |
| 680 0.88 | 816 0.86 |
| 684 0.95 | 820 0.84 |
| 688 1.03 | 824 0.82 |
| 692 1.12 | 828 0.80 |
| 696 1.34 | 832 0.78 |
| 700 1.80 | 836 0.75 |
| 704 2.43 | 840 0.73 |
| 708 3.13 | 844 0.71 |
| 712 3.88 | 848 0.69 |
| 716 4.78 | 852 0.68 |
| 720 7.08 | 856 0.67 |
| 724 10.51 | 860 0.66 |
| 728 10.74 | 864 0.65 |
| 732 8.19 | 868 0.64 |
| 736 5.93 | 872 0.63 |
| 740 4.85 | 876 0.62 |
| 744 4.09 | 880 0.61 |
| 748 3.31 | 884 0.60 |
| 752 2.53 | 888 0.59 |
| 756 1.92 | 892 0.58 |
| 760 1.62 | 896 0.57 |
| 764 1.49 | |
| 768 1.41 | |
| 772 1.32 | ...End |
| 776 1.24 | |
| 780 1.16 | |
| 784 1.08 | |

Hydrograph Report

Hyd. No. 7

Post Subarea 3b

| | | | |
|-----------------|--------------|--------------------|------------|
| Hydrograph type | = SCS Runoff | Peak discharge | = 0.50 cfs |
| Storm frequency | = 10 yrs | Time interval | = 2 min |
| Drainage area | = 0.35 ac | Curve number | = 61 |
| Basin Slope | = 0.0 % | Hydraulic length | = 0 ft |
| Tc method | = USER | Time of conc. (Tc) | = 6 min |
| Total precip. | = 5.00 in | Distribution | = Type III |
| Storm duration | = 24 hrs | Shape factor | = 484 |

Hydrograph Volume = 1,631 cuft

Hydrograph Discharge Table

| Time (min) | Outflow (cfs) | Time (min) | Outflow (cfs) |
|------------|---------------|------------|---------------|
| 700 | 0.03 | 836 | 0.04 |
| 704 | 0.05 | 840 | 0.04 |
| 708 | 0.07 | 844 | 0.04 |
| 712 | 0.11 | 848 | 0.04 |
| 716 | 0.15 | 852 | 0.04 |
| 720 | 0.32 | 856 | 0.04 |
| 724 | 0.50 << | 860 | 0.04 |
| 728 | 0.40 | 864 | 0.04 |
| 732 | 0.28 | 868 | 0.04 |
| 736 | 0.25 | 872 | 0.04 |
| 740 | 0.22 | 876 | 0.04 |
| 744 | 0.19 | 880 | 0.04 |
| 748 | 0.15 | 884 | 0.04 |
| 752 | 0.11 | 888 | 0.04 |
| 756 | 0.09 | 892 | 0.03 |
| 760 | 0.08 | 896 | 0.03 |
| 764 | 0.08 | 900 | 0.03 |
| 768 | 0.07 | 904 | 0.03 |
| 772 | 0.07 | 908 | 0.03 |
| 776 | 0.07 | 912 | 0.03 |
| 780 | 0.06 | 916 | 0.03 |
| 784 | 0.06 | 920 | 0.03 |
| 788 | 0.06 | 924 | 0.03 |
| 792 | 0.06 | 928 | 0.03 |
| 796 | 0.05 | 932 | 0.03 |
| 800 | 0.05 | 936 | 0.03 |
| 804 | 0.05 | 940 | 0.03 |
| 808 | 0.05 | 944 | 0.03 |
| 812 | 0.05 | 948 | 0.03 |
| 816 | 0.05 | 952 | 0.03 |
| 820 | 0.05 | 956 | 0.02 |
| 824 | 0.05 | | |
| 828 | 0.05 | | |
| 832 | 0.05 | ...End | |

Hydrograph Report

Hyd. No. 8

Basin 1 In

Hydrograph type = Combine
Storm frequency = 10 yrs
Inflow hyds. = 2, 3

Peak discharge = 6.52 cfs
Time interval = 2 min

Hydrograph Volume = 25,260 cuft

Hydrograph Discharge Table

| Time (min) | Hyd. 2 + (cfs) | Hyd. 3 + (cfs) | Outflow (cfs) |
|------------|----------------|----------------|---------------|
| 648 | 0.33 | 0.00 | 0.33 |
| 652 | 0.34 | 0.00 | 0.34 |
| 656 | 0.36 | 0.00 | 0.36 |
| 660 | 0.37 | 0.00 | 0.37 |
| 664 | 0.39 | 0.00 | 0.39 |
| 668 | 0.41 | 0.00 | 0.41 |
| 672 | 0.44 | 0.00 | 0.44 |
| 676 | 0.48 | 0.00 | 0.48 |
| 680 | 0.52 | 0.00 | 0.52 |
| 684 | 0.56 | 0.01 | 0.57 |
| 688 | 0.61 | 0.01 | 0.62 |
| 692 | 0.66 | 0.01 | 0.67 |
| 696 | 0.76 | 0.01 | 0.77 |
| 700 | 0.96 | 0.02 | 0.99 |
| 704 | 1.27 | 0.04 | 1.31 |
| 708 | 1.66 | 0.06 | 1.72 |
| 712 | 2.11 | 0.08 | 2.19 |
| 716 | 2.62 | 0.12 | 2.74 |
| 720 | 3.62 | 0.25 | 3.87 |
| 724 | 5.26 | 0.40 << | 5.65 |
| 728 | 6.21 << | 0.32 | 6.52 << |
| 732 | 5.75 | 0.23 | 5.97 |
| 736 | 4.72 | 0.20 | 4.92 |
| 740 | 3.63 | 0.18 | 3.81 |
| 744 | 2.88 | 0.15 | 3.03 |
| 748 | 2.38 | 0.12 | 2.50 |
| 752 | 1.90 | 0.09 | 1.98 |
| 756 | 1.47 | 0.07 | 1.54 |
| 760 | 1.17 | 0.07 | 1.24 |
| 764 | 1.00 | 0.06 | 1.07 |
| 768 | 0.91 | 0.06 | 0.97 |
| 772 | 0.86 | 0.06 | 0.91 |
| 776 | 0.81 | 0.05 | 0.86 |
| 780 | 0.75 | 0.05 | 0.80 |
| 784 | 0.70 | 0.05 | 0.75 |
| 788 | 0.66 | 0.05 | 0.71 |
| 792 | 0.63 | 0.04 | 0.68 |
| 796 | 0.61 | 0.04 | 0.66 |

Continues on next page...

Hydrograph Discharge Table

| Time (min) | Hyd. 2 + (cfs) | Hyd. 3 + (cfs) | Outflow (cfs) |
|-----------------------|---------------------------|---------------------------|--------------------------|
| 800 | 0.60 | 0.04 | 0.64 |
| 804 | 0.59 | 0.04 | 0.63 |
| 808 | 0.57 | 0.04 | 0.62 |
| 812 | 0.56 | 0.04 | 0.60 |
| 816 | 0.55 | 0.04 | 0.59 |
| 820 | 0.53 | 0.04 | 0.57 |
| 824 | 0.52 | 0.04 | 0.56 |
| 828 | 0.51 | 0.04 | 0.54 |
| 832 | 0.49 | 0.04 | 0.53 |
| 836 | 0.48 | 0.04 | 0.51 |
| 840 | 0.46 | 0.03 | 0.50 |
| 844 | 0.45 | 0.03 | 0.48 |
| 848 | 0.44 | 0.03 | 0.47 |
| 852 | 0.43 | 0.03 | 0.46 |
| 856 | 0.42 | 0.03 | 0.45 |
| 860 | 0.42 | 0.03 | 0.45 |
| 864 | 0.41 | 0.03 | 0.44 |
| 868 | 0.40 | 0.03 | 0.43 |
| 872 | 0.40 | 0.03 | 0.43 |
| 876 | 0.39 | 0.03 | 0.42 |
| 880 | 0.38 | 0.03 | 0.41 |
| 884 | 0.38 | 0.03 | 0.41 |
| 888 | 0.37 | 0.03 | 0.40 |
| 892 | 0.36 | 0.03 | 0.39 |
| 896 | 0.36 | 0.03 | 0.38 |
| 900 | 0.35 | 0.03 | 0.38 |
| 904 | 0.34 | 0.03 | 0.37 |
| 908 | 0.34 | 0.03 | 0.36 |
| 912 | 0.33 | 0.03 | 0.36 |
| 916 | 0.32 | 0.03 | 0.35 |
| 920 | 0.32 | 0.02 | 0.34 |
| 924 | 0.31 | 0.02 | 0.33 |
| 928 | 0.30 | 0.02 | 0.33 |

...End

Hydrograph Report

Hyd. No. 9

Basin 2 In

Hydrograph type = Combine
Storm frequency = 10 yrs
Inflow hyds. = 4, 5

Peak discharge = 7.51 cfs
Time interval = 2 min

Hydrograph Volume = 31,384 cuft

Hydrograph Discharge Table

| Time (min) | Hyd. 4 + (cfs) | Hyd. 5 + (cfs) | Outflow (cfs) |
|------------|----------------|----------------|---------------|
| 632 | 0.39 | 0.00 | 0.39 |
| 636 | 0.40 | 0.00 | 0.40 |
| 640 | 0.42 | 0.00 | 0.42 |
| 644 | 0.43 | 0.00 | 0.43 |
| 648 | 0.45 | 0.00 | 0.45 |
| 652 | 0.47 | 0.00 | 0.47 |
| 656 | 0.48 | 0.00 | 0.48 |
| 660 | 0.50 | 0.00 | 0.50 |
| 664 | 0.52 | 0.00 | 0.52 |
| 668 | 0.54 | 0.00 | 0.54 |
| 672 | 0.58 | 0.00 | 0.58 |
| 676 | 0.62 | 0.00 | 0.62 |
| 680 | 0.67 | 0.00 | 0.68 |
| 684 | 0.73 | 0.00 | 0.73 |
| 688 | 0.78 | 0.01 | 0.79 |
| 692 | 0.85 | 0.01 | 0.86 |
| 696 | 0.95 | 0.01 | 0.96 |
| 700 | 1.15 | 0.02 | 1.18 |
| 704 | 1.48 | 0.04 | 1.52 |
| 708 | 1.92 | 0.06 | 1.98 |
| 712 | 2.44 | 0.08 | 2.53 |
| 716 | 3.05 | 0.12 | 3.17 |
| 720 | 4.06 | 0.24 | 4.31 |
| 724 | 5.66 | 0.38 << | 6.05 |
| 728 | 7.03 | 0.31 | 7.33 |
| 732 | 7.15 | 0.22 | 7.37 |
| 736 | 6.32 | 0.19 | 6.51 |
| 740 | 5.20 | 0.17 | 5.37 |
| 744 | 4.04 | 0.14 | 4.19 |
| 748 | 3.20 | 0.11 | 3.31 |
| 752 | 2.59 | 0.08 | 2.68 |
| 756 | 2.05 | 0.07 | 2.12 |
| 760 | 1.62 | 0.06 | 1.68 |
| 764 | 1.34 | 0.06 | 1.40 |
| 768 | 1.17 | 0.06 | 1.22 |
| 772 | 1.07 | 0.05 | 1.12 |
| 776 | 1.00 | 0.05 | 1.06 |
| 780 | 0.94 | 0.05 | 0.99 |

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Hydrograph Discharge Table

| Time (min) | Hyd. 4 + (cfs) | Hyd. 5 + (cfs) | Outflow (cfs) |
|-----------------------|---------------------------|---------------------------|--------------------------|
| 784 | 0.88 | 0.05 | 0.92 |
| 788 | 0.83 | 0.04 | 0.87 |
| 792 | 0.78 | 0.04 | 0.83 |
| 796 | 0.75 | 0.04 | 0.80 |
| 800 | 0.73 | 0.04 | 0.77 |
| 804 | 0.71 | 0.04 | 0.75 |
| 808 | 0.70 | 0.04 | 0.74 |
| 812 | 0.68 | 0.04 | 0.72 |
| 816 | 0.66 | 0.04 | 0.70 |
| 820 | 0.65 | 0.04 | 0.69 |
| 824 | 0.63 | 0.04 | 0.67 |
| 828 | 0.62 | 0.04 | 0.65 |
| 832 | 0.60 | 0.03 | 0.63 |
| 836 | 0.58 | 0.03 | 0.62 |
| 840 | 0.57 | 0.03 | 0.60 |
| 844 | 0.55 | 0.03 | 0.58 |
| 848 | 0.53 | 0.03 | 0.57 |
| 852 | 0.52 | 0.03 | 0.55 |
| 856 | 0.51 | 0.03 | 0.54 |
| 860 | 0.50 | 0.03 | 0.53 |
| 864 | 0.49 | 0.03 | 0.52 |
| 868 | 0.49 | 0.03 | 0.52 |
| 872 | 0.48 | 0.03 | 0.51 |
| 876 | 0.47 | 0.03 | 0.50 |
| 880 | 0.46 | 0.03 | 0.49 |
| 884 | 0.45 | 0.03 | 0.48 |
| 888 | 0.45 | 0.03 | 0.47 |
| 892 | 0.44 | 0.03 | 0.47 |
| 896 | 0.43 | 0.03 | 0.46 |
| 900 | 0.42 | 0.03 | 0.45 |
| 904 | 0.41 | 0.03 | 0.44 |
| 908 | 0.41 | 0.03 | 0.43 |
| 912 | 0.40 | 0.02 | 0.42 |
| 916 | 0.39 | 0.02 | 0.41 |
| 920 | 0.38 | 0.02 | 0.41 |
| 924 | 0.37 | 0.02 | 0.40 |
| 928 | 0.37 | 0.02 | 0.39 |
| 932 | 0.36 | 0.02 | 0.38 |

...End

Hydrograph Report

Hyd. No. 10

Basin 3 In

Hydrograph type = Combine
Storm frequency = 10 yrs
Inflow hyds. = 6, 7

Peak discharge = 11.65 cfs
Time interval = 2 min

Hydrograph Volume = 40,143 cuft

Hydrograph Discharge Table

| Time (min) | Hyd. 6 + (cfs) | Hyd. 7 + (cfs) | Outflow (cfs) |
|------------|----------------|----------------|---------------|
| 656 | 0.59 | 0.00 | 0.59 |
| 660 | 0.61 | 0.00 | 0.61 |
| 664 | 0.64 | 0.00 | 0.64 |
| 668 | 0.68 | 0.00 | 0.68 |
| 672 | 0.74 | 0.00 | 0.74 |
| 676 | 0.81 | 0.00 | 0.81 |
| 680 | 0.88 | 0.00 | 0.89 |
| 684 | 0.95 | 0.01 | 0.96 |
| 688 | 1.03 | 0.01 | 1.04 |
| 692 | 1.12 | 0.01 | 1.13 |
| 696 | 1.34 | 0.02 | 1.36 |
| 700 | 1.80 | 0.03 | 1.84 |
| 704 | 2.43 | 0.05 | 2.48 |
| 708 | 3.13 | 0.07 | 3.20 |
| 712 | 3.88 | 0.11 | 3.98 |
| 716 | 4.78 | 0.15 | 4.93 |
| 720 | 7.08 | 0.32 | 7.39 |
| 724 | 10.51 | 0.50 << | 11.01 |
| 728 | 10.74 | 0.40 | 11.14 |
| 732 | 8.19 | 0.28 | 8.47 |
| 736 | 5.93 | 0.25 | 6.18 |
| 740 | 4.85 | 0.22 | 5.07 |
| 744 | 4.09 | 0.19 | 4.27 |
| 748 | 3.31 | 0.15 | 3.45 |
| 752 | 2.53 | 0.11 | 2.64 |
| 756 | 1.92 | 0.09 | 2.01 |
| 760 | 1.62 | 0.08 | 1.70 |
| 764 | 1.49 | 0.08 | 1.57 |
| 768 | 1.41 | 0.07 | 1.48 |
| 772 | 1.32 | 0.07 | 1.40 |
| 776 | 1.24 | 0.07 | 1.31 |
| 780 | 1.16 | 0.06 | 1.22 |
| 784 | 1.08 | 0.06 | 1.14 |
| 788 | 1.03 | 0.06 | 1.08 |
| 792 | 0.99 | 0.06 | 1.05 |
| 796 | 0.97 | 0.05 | 1.03 |
| 800 | 0.95 | 0.05 | 1.00 |
| 804 | 0.93 | 0.05 | 0.98 |

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Hydrograph Discharge Table

| Time (min) | Hyd. 6 + (cfs) | Hyd. 7 + (cfs) | Outflow (cfs) |
|-----------------------|---------------------------|---------------------------|--------------------------|
| 808 | 0.91 | 0.05 | 0.96 |
| 812 | 0.89 | 0.05 | 0.94 |
| 816 | 0.86 | 0.05 | 0.91 |
| 820 | 0.84 | 0.05 | 0.89 |
| 824 | 0.82 | 0.05 | 0.87 |
| 828 | 0.80 | 0.05 | 0.84 |
| 832 | 0.78 | 0.05 | 0.82 |
| 836 | 0.75 | 0.04 | 0.80 |
| 840 | 0.73 | 0.04 | 0.78 |
| 844 | 0.71 | 0.04 | 0.75 |
| 848 | 0.69 | 0.04 | 0.74 |
| 852 | 0.68 | 0.04 | 0.72 |
| 856 | 0.67 | 0.04 | 0.71 |
| 860 | 0.66 | 0.04 | 0.70 |
| 864 | 0.65 | 0.04 | 0.69 |
| 868 | 0.64 | 0.04 | 0.68 |
| 872 | 0.63 | 0.04 | 0.67 |
| 876 | 0.62 | 0.04 | 0.66 |
| 880 | 0.61 | 0.04 | 0.65 |
| 884 | 0.60 | 0.04 | 0.63 |
| 888 | 0.59 | 0.04 | 0.62 |
| 892 | 0.58 | 0.03 | 0.61 |
| 896 | 0.57 | 0.03 | 0.60 |
| 900 | 0.56 | 0.03 | 0.59 |

...End

Hydrograph Report

Hyd. No. 11

Basin 1 Out

Hydrograph type = Reservoir
 Storm frequency = 10 yrs
 Inflow hyd. No. = 8
 Max. Elevation = 242.34 ft

Peak discharge = 0.35 cfs
 Time interval = 2 min
 Reservoir name = Retention Basin N
 Max. Storage = 26,745 cuft

Storage Indication method used.

Outflow hydrograph volume = 24,998 cuft

Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 544 | 0.11 | 240.06 | 23.09 | 0.02 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.02 |
| 548 | 0.12 | 240.06 | 23.09 | 0.02 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.02 |
| 552 | 0.12 | 240.06 | 23.09 | 0.02 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.02 |
| 556 | 0.13 | 240.07 | 23.09 | 0.02 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.02 |
| 560 | 0.13 | 240.07 | 23.09 | 0.02 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.02 |
| 564 | 0.14 | 240.08 | 23.09 | 0.02 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.02 |
| 568 | 0.15 | 240.08 | 23.09 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.03 |
| 572 | 0.15 | 240.08 | 23.09 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.03 |
| 576 | 0.16 | 240.09 | 23.09 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.03 |
| 580 | 0.16 | 240.09 | 23.09 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.03 |
| 584 | 0.17 | 240.10 | 23.09 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.03 |
| 588 | 0.18 | 240.10 | 23.09 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.03 |
| 592 | 0.18 | 240.11 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 596 | 0.19 | 240.11 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 600 | 0.20 | 240.12 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 604 | 0.20 | 240.13 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 608 | 0.21 | 240.13 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 612 | 0.22 | 240.14 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 616 | 0.23 | 240.14 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 620 | 0.24 | 240.15 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 624 | 0.26 | 240.16 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 628 | 0.27 | 240.17 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 632 | 0.28 | 240.17 | 23.09 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |
| 636 | 0.29 | 240.18 | 23.09 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |
| 640 | 0.30 | 240.19 | 23.09 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |
| 644 | 0.32 | 240.20 | 23.09 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |
| 648 | 0.33 | 240.21 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 652 | 0.34 | 240.22 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 656 | 0.36 | 240.23 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 660 | 0.37 | 240.24 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 664 | 0.39 | 240.25 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 668 | 0.41 | 240.26 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 672 | 0.44 | 240.27 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 676 | 0.48 | 240.29 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 680 | 0.52 | 240.30 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 684 | 0.57 | 240.32 | 23.09 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 688 | 0.62 | 240.33 | 23.09 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 692 | 0.67 | 240.35 | 23.09 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.11 |

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Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 696 | 0.77 | 240.38 | 23.09 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.12 |
| 700 | 0.99 | 240.40 | 23.09 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.12 |
| 704 | 1.31 | 240.44 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 708 | 1.72 | 240.49 | 23.09 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 712 | 2.19 | 240.55 | 23.09 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 716 | 2.74 | 240.64 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 720 | 3.87 | 240.75 | 23.09 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 724 | 5.65 | 240.91 | 23.09 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 728 | 6.52 << | 241.12 | 23.09 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 732 | 5.97 | 241.34 | 23.09 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 736 | 4.92 | 241.53 | 23.09 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 740 | 3.81 | 241.67 | 23.09 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 744 | 3.03 | 241.79 | 23.09 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 748 | 2.50 | 241.87 | 23.09 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 752 | 1.98 | 241.94 | 23.09 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 756 | 1.54 | 241.99 | 23.09 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 760 | 1.24 | 242.03 | 23.09 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 764 | 1.07 | 242.06 | 23.09 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 768 | 0.97 | 242.09 | 23.09 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 772 | 0.91 | 242.11 | 23.09 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 776 | 0.86 | 242.13 | 23.09 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 780 | 0.80 | 242.15 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 784 | 0.75 | 242.16 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 788 | 0.71 | 242.18 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 792 | 0.68 | 242.19 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 796 | 0.66 | 242.20 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 800 | 0.64 | 242.21 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 804 | 0.63 | 242.22 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 808 | 0.62 | 242.23 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 812 | 0.60 | 242.24 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 816 | 0.59 | 242.25 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 820 | 0.57 | 242.26 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 824 | 0.56 | 242.27 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 828 | 0.54 | 242.27 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 832 | 0.53 | 242.28 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 836 | 0.51 | 242.29 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 840 | 0.50 | 242.29 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 844 | 0.48 | 242.30 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 848 | 0.47 | 242.30 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 852 | 0.46 | 242.31 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 856 | 0.45 | 242.31 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 860 | 0.45 | 242.31 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 864 | 0.44 | 242.32 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 868 | 0.43 | 242.32 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 872 | 0.43 | 242.32 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 876 | 0.42 | 242.33 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 880 | 0.41 | 242.33 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 884 | 0.41 | 242.33 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 888 | 0.40 | 242.33 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 892 | 0.39 | 242.33 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 896 | 0.38 | 242.34 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |

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Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 900 | 0.38 | 242.34 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 904 | 0.37 | 242.34 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 908 | 0.36 | 242.34 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 912 | 0.36 | 242.34 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 916 | 0.35 | 242.34 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 920 | 0.34 | 242.34 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 924 | 0.33 | 242.34 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 928 | 0.33 | 242.34 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 932 | 0.32 | 242.34 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 936 | 0.31 | 242.33 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 940 | 0.30 | 242.33 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 944 | 0.30 | 242.33 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 948 | 0.29 | 242.33 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 952 | 0.28 | 242.33 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 956 | 0.28 | 242.32 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 960 | 0.27 | 242.32 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 964 | 0.26 | 242.32 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 968 | 0.26 | 242.32 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 972 | 0.25 | 242.31 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 976 | 0.25 | 242.31 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 980 | 0.24 | 242.30 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 984 | 0.24 | 242.30 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 988 | 0.24 | 242.30 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 992 | 0.23 | 242.29 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 996 | 0.23 | 242.29 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1000 | 0.23 | 242.28 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1004 | 0.22 | 242.28 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1008 | 0.22 | 242.28 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1012 | 0.22 | 242.27 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1016 | 0.21 | 242.27 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1020 | 0.21 | 242.26 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1024 | 0.21 | 242.26 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1028 | 0.21 | 242.25 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1032 | 0.20 | 242.25 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1036 | 0.20 | 242.24 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1040 | 0.20 | 242.24 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1044 | 0.19 | 242.23 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1048 | 0.19 | 242.23 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1052 | 0.19 | 242.22 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1056 | 0.18 | 242.21 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1060 | 0.18 | 242.21 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1064 | 0.18 | 242.20 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1068 | 0.17 | 242.20 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1072 | 0.17 | 242.19 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1076 | 0.17 | 242.18 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1080 | 0.16 | 242.18 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1084 | 0.16 | 242.17 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1088 | 0.16 | 242.17 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1092 | 0.16 | 242.16 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1096 | 0.16 | 242.15 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1100 | 0.15 | 242.15 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |

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Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 1104 | 0.15 | 242.14 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1108 | 0.15 | 242.13 | 23.09 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1112 | 0.15 | 242.13 | 23.09 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1116 | 0.15 | 242.12 | 23.09 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1120 | 0.15 | 242.11 | 23.09 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1124 | 0.15 | 242.11 | 23.09 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1128 | 0.15 | 242.10 | 23.09 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1132 | 0.15 | 242.09 | 23.09 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1136 | 0.15 | 242.09 | 23.09 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1140 | 0.14 | 242.08 | 23.09 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1144 | 0.14 | 242.07 | 23.09 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1148 | 0.14 | 242.07 | 23.09 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1152 | 0.14 | 242.06 | 23.09 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1156 | 0.14 | 242.05 | 23.09 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1160 | 0.14 | 242.05 | 23.09 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1164 | 0.14 | 242.04 | 23.09 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1168 | 0.14 | 242.03 | 23.09 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1172 | 0.14 | 242.03 | 23.09 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1176 | 0.14 | 242.02 | 23.09 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1180 | 0.13 | 242.01 | 23.09 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1184 | 0.13 | 242.01 | 23.09 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1188 | 0.13 | 242.00 | 23.09 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1192 | 0.13 | 241.99 | 23.09 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1196 | 0.13 | 241.98 | 23.09 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1200 | 0.13 | 241.98 | 23.09 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1204 | 0.13 | 241.97 | 23.09 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1208 | 0.13 | 241.96 | 23.09 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1212 | 0.13 | 241.96 | 23.09 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1216 | 0.13 | 241.95 | 23.09 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1220 | 0.13 | 241.94 | 23.09 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1224 | 0.12 | 241.94 | 23.09 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1228 | 0.12 | 241.93 | 23.09 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1232 | 0.12 | 241.92 | 23.09 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1236 | 0.12 | 241.92 | 23.09 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1240 | 0.12 | 241.91 | 23.09 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1244 | 0.12 | 241.90 | 23.09 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1248 | 0.12 | 241.89 | 23.09 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1252 | 0.12 | 241.89 | 23.09 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1256 | 0.12 | 241.88 | 23.09 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1260 | 0.12 | 241.87 | 23.09 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1264 | 0.11 | 241.87 | 23.09 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1268 | 0.11 | 241.86 | 23.09 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1272 | 0.11 | 241.85 | 23.09 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1276 | 0.11 | 241.84 | 23.09 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1280 | 0.11 | 241.84 | 23.09 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1284 | 0.11 | 241.83 | 23.09 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1288 | 0.11 | 241.82 | 23.09 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1292 | 0.11 | 241.82 | 23.09 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1296 | 0.11 | 241.81 | 23.09 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1300 | 0.11 | 241.80 | 23.09 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1304 | 0.10 | 241.79 | 23.09 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |

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Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 1308 | 0.10 | 241.79 | 23.09 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1312 | 0.10 | 241.78 | 23.09 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1316 | 0.10 | 241.77 | 23.09 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1320 | 0.10 | 241.77 | 23.09 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1324 | 0.13 | 241.76 | 23.09 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1328 | 0.14 | 241.75 | 23.09 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1332 | 0.13 | 241.75 | 23.09 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1336 | 0.12 | 241.74 | 23.09 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1340 | 0.11 | 241.73 | 23.09 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1344 | 0.10 | 241.73 | 23.09 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1348 | 0.10 | 241.72 | 23.09 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1352 | 0.10 | 241.71 | 23.09 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1356 | 0.10 | 241.71 | 23.09 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1360 | 0.10 | 241.70 | 23.09 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1364 | 0.10 | 241.69 | 23.09 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1368 | 0.10 | 241.69 | 23.09 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1372 | 0.10 | 241.68 | 23.09 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1376 | 0.10 | 241.67 | 23.09 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1380 | 0.10 | 241.66 | 23.09 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1384 | 0.10 | 241.66 | 23.09 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1388 | 0.10 | 241.65 | 23.09 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1392 | 0.09 | 241.64 | 23.09 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1396 | 0.09 | 241.64 | 23.09 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1400 | 0.09 | 241.63 | 23.09 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1404 | 0.09 | 241.62 | 23.09 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1408 | 0.09 | 241.61 | 23.09 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1412 | 0.09 | 241.61 | 23.09 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1416 | 0.09 | 241.60 | 23.09 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1420 | 0.09 | 241.59 | 23.09 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1424 | 0.09 | 241.59 | 23.09 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1428 | 0.09 | 241.58 | 23.09 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 1432 | 0.09 | 241.57 | 23.09 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 1436 | 0.09 | 241.57 | 23.09 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 1440 | 0.09 | 241.56 | 23.09 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 1444 | 0.07 | 241.55 | 23.09 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 1448 | 0.04 | 241.54 | 23.09 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 1452 | 0.02 | 241.53 | 23.09 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 1456 | 0.01 | 241.52 | 23.09 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 1460 | 0.00 | 241.51 | 23.09 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 1464 | 0.00 | 241.50 | 23.09 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 1468 | 0.00 | 241.49 | 23.09 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 1472 | 0.00 | 241.48 | 23.09 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 1476 | 0.00 | 241.47 | 23.09 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 1480 | 0.00 | 241.46 | 23.09 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 1484 | 0.00 | 241.45 | 23.09 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 1488 | 0.00 | 241.45 | 23.09 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 1492 | 0.00 | 241.44 | 23.09 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 1496 | 0.00 | 241.43 | 23.09 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 1500 | 0.00 | 241.42 | 23.09 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 1504 | 0.00 | 241.41 | 23.09 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 1508 | 0.00 | 241.40 | 23.09 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |

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Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 1512 | 0.00 | 241.39 | 23.09 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 1516 | 0.00 | 241.38 | 23.09 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 1520 | 0.00 | 241.37 | 23.09 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 1524 | 0.00 | 241.36 | 23.09 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 1528 | 0.00 | 241.35 | 23.09 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 1532 | 0.00 | 241.34 | 23.09 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 1536 | 0.00 | 241.33 | 23.09 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 1540 | 0.00 | 241.32 | 23.09 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 1544 | 0.00 | 241.31 | 23.09 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 1548 | 0.00 | 241.30 | 23.09 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 1552 | 0.00 | 241.29 | 23.09 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 1556 | 0.00 | 241.28 | 23.09 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 1560 | 0.00 | 241.28 | 23.09 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 1564 | 0.00 | 241.27 | 23.09 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 1568 | 0.00 | 241.26 | 23.09 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 1572 | 0.00 | 241.25 | 23.09 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 1576 | 0.00 | 241.24 | 23.09 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 1580 | 0.00 | 241.23 | 23.09 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 1584 | 0.00 | 241.22 | 23.09 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 1588 | 0.00 | 241.21 | 23.09 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 1592 | 0.00 | 241.20 | 23.09 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 1596 | 0.00 | 241.19 | 23.09 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 1600 | 0.00 | 241.19 | 23.09 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 1604 | 0.00 | 241.18 | 23.09 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 1608 | 0.00 | 241.17 | 23.09 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 1612 | 0.00 | 241.16 | 23.09 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 1616 | 0.00 | 241.15 | 23.09 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 1620 | 0.00 | 241.14 | 23.09 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 1624 | 0.00 | 241.13 | 23.09 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 1628 | 0.00 | 241.13 | 23.09 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 1632 | 0.00 | 241.12 | 23.09 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 1636 | 0.00 | 241.11 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 1640 | 0.00 | 241.10 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 1644 | 0.00 | 241.09 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 1648 | 0.00 | 241.08 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 1652 | 0.00 | 241.08 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 1656 | 0.00 | 241.07 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 1660 | 0.00 | 241.06 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 1664 | 0.00 | 241.05 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 1668 | 0.00 | 241.04 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 1672 | 0.00 | 241.03 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 1676 | 0.00 | 241.03 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 1680 | 0.00 | 241.02 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 1684 | 0.00 | 241.01 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 1688 | 0.00 | 241.00 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 1692 | 0.00 | 240.99 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 1696 | 0.00 | 240.99 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 1700 | 0.00 | 240.98 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 1704 | 0.00 | 240.97 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 1708 | 0.00 | 240.96 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 1712 | 0.00 | 240.96 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |

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Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 1716 | 0.00 | 240.95 | 23.09 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 1720 | 0.00 | 240.94 | 23.09 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 1724 | 0.00 | 240.93 | 23.09 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 1728 | 0.00 | 240.92 | 23.09 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 1732 | 0.00 | 240.92 | 23.09 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 1736 | 0.00 | 240.91 | 23.09 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 1740 | 0.00 | 240.90 | 23.09 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 1744 | 0.00 | 240.89 | 23.09 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 1748 | 0.00 | 240.89 | 23.09 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 1752 | 0.00 | 240.88 | 23.09 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 1756 | 0.00 | 240.87 | 23.09 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 1760 | 0.00 | 240.87 | 23.09 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 1764 | 0.00 | 240.86 | 23.09 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 1768 | 0.00 | 240.85 | 23.09 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 1772 | 0.00 | 240.84 | 23.09 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 1776 | 0.00 | 240.84 | 23.09 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 1780 | 0.00 | 240.83 | 23.09 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 1784 | 0.00 | 240.82 | 23.09 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 1788 | 0.00 | 240.82 | 23.09 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 1792 | 0.00 | 240.81 | 23.09 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 1796 | 0.00 | 240.80 | 23.09 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 1800 | 0.00 | 240.79 | 23.09 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 1804 | 0.00 | 240.79 | 23.09 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 1808 | 0.00 | 240.78 | 23.09 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 1812 | 0.00 | 240.77 | 23.09 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 1816 | 0.00 | 240.77 | 23.09 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 1820 | 0.00 | 240.76 | 23.09 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 1824 | 0.00 | 240.75 | 23.09 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 1828 | 0.00 | 240.75 | 23.09 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 1832 | 0.00 | 240.74 | 23.09 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 1836 | 0.00 | 240.73 | 23.09 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 1840 | 0.00 | 240.73 | 23.09 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 1844 | 0.00 | 240.72 | 23.09 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 1848 | 0.00 | 240.71 | 23.09 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 1852 | 0.00 | 240.71 | 23.09 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 1856 | 0.00 | 240.70 | 23.09 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 1860 | 0.00 | 240.69 | 23.09 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 1864 | 0.00 | 240.69 | 23.09 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 1868 | 0.00 | 240.68 | 23.09 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 1872 | 0.00 | 240.68 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 1876 | 0.00 | 240.67 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 1880 | 0.00 | 240.66 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 1884 | 0.00 | 240.66 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 1888 | 0.00 | 240.65 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 1892 | 0.00 | 240.64 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 1896 | 0.00 | 240.64 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 1900 | 0.00 | 240.63 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 1904 | 0.00 | 240.63 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 1908 | 0.00 | 240.62 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 1912 | 0.00 | 240.61 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 1916 | 0.00 | 240.61 | 23.09 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |

Continues on next page...

Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 1920 | 0.00 | 240.60 | 23.09 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |
| 1924 | 0.00 | 240.60 | 23.09 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |
| 1928 | 0.00 | 240.59 | 23.09 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |
| 1932 | 0.00 | 240.59 | 23.09 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |
| 1936 | 0.00 | 240.58 | 23.09 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |
| 1940 | 0.00 | 240.57 | 23.09 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |
| 1944 | 0.00 | 240.57 | 23.09 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |
| 1948 | 0.00 | 240.56 | 23.09 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |
| 1952 | 0.00 | 240.56 | 23.09 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 1956 | 0.00 | 240.55 | 23.09 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 1960 | 0.00 | 240.55 | 23.09 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 1964 | 0.00 | 240.54 | 23.09 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 1968 | 0.00 | 240.53 | 23.09 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 1972 | 0.00 | 240.53 | 23.09 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 1976 | 0.00 | 240.52 | 23.09 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 1980 | 0.00 | 240.52 | 23.09 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 1984 | 0.00 | 240.51 | 23.09 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 1988 | 0.00 | 240.51 | 23.09 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 1992 | 0.00 | 240.50 | 23.09 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 1996 | 0.00 | 240.50 | 23.09 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 2000 | 0.00 | 240.49 | 23.09 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 2004 | 0.00 | 240.49 | 23.09 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 2008 | 0.00 | 240.48 | 23.09 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 2012 | 0.00 | 240.48 | 23.09 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 2016 | 0.00 | 240.47 | 23.09 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 2020 | 0.00 | 240.47 | 23.09 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 2024 | 0.00 | 240.46 | 23.09 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 2028 | 0.00 | 240.46 | 23.09 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 2032 | 0.00 | 240.45 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 2036 | 0.00 | 240.45 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 2040 | 0.00 | 240.44 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 2044 | 0.00 | 240.44 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 2048 | 0.00 | 240.43 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 2052 | 0.00 | 240.43 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 2056 | 0.00 | 240.42 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 2060 | 0.00 | 240.42 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 2064 | 0.00 | 240.42 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 2068 | 0.00 | 240.41 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 2072 | 0.00 | 240.41 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 2076 | 0.00 | 240.40 | 23.09 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.12 |
| 2080 | 0.00 | 240.40 | 23.09 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.12 |
| 2084 | 0.00 | 240.39 | 23.09 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.12 |
| 2088 | 0.00 | 240.39 | 23.09 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.12 |
| 2092 | 0.00 | 240.38 | 23.09 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.12 |
| 2096 | 0.00 | 240.38 | 23.09 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.12 |
| 2100 | 0.00 | 240.38 | 23.09 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.12 |
| 2104 | 0.00 | 240.37 | 23.09 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.12 |
| 2108 | 0.00 | 240.37 | 23.09 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.11 |
| 2112 | 0.00 | 240.36 | 23.09 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.11 |
| 2116 | 0.00 | 240.36 | 23.09 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.11 |
| 2120 | 0.00 | 240.36 | 23.09 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.11 |

Continues on next page...

Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 2124 | 0.00 | 240.35 | 23.09 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.11 |
| 2128 | 0.00 | 240.35 | 23.09 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.11 |
| 2132 | 0.00 | 240.34 | 23.09 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.11 |
| 2136 | 0.00 | 240.34 | 23.09 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.11 |
| 2140 | 0.00 | 240.34 | 23.09 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.11 |
| 2144 | 0.00 | 240.33 | 23.09 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 2148 | 0.00 | 240.33 | 23.09 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 2152 | 0.00 | 240.33 | 23.09 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 2156 | 0.00 | 240.32 | 23.09 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 2160 | 0.00 | 240.32 | 23.09 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 2164 | 0.00 | 240.31 | 23.09 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 2168 | 0.00 | 240.31 | 23.09 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 2172 | 0.00 | 240.31 | 23.09 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 2176 | 0.00 | 240.30 | 23.09 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 2180 | 0.00 | 240.30 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 2184 | 0.00 | 240.30 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 2188 | 0.00 | 240.29 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 2192 | 0.00 | 240.29 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 2196 | 0.00 | 240.29 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 2200 | 0.00 | 240.28 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 2204 | 0.00 | 240.28 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 2208 | 0.00 | 240.28 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 2212 | 0.00 | 240.27 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 2216 | 0.00 | 240.27 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 2220 | 0.00 | 240.27 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 2224 | 0.00 | 240.27 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 2228 | 0.00 | 240.26 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 2232 | 0.00 | 240.26 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 2236 | 0.00 | 240.26 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 2240 | 0.00 | 240.25 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 2244 | 0.00 | 240.25 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 2248 | 0.00 | 240.25 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 2252 | 0.00 | 240.24 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 2256 | 0.00 | 240.24 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 2260 | 0.00 | 240.24 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 2264 | 0.00 | 240.24 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 2268 | 0.00 | 240.23 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 2272 | 0.00 | 240.23 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 2276 | 0.00 | 240.23 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 2280 | 0.00 | 240.23 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 2284 | 0.00 | 240.22 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 2288 | 0.00 | 240.22 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 2292 | 0.00 | 240.22 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 2296 | 0.00 | 240.22 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 2300 | 0.00 | 240.21 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 2304 | 0.00 | 240.21 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 2308 | 0.00 | 240.21 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 2312 | 0.00 | 240.21 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 2316 | 0.00 | 240.20 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 2320 | 0.00 | 240.20 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 2324 | 0.00 | 240.20 | 23.09 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |

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Stage / Storage / Discharge Table

| Stage ft | Storage cuft | Elevation ft | Civ A cfs | Civ B cfs | Civ C cfs | Civ D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Total cfs |
|-------------|-----------------|-----------------|--------------|--------------|--------------|--------------|-------------|-------------|-------------|-------------|--------------|--------------|
| 6.40 | 40,516 | 244.40 | 23.09 | 0.49 | --- | --- | 5.52 | 0.00 | 13.48 | --- | --- | 19.48 |
| 6.60 | 41,851 | 244.60 | 27.65 | 0.12 | --- | --- | 3.92 | 3.29 | 20.31 | --- | --- | 27.64 |
| 6.80 | 43,187 | 244.80 | 27.92 | 0.05 | --- | --- | 2.40 | 10.00 | 15.47 | --- | --- | 27.92 |
| 7.00 | 44,523 | 245.00 | 28.07 | 0.03 | --- | --- | 1.86 | 12.37 | 13.75 | --- | --- | 28.02 |
| 7.20 | 45,859 | 245.20 | 28.21 | 0.02 | --- | --- | 1.58 | 13.73 | 12.83 | --- | --- | 28.16 |
| 7.40 | 47,195 | 245.40 | 28.34 | 0.02 | --- | --- | 1.40 | 14.64 | 12.28 | --- | --- | 28.34 |
| 7.60 | 48,530 | 245.60 | 28.47 | 0.01 | --- | --- | 1.28 | 15.27 | 11.88 | --- | --- | 28.43 |
| 7.80 | 49,866 | 245.80 | 28.60 | 0.01 | --- | --- | 1.18 | 15.60 | 11.49 | --- | --- | 28.28 |
| 8.00 | 51,202 | 246.00 | 28.73 | 0.01 | --- | --- | 1.11 | 15.96 | 11.27 | --- | --- | 28.34 |
| 8.05 | 51,536 | 246.05 | 28.76 | 0.01 | --- | --- | 1.10 | 16.14 | 11.30 | --- | --- | 28.55 |
| 8.10 | 51,870 | 246.10 | 28.79 | 0.01 | --- | --- | 1.09 | 16.28 | 11.29 | --- | --- | 28.67 |
| 8.15 | 52,204 | 246.15 | 28.82 | 0.01 | --- | --- | 1.08 | 16.37 | 11.27 | --- | --- | 28.72 |
| 8.20 | 52,538 | 246.20 | 28.86 | 0.01 | --- | --- | 1.06 | 16.40 | 11.20 | --- | --- | 28.68 |
| 8.25 | 52,872 | 246.25 | 28.89 | 0.01 | --- | --- | 1.05 | 16.38 | 11.10 | --- | --- | 28.53 |
| 8.30 | 53,206 | 246.30 | 28.92 | 0.01 | --- | --- | 1.02 | 16.28 | 10.96 | --- | --- | 28.28 |
| 8.35 | 53,540 | 246.35 | 28.95 | 0.01 | --- | --- | 1.00 | 16.06 | 10.74 | --- | --- | 27.80 |
| 8.40 | 53,874 | 246.40 | 28.98 | 0.01 | --- | --- | 1.01 | 16.54 | 11.00 | --- | --- | 28.56 |
| 8.45 | 54,208 | 246.45 | 29.01 | 0.01 | --- | --- | 0.98 | 16.25 | 10.74 | --- | --- | 27.98 |
| 8.50 | 54,542 | 246.50 | 29.05 | 0.01 | --- | --- | 0.98 | 16.46 | 10.82 | --- | --- | 28.27 |

...End

Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 880 | 0.49 | 232.32 | 6.68 | 0.26 | ---- | ---- | 0.42 | ---- | ---- | ---- | 0.043 | 0.72 |
| 884 | 0.48 | 232.32 | 6.68 | 0.26 | ---- | ---- | 0.40 | ---- | ---- | ---- | 0.043 | 0.70 |
| 888 | 0.47 | 232.31 | 6.68 | 0.26 | ---- | ---- | 0.39 | ---- | ---- | ---- | 0.043 | 0.69 |
| 892 | 0.47 | 232.30 | 6.68 | 0.26 | ---- | ---- | 0.37 | ---- | ---- | ---- | 0.043 | 0.67 |
| 896 | 0.46 | 232.29 | 6.68 | 0.25 | ---- | ---- | 0.36 | ---- | ---- | ---- | 0.043 | 0.66 |
| 900 | 0.45 | 232.28 | 6.68 | 0.25 | ---- | ---- | 0.35 | ---- | ---- | ---- | 0.043 | 0.64 |
| 904 | 0.44 | 232.28 | 6.68 | 0.25 | ---- | ---- | 0.33 | ---- | ---- | ---- | 0.043 | 0.63 |
| 908 | 0.43 | 232.27 | 6.68 | 0.25 | ---- | ---- | 0.32 | ---- | ---- | ---- | 0.043 | 0.61 |
| 912 | 0.42 | 232.26 | 6.68 | 0.25 | ---- | ---- | 0.31 | ---- | ---- | ---- | 0.043 | 0.60 |
| 916 | 0.41 | 232.25 | 6.68 | 0.25 | ---- | ---- | 0.29 | ---- | ---- | ---- | 0.043 | 0.59 |
| 920 | 0.41 | 232.25 | 6.68 | 0.25 | ---- | ---- | 0.28 | ---- | ---- | ---- | 0.043 | 0.57 |
| 924 | 0.40 | 232.24 | 6.68 | 0.25 | ---- | ---- | 0.27 | ---- | ---- | ---- | 0.043 | 0.56 |
| 928 | 0.39 | 232.23 | 6.68 | 0.25 | ---- | ---- | 0.26 | ---- | ---- | ---- | 0.043 | 0.55 |
| 932 | 0.38 | 232.23 | 6.68 | 0.25 | ---- | ---- | 0.25 | ---- | ---- | ---- | 0.043 | 0.54 |
| 936 | 0.37 | 232.22 | 6.68 | 0.25 | ---- | ---- | 0.24 | ---- | ---- | ---- | 0.043 | 0.53 |
| 940 | 0.36 | 232.22 | 6.68 | 0.25 | ---- | ---- | 0.22 | ---- | ---- | ---- | 0.043 | 0.51 |
| 944 | 0.35 | 232.21 | 6.68 | 0.25 | ---- | ---- | 0.21 | ---- | ---- | ---- | 0.043 | 0.50 |
| 948 | 0.35 | 232.20 | 6.68 | 0.25 | ---- | ---- | 0.20 | ---- | ---- | ---- | 0.043 | 0.49 |
| 952 | 0.34 | 232.20 | 6.68 | 0.24 | ---- | ---- | 0.19 | ---- | ---- | ---- | 0.043 | 0.48 |
| 956 | 0.33 | 232.19 | 6.68 | 0.24 | ---- | ---- | 0.19 | ---- | ---- | ---- | 0.043 | 0.48 |
| 960 | 0.32 | 232.19 | 6.68 | 0.24 | ---- | ---- | 0.18 | ---- | ---- | ---- | 0.043 | 0.47 |
| 964 | 0.31 | 232.18 | 6.68 | 0.24 | ---- | ---- | 0.18 | ---- | ---- | ---- | 0.043 | 0.46 |
| 968 | 0.30 | 232.17 | 6.68 | 0.24 | ---- | ---- | 0.17 | ---- | ---- | ---- | 0.043 | 0.46 |
| 972 | 0.30 | 232.17 | 6.68 | 0.24 | ---- | ---- | 0.17 | ---- | ---- | ---- | 0.043 | 0.45 |
| 976 | 0.29 | 232.16 | 6.68 | 0.24 | ---- | ---- | 0.16 | ---- | ---- | ---- | 0.043 | 0.44 |
| 980 | 0.29 | 232.16 | 6.68 | 0.24 | ---- | ---- | 0.15 | ---- | ---- | ---- | 0.043 | 0.44 |
| 984 | 0.28 | 232.15 | 6.68 | 0.24 | ---- | ---- | 0.15 | ---- | ---- | ---- | 0.043 | 0.43 |
| 988 | 0.28 | 232.15 | 6.68 | 0.24 | ---- | ---- | 0.14 | ---- | ---- | ---- | 0.043 | 0.42 |
| 992 | 0.28 | 232.14 | 6.68 | 0.24 | ---- | ---- | 0.14 | ---- | ---- | ---- | 0.043 | 0.42 |
| 996 | 0.27 | 232.13 | 6.68 | 0.24 | ---- | ---- | 0.13 | ---- | ---- | ---- | 0.043 | 0.41 |
| 1000 | 0.27 | 232.13 | 6.68 | 0.24 | ---- | ---- | 0.13 | ---- | ---- | ---- | 0.043 | 0.41 |
| 1004 | 0.27 | 232.12 | 6.68 | 0.24 | ---- | ---- | 0.12 | ---- | ---- | ---- | 0.043 | 0.40 |
| 1008 | 0.26 | 232.12 | 6.68 | 0.24 | ---- | ---- | 0.12 | ---- | ---- | ---- | 0.043 | 0.39 |
| 1012 | 0.26 | 232.11 | 6.68 | 0.23 | ---- | ---- | 0.11 | ---- | ---- | ---- | 0.042 | 0.39 |
| 1016 | 0.25 | 232.11 | 6.68 | 0.23 | ---- | ---- | 0.11 | ---- | ---- | ---- | 0.042 | 0.38 |
| 1020 | 0.25 | 232.10 | 6.68 | 0.23 | ---- | ---- | 0.10 | ---- | ---- | ---- | 0.042 | 0.38 |
| 1024 | 0.25 | 232.10 | 6.68 | 0.23 | ---- | ---- | 0.10 | ---- | ---- | ---- | 0.042 | 0.37 |
| 1028 | 0.24 | 232.09 | 6.68 | 0.23 | ---- | ---- | 0.09 | ---- | ---- | ---- | 0.042 | 0.37 |
| 1032 | 0.24 | 232.09 | 6.68 | 0.23 | ---- | ---- | 0.09 | ---- | ---- | ---- | 0.042 | 0.36 |
| 1036 | 0.24 | 232.08 | 6.68 | 0.23 | ---- | ---- | 0.08 | ---- | ---- | ---- | 0.042 | 0.36 |
| 1040 | 0.23 | 232.08 | 6.68 | 0.23 | ---- | ---- | 0.08 | ---- | ---- | ---- | 0.042 | 0.35 |
| 1044 | 0.23 | 232.07 | 6.68 | 0.23 | ---- | ---- | 0.07 | ---- | ---- | ---- | 0.042 | 0.35 |
| 1048 | 0.22 | 232.07 | 6.68 | 0.23 | ---- | ---- | 0.07 | ---- | ---- | ---- | 0.042 | 0.34 |
| 1052 | 0.22 | 232.07 | 6.68 | 0.23 | ---- | ---- | 0.06 | ---- | ---- | ---- | 0.042 | 0.34 |
| 1056 | 0.22 | 232.06 | 6.68 | 0.23 | ---- | ---- | 0.06 | ---- | ---- | ---- | 0.042 | 0.33 |
| 1060 | 0.21 | 232.06 | 6.68 | 0.23 | ---- | ---- | 0.06 | ---- | ---- | ---- | 0.042 | 0.33 |
| 1064 | 0.21 | 232.05 | 6.68 | 0.23 | ---- | ---- | 0.05 | ---- | ---- | ---- | 0.042 | 0.32 |
| 1068 | 0.21 | 232.05 | 6.68 | 0.23 | ---- | ---- | 0.05 | ---- | ---- | ---- | 0.042 | 0.32 |
| 1072 | 0.20 | 232.04 | 6.68 | 0.23 | ---- | ---- | 0.04 | ---- | ---- | ---- | 0.042 | 0.31 |
| 1076 | 0.20 | 232.04 | 6.68 | 0.23 | ---- | ---- | 0.04 | ---- | ---- | ---- | 0.042 | 0.31 |
| 1080 | 0.19 | 232.03 | 6.68 | 0.23 | ---- | ---- | 0.03 | ---- | ---- | ---- | 0.042 | 0.30 |

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Reservoir Report

Reservoir No. 2 - Detention Basin 2

Hydraflow Hydrographs by Intelisolve

Pond Data

Pond storage is based on known contour areas. Average end area method used.

Stage / Storage Table

| Stage (ft) | Elevation (ft) | Contour area (sqft) | Incr. Storage (cuft) | Total storage (cuft) |
|------------|----------------|---------------------|----------------------|----------------------|
| 0.00 | 229.33 | 00 | 0 | 0 |
| 0.67 | 230.00 | 2,454 | 822 | 822 |
| 2.67 | 232.00 | 5,689 | 8,143 | 8,965 |
| 4.67 | 234.00 | 6,522 | 12,211 | 21,176 |
| 6.67 | 236.00 | 7,413 | 13,935 | 35,111 |
| 8.67 | 238.00 | 9,192 | 16,605 | 51,716 |

Culvert / Orifice Structures

| | [A] | [B] | [C] | [D] |
|---------------|----------|--------|------|------|
| Rise in | = 6.0 | 3.0 | 0.0 | 0.0 |
| Span in | = 6.0 | 3.0 | 0.0 | 0.0 |
| No. Barrels | = 10 | 1 | 0 | 0 |
| Invert El. ft | = 228.40 | 231.00 | 0.00 | 0.00 |
| Length ft | = 40.0 | 1.0 | 0.0 | 0.0 |
| Slope % | = 1.00 | 0.00 | 0.00 | 0.00 |
| N-Value | = .013 | .013 | .000 | .000 |
| Orif. Coeff. | = 0.60 | 0.60 | 0.00 | 0.00 |
| Multi-Stage | = n/a | Yes | No | No |

Weir Structures

| | [A] | [B] | [C] | [D] |
|--------------|----------|--------|--------|------|
| Crest Len ft | = 0.66 | 20.00 | 16.00 | 0.00 |
| Crest El. ft | = 232.00 | 236.00 | 235.50 | 0.00 |
| Weir Coeff. | = 3.33 | 2.60 | 3.33 | 0.00 |
| Weir Type | = Rect | Broad | Rect | --- |
| Multi-Stage | = Yes | No | Yes | No |

Exfiltration Rate = 0.32 in/hr/sqft Tailwater Elev. = 0.00 ft

Note: All outflows have been analyzed under inlet and outlet control.

Stage / Storage / Discharge Table

| Stage ft | Storage cuft | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Total cfs |
|----------|--------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-----------|
| 0.00 | 0 | 229.33 | 0.00 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.000 | 0.00 |
| 0.07 | 82 | 229.40 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.002 | 0.00 |
| 0.13 | 164 | 229.46 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.004 | 0.00 |
| 0.20 | 247 | 229.53 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.005 | 0.01 |
| 0.27 | 329 | 229.60 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.007 | 0.01 |
| 0.34 | 411 | 229.67 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.009 | 0.01 |
| 0.40 | 493 | 229.73 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.011 | 0.01 |
| 0.47 | 575 | 229.80 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.013 | 0.01 |
| 0.54 | 658 | 229.87 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.015 | 0.01 |
| 0.60 | 740 | 229.93 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.016 | 0.02 |
| 0.67 | 822 | 230.00 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.018 | 0.02 |
| 0.87 | 1,636 | 230.20 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.021 | 0.02 |
| 1.07 | 2,451 | 230.40 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.023 | 0.02 |
| 1.27 | 3,265 | 230.60 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.025 | 0.03 |
| 1.47 | 4,079 | 230.80 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.028 | 0.03 |
| 1.67 | 4,894 | 231.00 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.030 | 0.03 |
| 1.87 | 5,708 | 231.20 | 6.68 | 0.06 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.033 | 0.10 |
| 2.07 | 6,522 | 231.40 | 6.68 | 0.12 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.035 | 0.16 |
| 2.27 | 7,336 | 231.60 | 6.68 | 0.16 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.037 | 0.20 |
| 2.47 | 8,151 | 231.80 | 6.68 | 0.19 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.040 | 0.23 |
| 2.67 | 8,965 | 232.00 | 6.68 | 0.22 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.042 | 0.26 |
| 2.87 | 10,186 | 232.20 | 6.68 | 0.25 | --- | --- | 0.20 | 0.00 | 0.00 | --- | 0.043 | 0.48 |
| 3.07 | 11,407 | 232.40 | 6.68 | 0.27 | --- | --- | 0.56 | 0.00 | 0.00 | --- | 0.043 | 0.87 |
| 3.27 | 12,628 | 232.60 | 6.68 | 0.29 | --- | --- | 1.02 | 0.00 | 0.00 | --- | 0.044 | 1.35 |
| 3.47 | 13,849 | 232.80 | 6.68 | 0.31 | --- | --- | 1.57 | 0.00 | 0.00 | --- | 0.045 | 1.92 |
| 3.67 | 15,071 | 233.00 | 6.68 | 0.32 | --- | --- | 2.20 | 0.00 | 0.00 | --- | 0.045 | 2.57 |
| 3.87 | 16,292 | 233.20 | 6.68 | 0.34 | --- | --- | 2.89 | 0.00 | 0.00 | --- | 0.046 | 3.28 |
| 4.07 | 17,513 | 233.40 | 6.68 | 0.36 | --- | --- | 3.64 | 0.00 | 0.00 | --- | 0.046 | 4.04 |
| 4.27 | 18,734 | 233.60 | 6.68 | 0.37 | --- | --- | 4.45 | 0.00 | 0.00 | --- | 0.047 | 4.87 |
| 4.47 | 19,955 | 233.80 | 6.68 | 0.39 | --- | --- | 5.31 | 0.00 | 0.00 | --- | 0.048 | 5.74 |
| 4.67 | 21,176 | 234.00 | 6.68 | 0.40 | --- | --- | 6.22 | 0.00 | 0.00 | --- | 0.048 | 6.67 |
| 4.87 | 22,570 | 234.20 | 7.59 | 0.41 | --- | --- | 7.17 | 0.00 | 0.00 | --- | 0.049 | 7.64 |

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Stage / Storage / Discharge Table

| Stage ft | Storage cuft | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Total cfs |
|-------------|-----------------|-----------------|--------------|--------------|--------------|--------------|-------------|-------------|-------------|-------------|--------------|--------------|
| 5.07 | 23,963 | 234.40 | 8.60 | 0.43 | --- | --- | 8.17 | 0.00 | 0.00 | --- | 0.050 | 8.65 |
| 5.27 | 25,357 | 234.60 | 9.65 | 0.44 | --- | --- | 9.21 | 0.00 | 0.00 | --- | 0.050 | 9.70 |
| 5.47 | 26,750 | 234.80 | 10.75 | 0.45 | --- | --- | 10.30 | 0.00 | 0.00 | --- | 0.051 | 10.80 |
| 5.67 | 28,144 | 235.00 | 11.89 | 0.47 | --- | --- | 11.42 | 0.00 | 0.00 | --- | 0.052 | 11.94 |
| 5.87 | 29,537 | 235.20 | 13.03 | 0.44 | --- | --- | 12.58 | 0.00 | 0.00 | --- | 0.052 | 13.08 |
| 6.07 | 30,931 | 235.40 | 14.12 | 0.42 | --- | --- | 13.70 | 0.00 | 0.00 | --- | 0.053 | 14.17 |
| 6.27 | 32,324 | 235.60 | 15.89 | 0.37 | --- | --- | 13.84 | 0.00 | 1.68 | --- | 0.054 | 15.94 |
| 6.47 | 33,718 | 235.80 | 18.81 | 0.20 | --- | --- | 9.85 | 0.00 | 8.75 | --- | 0.054 | 18.86 |
| 6.67 | 35,111 | 236.00 | 19.86 | 0.10 | --- | --- | 5.97 | 0.00 | 13.80 | --- | 0.055 | 19.92 |
| 6.87 | 36,772 | 236.20 | 20.25 | 0.07 | --- | --- | 4.74 | 4.65 | 15.44 | --- | 0.056 | 24.95 |
| 7.07 | 38,432 | 236.40 | 20.56 | 0.05 | --- | --- | 4.01 | 13.15 | 16.50 | --- | 0.058 | 33.77 |
| 7.27 | 40,093 | 236.60 | 20.84 | 0.04 | --- | --- | 3.52 | 24.17 | 17.27 | --- | 0.059 | 45.05 |
| 7.47 | 41,753 | 236.80 | 21.10 | 0.03 | --- | --- | 3.17 | 37.21 | 17.88 | --- | 0.060 | 58.35 |
| 7.67 | 43,414 | 237.00 | 21.36 | 0.03 | --- | --- | 2.91 | 52.00 | 18.41 | --- | 0.061 | 73.40 |
| 7.87 | 45,074 | 237.20 | 21.62 | 0.02 | --- | --- | 2.71 | 68.35 | 18.85 | --- | 0.063 | 90.00 |
| 8.07 | 46,735 | 237.40 | 21.87 | 0.02 | --- | --- | 2.54 | 86.14 | 19.22 | --- | 0.064 | 107.99 |
| 8.27 | 48,395 | 237.60 | 22.12 | 0.02 | --- | --- | 2.41 | 105.24 | 19.56 | --- | 0.065 | 127.29 |
| 8.47 | 50,056 | 237.80 | 22.36 | 0.02 | --- | --- | 2.31 | 125.57 | 19.95 | --- | 0.067 | 147.91 |
| 8.67 | 51,716 | 238.00 | 22.60 | 0.01 | --- | --- | 2.21 | 147.08 | 20.20 | --- | 0.068 | 169.58 |

...End

Hydrograph Report

Hyd. No. 13

Basin 3 Out

Hydrograph type = Reservoir
 Storm frequency = 10 yrs
 Inflow hyd. No. = 10
 Max. Elevation = 224.38 ft

Peak discharge = 1.15 cfs
 Time interval = 2 min
 Reservoir name = Basin 3 (Hotel)
 Max. Storage = 20,176 cuft

Storage Indication method used.

Outflow hydrograph volume = 40,143 cuft

Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 536 | 0.17 | 219.24 | 10.70 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.11 |
| 540 | 0.18 | 219.26 | 10.70 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.12 |
| 544 | 0.19 | 219.28 | 10.70 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.12 |
| 548 | 0.19 | 219.30 | 10.70 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 552 | 0.20 | 219.32 | 10.70 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 556 | 0.21 | 219.35 | 10.70 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 560 | 0.22 | 219.37 | 10.70 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 564 | 0.23 | 219.40 | 10.70 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 568 | 0.24 | 219.43 | 10.70 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 572 | 0.25 | 219.46 | 10.70 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |
| 576 | 0.26 | 219.49 | 10.70 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 580 | 0.27 | 219.52 | 10.70 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 584 | 0.28 | 219.56 | 10.70 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 588 | 0.29 | 219.60 | 10.70 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 592 | 0.30 | 219.63 | 10.70 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 596 | 0.31 | 219.67 | 10.70 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 600 | 0.32 | 219.71 | 10.70 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 604 | 0.34 | 219.76 | 10.70 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 608 | 0.35 | 219.80 | 10.70 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 612 | 0.37 | 219.85 | 10.70 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 616 | 0.38 | 219.91 | 10.70 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 620 | 0.40 | 219.96 | 10.70 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 624 | 0.42 | 220.01 | 10.70 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 628 | 0.44 | 220.02 | 10.70 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 632 | 0.46 | 220.04 | 10.70 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 636 | 0.48 | 220.05 | 10.70 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 640 | 0.50 | 220.07 | 10.70 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 644 | 0.52 | 220.09 | 10.70 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 648 | 0.55 | 220.12 | 10.70 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 652 | 0.57 | 220.14 | 10.70 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 656 | 0.59 | 220.17 | 10.70 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 660 | 0.61 | 220.19 | 10.70 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 664 | 0.64 | 220.22 | 10.70 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 668 | 0.68 | 220.25 | 10.70 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 672 | 0.74 | 220.29 | 10.70 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 676 | 0.81 | 220.33 | 10.70 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 680 | 0.89 | 220.37 | 10.70 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 684 | 0.96 | 220.42 | 10.70 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |

Continues on next page...

Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 688 | 1.04 | 220.48 | 10.70 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 692 | 1.13 | 220.54 | 10.70 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 696 | 1.36 | 220.61 | 10.70 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 700 | 1.84 | 220.71 | 10.70 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 704 | 2.48 | 220.85 | 10.70 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 708 | 3.20 | 221.05 | 10.70 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 712 | 3.98 | 221.30 | 10.70 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 716 | 4.93 | 221.61 | 10.70 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 720 | 7.39 | 222.03 | 10.70 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.41 |
| 724 | 11.01 | 222.42 | 10.70 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.44 |
| 728 | 11.14 | 222.91 | 10.70 | 0.47 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.47 |
| 732 | 8.47 | 223.33 | 10.70 | 0.49 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.49 |
| 736 | 6.18 | 223.63 | 10.70 | 0.51 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.51 |
| 740 | 5.07 | 223.86 | 10.70 | 0.52 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.52 |
| 744 | 4.27 | 224.03 | 10.70 | 0.53 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | 0.56 |
| 748 | 3.45 | 224.15 | 10.70 | 0.54 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | 0.67 |
| 752 | 2.64 | 224.24 | 10.70 | 0.54 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | 0.80 |
| 756 | 2.01 | 224.29 | 10.70 | 0.54 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | 0.92 |
| 760 | 1.70 | 224.32 | 10.70 | 0.55 | 0.45 | ---- | ---- | ---- | ---- | ---- | ---- | 1.00 |
| 764 | 1.57 | 224.34 | 10.70 | 0.55 | 0.50 | ---- | ---- | ---- | ---- | ---- | ---- | 1.05 |
| 768 | 1.48 | 224.36 | 10.70 | 0.55 | 0.54 | ---- | ---- | ---- | ---- | ---- | ---- | 1.09 |
| 772 | 1.40 | 224.37 | 10.70 | 0.55 | 0.57 | ---- | ---- | ---- | ---- | ---- | ---- | 1.12 |
| 776 | 1.31 | 224.38 | 10.70 | 0.55 | 0.59 | ---- | ---- | ---- | ---- | ---- | ---- | 1.14 |
| 780 | 1.22 | 224.38 | 10.70 | 0.55 | 0.60 | ---- | ---- | ---- | ---- | ---- | ---- | 1.15 |
| 784 | 1.14 | 224.38 << | 10.70 | 0.55 | 0.60 | ---- | ---- | ---- | ---- | ---- | ---- | 1.15 << |
| 788 | 1.08 | 224.38 | 10.70 | 0.55 | 0.60 | ---- | ---- | ---- | ---- | ---- | ---- | 1.15 |
| 792 | 1.05 | 224.38 | 10.70 | 0.55 | 0.59 | ---- | ---- | ---- | ---- | ---- | ---- | 1.14 |
| 796 | 1.03 | 224.38 | 10.70 | 0.55 | 0.58 | ---- | ---- | ---- | ---- | ---- | ---- | 1.13 |
| 800 | 1.00 | 224.37 | 10.70 | 0.55 | 0.57 | ---- | ---- | ---- | ---- | ---- | ---- | 1.12 |
| 804 | 0.98 | 224.37 | 10.70 | 0.55 | 0.56 | ---- | ---- | ---- | ---- | ---- | ---- | 1.11 |
| 808 | 0.96 | 224.36 | 10.70 | 0.55 | 0.55 | ---- | ---- | ---- | ---- | ---- | ---- | 1.10 |
| 812 | 0.94 | 224.36 | 10.70 | 0.55 | 0.54 | ---- | ---- | ---- | ---- | ---- | ---- | 1.09 |
| 816 | 0.91 | 224.35 | 10.70 | 0.55 | 0.53 | ---- | ---- | ---- | ---- | ---- | ---- | 1.07 |
| 820 | 0.89 | 224.35 | 10.70 | 0.55 | 0.51 | ---- | ---- | ---- | ---- | ---- | ---- | 1.06 |
| 824 | 0.87 | 224.34 | 10.70 | 0.55 | 0.50 | ---- | ---- | ---- | ---- | ---- | ---- | 1.05 |
| 828 | 0.84 | 224.33 | 10.70 | 0.55 | 0.48 | ---- | ---- | ---- | ---- | ---- | ---- | 1.03 |
| 832 | 0.82 | 224.33 | 10.70 | 0.55 | 0.47 | ---- | ---- | ---- | ---- | ---- | ---- | 1.01 |
| 836 | 0.80 | 224.32 | 10.70 | 0.55 | 0.45 | ---- | ---- | ---- | ---- | ---- | ---- | 1.00 |
| 840 | 0.78 | 224.31 | 10.70 | 0.54 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | 0.98 |
| 844 | 0.75 | 224.30 | 10.70 | 0.54 | 0.42 | ---- | ---- | ---- | ---- | ---- | ---- | 0.96 |
| 848 | 0.74 | 224.30 | 10.70 | 0.54 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | 0.94 |
| 852 | 0.72 | 224.29 | 10.70 | 0.54 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | 0.93 |
| 856 | 0.71 | 224.28 | 10.70 | 0.54 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | 0.91 |
| 860 | 0.70 | 224.28 | 10.70 | 0.54 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | 0.89 |
| 864 | 0.69 | 224.27 | 10.70 | 0.54 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | 0.88 |
| 868 | 0.68 | 224.26 | 10.70 | 0.54 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | 0.86 |
| 872 | 0.67 | 224.26 | 10.70 | 0.54 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | 0.85 |
| 876 | 0.66 | 224.25 | 10.70 | 0.54 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | 0.83 |
| 880 | 0.65 | 224.24 | 10.70 | 0.54 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | 0.82 |
| 884 | 0.63 | 224.24 | 10.70 | 0.54 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | 0.80 |
| 888 | 0.62 | 224.23 | 10.70 | 0.54 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | 0.79 |

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Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 892 | 0.61 | 224.22 | 10.70 | 0.54 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | 0.77 |
| 896 | 0.60 | 224.22 | 10.70 | 0.54 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | 0.76 |
| 900 | 0.59 | 224.21 | 10.70 | 0.54 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | 0.75 |
| 904 | 0.58 | 224.21 | 10.70 | 0.54 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | 0.73 |
| 908 | 0.57 | 224.20 | 10.70 | 0.54 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | 0.72 |
| 912 | 0.55 | 224.20 | 10.70 | 0.54 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | 0.71 |
| 916 | 0.54 | 224.19 | 10.70 | 0.54 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | 0.71 |
| 920 | 0.53 | 224.18 | 10.70 | 0.54 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | 0.70 |
| 924 | 0.52 | 224.18 | 10.70 | 0.54 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | 0.70 |
| 928 | 0.51 | 224.17 | 10.70 | 0.54 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | 0.69 |
| 932 | 0.50 | 224.16 | 10.70 | 0.54 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | 0.68 |
| 936 | 0.49 | 224.16 | 10.70 | 0.54 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | 0.68 |
| 940 | 0.47 | 224.15 | 10.70 | 0.54 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | 0.67 |
| 944 | 0.46 | 224.14 | 10.70 | 0.54 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | 0.66 |
| 948 | 0.45 | 224.14 | 10.70 | 0.54 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | 0.66 |
| 952 | 0.44 | 224.13 | 10.70 | 0.54 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | 0.65 |
| 956 | 0.43 | 224.12 | 10.70 | 0.53 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | 0.64 |
| 960 | 0.42 | 224.11 | 10.70 | 0.53 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | 0.64 |
| 964 | 0.41 | 224.11 | 10.70 | 0.53 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | 0.63 |
| 968 | 0.40 | 224.10 | 10.70 | 0.53 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | 0.62 |
| 972 | 0.39 | 224.09 | 10.70 | 0.53 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | 0.61 |
| 976 | 0.39 | 224.08 | 10.70 | 0.53 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | 0.60 |
| 980 | 0.38 | 224.07 | 10.70 | 0.53 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | 0.60 |
| 984 | 0.38 | 224.07 | 10.70 | 0.53 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | 0.59 |
| 988 | 0.37 | 224.06 | 10.70 | 0.53 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | 0.58 |
| 992 | 0.37 | 224.05 | 10.70 | 0.53 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | 0.58 |
| 996 | 0.36 | 224.04 | 10.70 | 0.53 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | 0.57 |
| 1000 | 0.36 | 224.04 | 10.70 | 0.53 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | 0.56 |
| 1004 | 0.35 | 224.03 | 10.70 | 0.53 | 0.02 | ---- | ---- | ---- | ---- | ---- | ---- | 0.55 |
| 1008 | 0.35 | 224.02 | 10.70 | 0.53 | 0.02 | ---- | ---- | ---- | ---- | ---- | ---- | 0.55 |
| 1012 | 0.34 | 224.01 | 10.70 | 0.53 | 0.01 | ---- | ---- | ---- | ---- | ---- | ---- | 0.54 |
| 1016 | 0.34 | 224.01 | 10.70 | 0.53 | 0.01 | ---- | ---- | ---- | ---- | ---- | ---- | 0.53 |
| 1020 | 0.33 | 224.00 | 10.70 | 0.53 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.53 |
| 1024 | 0.33 | 223.99 | 10.70 | 0.53 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.53 |
| 1028 | 0.32 | 223.98 | 10.70 | 0.53 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.53 |
| 1032 | 0.32 | 223.97 | 10.70 | 0.53 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.53 |
| 1036 | 0.31 | 223.96 | 10.70 | 0.53 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.53 |
| 1040 | 0.31 | 223.95 | 10.70 | 0.53 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.53 |
| 1044 | 0.30 | 223.94 | 10.70 | 0.53 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.53 |
| 1048 | 0.30 | 223.93 | 10.70 | 0.52 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.52 |
| 1052 | 0.29 | 223.92 | 10.70 | 0.52 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.52 |
| 1056 | 0.29 | 223.91 | 10.70 | 0.52 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.52 |
| 1060 | 0.28 | 223.90 | 10.70 | 0.52 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.52 |
| 1064 | 0.28 | 223.89 | 10.70 | 0.52 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.52 |
| 1068 | 0.27 | 223.88 | 10.70 | 0.52 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.52 |
| 1072 | 0.27 | 223.87 | 10.70 | 0.52 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.52 |
| 1076 | 0.26 | 223.86 | 10.70 | 0.52 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.52 |
| 1080 | 0.26 | 223.84 | 10.70 | 0.52 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.52 |
| 1084 | 0.25 | 223.83 | 10.70 | 0.52 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.52 |
| 1088 | 0.25 | 223.82 | 10.70 | 0.52 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.52 |
| 1092 | 0.25 | 223.81 | 10.70 | 0.52 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.52 |

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Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 1096 | 0.24 | 223.80 | 10.70 | 0.52 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.52 |
| 1100 | 0.24 | 223.78 | 10.70 | 0.52 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.52 |
| 1104 | 0.24 | 223.77 | 10.70 | 0.52 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.52 |
| 1108 | 0.24 | 223.76 | 10.70 | 0.52 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.52 |
| 1112 | 0.24 | 223.75 | 10.70 | 0.51 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.51 |
| 1116 | 0.24 | 223.73 | 10.70 | 0.51 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.51 |
| 1120 | 0.23 | 223.72 | 10.70 | 0.51 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.51 |
| 1124 | 0.23 | 223.71 | 10.70 | 0.51 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.51 |
| 1128 | 0.23 | 223.70 | 10.70 | 0.51 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.51 |
| 1132 | 0.23 | 223.68 | 10.70 | 0.51 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.51 |
| 1136 | 0.23 | 223.67 | 10.70 | 0.51 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.51 |
| 1140 | 0.23 | 223.66 | 10.70 | 0.51 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.51 |
| 1144 | 0.23 | 223.65 | 10.70 | 0.51 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.51 |
| 1148 | 0.22 | 223.63 | 10.70 | 0.51 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.51 |
| 1152 | 0.22 | 223.62 | 10.70 | 0.51 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.51 |
| 1156 | 0.22 | 223.61 | 10.70 | 0.51 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.51 |
| 1160 | 0.22 | 223.60 | 10.70 | 0.51 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.51 |
| 1164 | 0.22 | 223.58 | 10.70 | 0.51 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.51 |
| 1168 | 0.22 | 223.57 | 10.70 | 0.51 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.51 |
| 1172 | 0.22 | 223.56 | 10.70 | 0.50 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.50 |
| 1176 | 0.21 | 223.54 | 10.70 | 0.50 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.50 |
| 1180 | 0.21 | 223.53 | 10.70 | 0.50 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.50 |
| 1184 | 0.21 | 223.52 | 10.70 | 0.50 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.50 |
| 1188 | 0.21 | 223.51 | 10.70 | 0.50 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.50 |
| 1192 | 0.21 | 223.49 | 10.70 | 0.50 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.50 |
| 1196 | 0.21 | 223.48 | 10.70 | 0.50 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.50 |
| 1200 | 0.20 | 223.47 | 10.70 | 0.50 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.50 |
| 1204 | 0.20 | 223.45 | 10.70 | 0.50 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.50 |
| 1208 | 0.20 | 223.44 | 10.70 | 0.50 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.50 |
| 1212 | 0.20 | 223.43 | 10.70 | 0.50 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.50 |
| 1216 | 0.20 | 223.41 | 10.70 | 0.50 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.50 |
| 1220 | 0.20 | 223.40 | 10.70 | 0.50 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.50 |
| 1224 | 0.20 | 223.39 | 10.70 | 0.49 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.49 |
| 1228 | 0.19 | 223.37 | 10.70 | 0.49 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.49 |
| 1232 | 0.19 | 223.36 | 10.70 | 0.49 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.49 |
| 1236 | 0.19 | 223.35 | 10.70 | 0.49 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.49 |
| 1240 | 0.19 | 223.33 | 10.70 | 0.49 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.49 |
| 1244 | 0.19 | 223.32 | 10.70 | 0.49 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.49 |
| 1248 | 0.19 | 223.31 | 10.70 | 0.49 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.49 |
| 1252 | 0.18 | 223.29 | 10.70 | 0.49 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.49 |
| 1256 | 0.18 | 223.28 | 10.70 | 0.49 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.49 |
| 1260 | 0.18 | 223.26 | 10.70 | 0.49 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.49 |
| 1264 | 0.18 | 223.25 | 10.70 | 0.49 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.49 |
| 1268 | 0.18 | 223.24 | 10.70 | 0.49 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.49 |
| 1272 | 0.18 | 223.22 | 10.70 | 0.49 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.49 |
| 1276 | 0.18 | 223.21 | 10.70 | 0.48 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.48 |
| 1280 | 0.17 | 223.20 | 10.70 | 0.48 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.48 |
| 1284 | 0.17 | 223.18 | 10.70 | 0.48 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.48 |
| 1288 | 0.17 | 223.17 | 10.70 | 0.48 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.48 |
| 1292 | 0.17 | 223.15 | 10.70 | 0.48 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.48 |
| 1296 | 0.17 | 223.14 | 10.70 | 0.48 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.48 |

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Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 1300 | 0.17 | 223.13 | 10.70 | 0.48 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.48 |
| 1304 | 0.16 | 223.11 | 10.70 | 0.48 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.48 |
| 1308 | 0.16 | 223.10 | 10.70 | 0.48 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.48 |
| 1312 | 0.16 | 223.08 | 10.70 | 0.48 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.48 |
| 1316 | 0.16 | 223.07 | 10.70 | 0.48 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.48 |
| 1320 | 0.16 | 223.06 | 10.70 | 0.48 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.48 |
| 1324 | 0.22 | 223.04 | 10.70 | 0.48 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.48 |
| 1328 | 0.23 | 223.03 | 10.70 | 0.47 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.47 |
| 1332 | 0.20 | 223.02 | 10.70 | 0.47 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.47 |
| 1336 | 0.17 | 223.01 | 10.70 | 0.47 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.47 |
| 1340 | 0.16 | 222.99 | 10.70 | 0.47 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.47 |
| 1344 | 0.16 | 222.98 | 10.70 | 0.47 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.47 |
| 1348 | 0.16 | 222.97 | 10.70 | 0.47 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.47 |
| 1352 | 0.16 | 222.95 | 10.70 | 0.47 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.47 |
| 1356 | 0.16 | 222.94 | 10.70 | 0.47 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.47 |
| 1360 | 0.16 | 222.92 | 10.70 | 0.47 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.47 |
| 1364 | 0.16 | 222.91 | 10.70 | 0.47 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.47 |
| 1368 | 0.16 | 222.90 | 10.70 | 0.47 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.47 |
| 1372 | 0.15 | 222.88 | 10.70 | 0.47 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.47 |
| 1376 | 0.15 | 222.87 | 10.70 | 0.46 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.46 |
| 1380 | 0.15 | 222.86 | 10.70 | 0.46 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.46 |
| 1384 | 0.15 | 222.84 | 10.70 | 0.46 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.46 |
| 1388 | 0.15 | 222.83 | 10.70 | 0.46 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.46 |
| 1392 | 0.15 | 222.81 | 10.70 | 0.46 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.46 |
| 1396 | 0.15 | 222.80 | 10.70 | 0.46 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.46 |
| 1400 | 0.15 | 222.79 | 10.70 | 0.46 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.46 |
| 1404 | 0.15 | 222.77 | 10.70 | 0.46 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.46 |
| 1408 | 0.14 | 222.76 | 10.70 | 0.46 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.46 |
| 1412 | 0.14 | 222.74 | 10.70 | 0.46 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.46 |
| 1416 | 0.14 | 222.73 | 10.70 | 0.46 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.46 |
| 1420 | 0.14 | 222.72 | 10.70 | 0.46 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.46 |
| 1424 | 0.14 | 222.70 | 10.70 | 0.45 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.45 |
| 1428 | 0.14 | 222.69 | 10.70 | 0.45 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.45 |
| 1432 | 0.14 | 222.67 | 10.70 | 0.45 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.45 |
| 1436 | 0.14 | 222.66 | 10.70 | 0.45 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.45 |
| 1440 | 0.14 | 222.65 | 10.70 | 0.45 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.45 |
| 1444 | 0.10 | 222.63 | 10.70 | 0.45 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.45 |
| 1448 | 0.04 | 222.61 | 10.70 | 0.45 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.45 |
| 1452 | 0.01 | 222.59 | 10.70 | 0.45 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.45 |
| 1456 | 0.00 | 222.57 | 10.70 | 0.45 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.45 |
| 1460 | 0.00 | 222.55 | 10.70 | 0.45 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.45 |
| 1464 | 0.00 | 222.53 | 10.70 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.44 |
| 1468 | 0.00 | 222.51 | 10.70 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.44 |
| 1472 | 0.00 | 222.49 | 10.70 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.44 |
| 1476 | 0.00 | 222.48 | 10.70 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.44 |
| 1480 | 0.00 | 222.46 | 10.70 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.44 |
| 1484 | 0.00 | 222.44 | 10.70 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.44 |
| 1488 | 0.00 | 222.42 | 10.70 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.44 |
| 1492 | 0.00 | 222.40 | 10.70 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.44 |
| 1496 | 0.00 | 222.38 | 10.70 | 0.43 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.43 |
| 1500 | 0.00 | 222.36 | 10.70 | 0.43 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.43 |

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Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Civ A cfs | Civ B cfs | Civ C cfs | Civ D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 1504 | 0.00 | 222.34 | 10.70 | 0.43 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.43 |
| 1508 | 0.00 | 222.32 | 10.70 | 0.43 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.43 |
| 1512 | 0.00 | 222.30 | 10.70 | 0.43 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.43 |
| 1516 | 0.00 | 222.28 | 10.70 | 0.43 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.43 |
| 1520 | 0.00 | 222.26 | 10.70 | 0.43 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.43 |
| 1524 | 0.00 | 222.24 | 10.70 | 0.43 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.43 |
| 1528 | 0.00 | 222.22 | 10.70 | 0.42 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.42 |
| 1532 | 0.00 | 222.21 | 10.70 | 0.42 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.42 |
| 1536 | 0.00 | 222.19 | 10.70 | 0.42 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.42 |
| 1540 | 0.00 | 222.17 | 10.70 | 0.42 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.42 |
| 1544 | 0.00 | 222.15 | 10.70 | 0.42 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.42 |
| 1548 | 0.00 | 222.13 | 10.70 | 0.42 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.42 |
| 1552 | 0.00 | 222.11 | 10.70 | 0.42 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.42 |
| 1556 | 0.00 | 222.09 | 10.70 | 0.42 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.42 |
| 1560 | 0.00 | 222.07 | 10.70 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.41 |
| 1564 | 0.00 | 222.06 | 10.70 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.41 |
| 1568 | 0.00 | 222.04 | 10.70 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.41 |
| 1572 | 0.00 | 222.02 | 10.70 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.41 |
| 1576 | 0.00 | 222.00 | 10.70 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.41 |
| 1580 | 0.00 | 221.97 | 10.70 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.41 |
| 1584 | 0.00 | 221.94 | 10.70 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.41 |
| 1588 | 0.00 | 221.91 | 10.70 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 1592 | 0.00 | 221.88 | 10.70 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 1596 | 0.00 | 221.84 | 10.70 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 1600 | 0.00 | 221.81 | 10.70 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 1604 | 0.00 | 221.78 | 10.70 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1608 | 0.00 | 221.75 | 10.70 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1612 | 0.00 | 221.72 | 10.70 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1616 | 0.00 | 221.69 | 10.70 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1620 | 0.00 | 221.66 | 10.70 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1624 | 0.00 | 221.63 | 10.70 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1628 | 0.00 | 221.60 | 10.70 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1632 | 0.00 | 221.57 | 10.70 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1636 | 0.00 | 221.54 | 10.70 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1640 | 0.00 | 221.51 | 10.70 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1644 | 0.00 | 221.49 | 10.70 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1648 | 0.00 | 221.46 | 10.70 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1652 | 0.00 | 221.43 | 10.70 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1656 | 0.00 | 221.40 | 10.70 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1660 | 0.00 | 221.37 | 10.70 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1664 | 0.00 | 221.34 | 10.70 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1668 | 0.00 | 221.31 | 10.70 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1672 | 0.00 | 221.29 | 10.70 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1676 | 0.00 | 221.26 | 10.70 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1680 | 0.00 | 221.23 | 10.70 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1684 | 0.00 | 221.20 | 10.70 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1688 | 0.00 | 221.18 | 10.70 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1692 | 0.00 | 221.15 | 10.70 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1696 | 0.00 | 221.12 | 10.70 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1700 | 0.00 | 221.10 | 10.70 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1704 | 0.00 | 221.07 | 10.70 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |

Continues on next page...

Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 1708 | 0.00 | 221.04 | 10.70 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1712 | 0.00 | 221.02 | 10.70 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1716 | 0.00 | 220.99 | 10.70 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1720 | 0.00 | 220.97 | 10.70 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1724 | 0.00 | 220.94 | 10.70 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1728 | 0.00 | 220.91 | 10.70 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1732 | 0.00 | 220.89 | 10.70 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1736 | 0.00 | 220.86 | 10.70 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1740 | 0.00 | 220.84 | 10.70 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1744 | 0.00 | 220.81 | 10.70 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1748 | 0.00 | 220.79 | 10.70 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1752 | 0.00 | 220.77 | 10.70 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1756 | 0.00 | 220.74 | 10.70 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1760 | 0.00 | 220.72 | 10.70 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1764 | 0.00 | 220.69 | 10.70 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1768 | 0.00 | 220.67 | 10.70 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1772 | 0.00 | 220.65 | 10.70 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1776 | 0.00 | 220.62 | 10.70 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1780 | 0.00 | 220.60 | 10.70 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1784 | 0.00 | 220.58 | 10.70 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1788 | 0.00 | 220.55 | 10.70 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1792 | 0.00 | 220.53 | 10.70 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1796 | 0.00 | 220.51 | 10.70 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1800 | 0.00 | 220.49 | 10.70 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1804 | 0.00 | 220.46 | 10.70 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1808 | 0.00 | 220.44 | 10.70 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 1812 | 0.00 | 220.42 | 10.70 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 1816 | 0.00 | 220.40 | 10.70 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 1820 | 0.00 | 220.38 | 10.70 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 1824 | 0.00 | 220.35 | 10.70 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 1828 | 0.00 | 220.33 | 10.70 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 1832 | 0.00 | 220.31 | 10.70 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 1836 | 0.00 | 220.29 | 10.70 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 1840 | 0.00 | 220.27 | 10.70 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 1844 | 0.00 | 220.25 | 10.70 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 1848 | 0.00 | 220.23 | 10.70 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 1852 | 0.00 | 220.21 | 10.70 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 1856 | 0.00 | 220.19 | 10.70 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 1860 | 0.00 | 220.17 | 10.70 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 1864 | 0.00 | 220.15 | 10.70 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 1868 | 0.00 | 220.13 | 10.70 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 1872 | 0.00 | 220.11 | 10.70 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 1876 | 0.00 | 220.09 | 10.70 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 1880 | 0.00 | 220.07 | 10.70 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 1884 | 0.00 | 220.05 | 10.70 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 1888 | 0.00 | 220.03 | 10.70 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 1892 | 0.00 | 220.02 | 10.70 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 1896 | 0.00 | 219.99 | 10.70 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 1900 | 0.00 | 219.91 | 10.70 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 1904 | 0.00 | 219.83 | 10.70 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 1908 | 0.00 | 219.76 | 10.70 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |

Continues on next page...

Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Civ A cfs | Civ B cfs | Civ C cfs | Civ D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 1912 | 0.00 | 219.69 | 10.70 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 1916 | 0.00 | 219.63 | 10.70 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 1920 | 0.00 | 219.57 | 10.70 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 1924 | 0.00 | 219.51 | 10.70 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 1928 | 0.00 | 219.45 | 10.70 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |
| 1932 | 0.00 | 219.40 | 10.70 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 1936 | 0.00 | 219.35 | 10.70 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 1940 | 0.00 | 219.30 | 10.70 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 1944 | 0.00 | 219.26 | 10.70 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.12 |

...End

Reservoir Report

Reservoir No. 3 - Basin 3 (Hotel)

Hydraflow Hydrographs by Intelisolve

Pond Data

Pond storage is based on known contour areas. Average end area method used.

Stage / Storage Table

| Stage (ft) | Elevation (ft) | Contour area (sqft) | Incr. Storage (cuft) | Total storage (cuft) |
|------------|----------------|---------------------|----------------------|----------------------|
| 0.00 | 219.00 | 00 | 0 | 0 |
| 1.00 | 220.00 | 1,406 | 703 | 703 |
| 3.00 | 222.00 | 4,776 | 6,182 | 6,885 |
| 5.00 | 224.00 | 5,971 | 10,747 | 17,632 |
| 7.00 | 226.00 | 7,278 | 13,249 | 30,881 |
| 9.00 | 228.00 | 8,709 | 15,987 | 46,868 |
| 9.50 | 228.50 | 9,086 | 4,449 | 51,317 |

Culvert / Orifice Structures

| | [A] | [B] | [C] | [D] |
|---------------|----------|--------|--------|------|
| Rise in | = 24.0 | 3.0 | 12.0 | 0.0 |
| Span in | = 24.0 | 3.0 | 12.0 | 0.0 |
| No. Barrels | = 1 | 1 | 1 | 0 |
| Invert El. ft | = 217.50 | 217.90 | 224.00 | 0.00 |
| Length ft | = 48.0 | 1.0 | 1.0 | 0.0 |
| Slope % | = 10.00 | 0.00 | 0.00 | 0.00 |
| N-Value | = .013 | .013 | .013 | .000 |
| Orif. Coeff. | = 0.60 | 0.60 | 0.60 | 0.00 |
| Multi-Stage | = n/a | Yes | Yes | No |

Weir Structures

| | [A] | [B] | [C] | [D] |
|--------------|----------|--------|--------|--------|
| Crest Len ft | = 1.00 | 2.00 | 16.00 | 90.00 |
| Crest El. ft | = 225.25 | 226.00 | 227.00 | 227.00 |
| Weir Coeff. | = 3.33 | 3.33 | 3.33 | 2.60 |
| Weir Type | = Rect | Rect | Rect | Broad |
| Multi-Stage | = Yes | Yes | Yes | Yes |

Exfiltration Rate = 0.00 in/hr/sqft Tailwater Elev. = 0.00 ft

Stage / Storage / Discharge Table

Note: All outflows have been analyzed under inlet and outlet control.

| Stage ft | Storage cuft | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Total cfs |
|----------|--------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-----------|
| 0.00 | 0 | 219.00 | 0.00 | 0.00 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.00 |
| 0.10 | 70 | 219.10 | 10.70 | 0.07 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.07 |
| 0.20 | 141 | 219.20 | 10.70 | 0.11 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.11 |
| 0.30 | 211 | 219.30 | 10.70 | 0.13 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.13 |
| 0.40 | 281 | 219.40 | 10.70 | 0.15 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.15 |
| 0.50 | 352 | 219.50 | 10.70 | 0.17 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.17 |
| 0.60 | 422 | 219.60 | 10.70 | 0.18 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.18 |
| 0.70 | 492 | 219.70 | 10.70 | 0.20 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.20 |
| 0.80 | 562 | 219.80 | 10.70 | 0.21 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.21 |
| 0.90 | 633 | 219.90 | 10.70 | 0.22 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.22 |
| 1.00 | 703 | 220.00 | 10.70 | 0.24 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.24 |
| 1.20 | 1,321 | 220.20 | 10.70 | 0.26 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.26 |
| 1.40 | 1,939 | 220.40 | 10.70 | 0.28 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.28 |
| 1.60 | 2,558 | 220.60 | 10.70 | 0.30 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.30 |
| 1.80 | 3,176 | 220.80 | 10.70 | 0.32 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.32 |
| 2.00 | 3,794 | 221.00 | 10.70 | 0.33 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.33 |
| 2.20 | 4,412 | 221.20 | 10.70 | 0.35 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.35 |
| 2.40 | 5,030 | 221.40 | 10.70 | 0.37 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.37 |
| 2.60 | 5,649 | 221.60 | 10.70 | 0.38 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.38 |
| 2.80 | 6,267 | 221.80 | 10.70 | 0.40 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.40 |
| 3.00 | 6,885 | 222.00 | 10.70 | 0.41 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.41 |
| 3.20 | 7,960 | 222.20 | 10.70 | 0.42 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.42 |
| 3.40 | 9,034 | 222.40 | 10.70 | 0.44 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.44 |
| 3.60 | 10,109 | 222.60 | 10.70 | 0.45 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.45 |
| 3.80 | 11,184 | 222.80 | 10.70 | 0.46 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.46 |
| 4.00 | 12,259 | 223.00 | 10.70 | 0.47 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.47 |
| 4.20 | 13,333 | 223.20 | 10.70 | 0.48 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.48 |
| 4.40 | 14,408 | 223.40 | 10.70 | 0.50 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.50 |
| 4.60 | 15,483 | 223.60 | 10.70 | 0.51 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.51 |
| 4.80 | 16,557 | 223.80 | 10.70 | 0.52 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.52 |
| 5.00 | 17,632 | 224.00 | 10.70 | 0.53 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.53 |

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Stage / Storage / Discharge Table

| Stage ft | Storage cuft | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Total cfs |
|-------------|-----------------|-----------------|--------------|--------------|--------------|--------------|-------------|-------------|-------------|-------------|--------------|--------------|
| 5.20 | 18,957 | 224.20 | 10.70 | 0.54 | 0.18 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.72 |
| 5.40 | 20,282 | 224.40 | 10.70 | 0.55 | 0.64 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 1.19 |
| 5.60 | 21,607 | 224.60 | 10.70 | 0.56 | 1.34 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 1.90 |
| 5.80 | 22,932 | 224.80 | 10.70 | 0.57 | 2.07 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 2.64 |
| 6.00 | 24,257 | 225.00 | 10.70 | 0.58 | 2.67 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 3.25 |
| 6.20 | 25,581 | 225.20 | 10.70 | 0.59 | 3.16 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 3.75 |
| 6.40 | 26,906 | 225.40 | 10.70 | 0.60 | 3.59 | --- | 0.19 | 0.00 | 0.00 | 0.00 | --- | 4.38 |
| 6.60 | 28,231 | 225.60 | 10.70 | 0.61 | 3.97 | --- | 0.69 | 0.00 | 0.00 | 0.00 | --- | 5.26 |
| 6.80 | 29,556 | 225.80 | 10.70 | 0.62 | 4.31 | --- | 1.36 | 0.00 | 0.00 | 0.00 | --- | 6.29 |
| 7.00 | 30,881 | 226.00 | 10.70 | 0.63 | 4.63 | --- | 2.16 | 0.00 | 0.00 | 0.00 | --- | 7.42 |
| 7.20 | 32,480 | 226.20 | 10.70 | 0.63 | 4.93 | --- | 3.08 | 0.60 | 0.00 | 0.00 | --- | 9.24 |
| 7.40 | 34,078 | 226.40 | 11.69 | 0.64 | 5.21 | --- | 4.11 | 1.68 | 0.00 | 0.00 | --- | 11.64 |
| 7.60 | 35,677 | 226.60 | 14.47 | 0.63 | 5.48 | --- | 5.22 | 3.10 | 0.00 | 0.00 | --- | 14.43 |
| 7.80 | 37,276 | 226.80 | 17.55 | 0.62 | 5.73 | --- | 6.43 | 4.77 | 0.00 | 0.00 | --- | 17.55 |
| 8.00 | 38,875 | 227.00 | 20.95 | 0.61 | 5.98 | --- | 7.71 | 6.66 | 0.00 | 0.00 | --- | 20.95 |
| 8.20 | 40,473 | 227.20 | 42.98 | 0.19 | 2.99 | --- | 6.61 | 7.50 | 4.76 | 20.93 | --- | 42.98 |
| 8.40 | 42,072 | 227.40 | 45.00 | 0.05 | 0.84 | --- | 2.87 | 3.56 | 6.98 | 30.65 | --- | 44.96 |
| 8.60 | 43,671 | 227.60 | 45.58 | 0.03 | 0.50 | --- | 2.13 | 2.78 | 7.43 | 32.62 | --- | 45.49 |
| 8.80 | 45,269 | 227.80 | 46.10 | 0.02 | 0.35 | --- | 1.75 | 2.38 | 7.69 | 33.77 | --- | 45.95 |
| 9.00 | 46,868 | 228.00 | 46.61 | 0.02 | 0.26 | --- | 1.53 | 2.14 | 7.90 | 34.69 | --- | 46.53 |
| 9.05 | 47,313 | 228.05 | 46.73 | 0.02 | 0.24 | --- | 1.48 | 2.09 | 7.91 | 34.75 | --- | 46.48 |
| 9.10 | 47,758 | 228.10 | 46.85 | 0.01 | 0.23 | --- | 1.43 | 2.04 | 7.92 | 34.79 | --- | 46.41 |
| 9.15 | 48,203 | 228.15 | 46.98 | 0.01 | 0.21 | --- | 1.39 | 2.00 | 7.95 | 34.93 | --- | 46.50 |
| 9.20 | 48,648 | 228.20 | 47.10 | 0.01 | 0.20 | --- | 1.37 | 1.97 | 8.02 | 35.22 | --- | 46.79 |
| 9.25 | 49,092 | 228.25 | 47.22 | 0.01 | 0.19 | --- | 1.33 | 1.94 | 8.04 | 35.33 | --- | 46.85 |
| 9.30 | 49,537 | 228.30 | 47.34 | 0.01 | 0.18 | --- | 1.30 | 1.89 | 8.01 | 35.19 | --- | 46.59 |
| 9.35 | 49,982 | 228.35 | 47.46 | 0.01 | 0.17 | --- | 1.27 | 1.87 | 8.07 | 35.43 | --- | 46.82 |
| 9.40 | 50,427 | 228.40 | 47.58 | 0.01 | 0.16 | --- | 1.25 | 1.84 | 8.07 | 35.43 | --- | 46.76 |
| 9.45 | 50,872 | 228.45 | 47.70 | 0.01 | 0.16 | --- | 1.24 | 1.84 | 8.21 | 36.07 | --- | 47.54 |
| 9.50 | 51,317 | 228.50 | 47.83 | 0.01 | 0.15 | --- | 1.20 | 1.79 | 8.08 | 35.50 | --- | 46.73 |

...End

Hydrograph Report

Hyd. No. 14

Hydrograph type = Combine
Storm frequency = 10 yrs
Inflow hyds. = 11, 12, 13

Peak discharge = 4.21 cfs
Time interval = 2 min

Hydrograph Volume = 93,343 cuft

Hydrograph Discharge Table

| Time (min) | Hyd. 11 + (cfs) | Hyd. 12 + (cfs) | Hyd. 13 = (cfs) | Outflow (cfs) |
|------------|-----------------|-----------------|-----------------|---------------|
| 692 | 0.11 | 0.03 | 0.29 | 0.43 |
| 696 | 0.12 | 0.03 | 0.30 | 0.44 |
| 700 | 0.12 | 0.03 | 0.31 | 0.46 |
| 704 | 0.13 | 0.03 | 0.32 | 0.48 |
| 708 | 0.14 | 0.05 | 0.34 | 0.53 |
| 712 | 0.15 | 0.10 | 0.36 | 0.61 |
| 716 | 0.17 | 0.14 | 0.38 | 0.70 |
| 720 | 0.19 | 0.19 | 0.41 | 0.79 |
| 724 | 0.21 | 0.24 | 0.44 | 0.89 |
| 728 | 0.24 | 0.43 | 0.47 | 1.22 |
| 732 | 0.26 | 0.92 | 0.49 | 1.95 |
| 736 | 0.28 | 1.49 | 0.51 | 2.77 |
| 740 | 0.29 | 1.97 | 0.52 | 3.41 |
| 744 | 0.30 | 2.30 | 0.56 | 3.82 |
| 748 | 0.31 | 2.47 | 0.67 | 4.07 |
| 752 | 0.32 | 2.53 | 0.80 | 4.19 |
| 756 | 0.32 | 2.51 | 0.92 | 4.19 |
| 760 | 0.33 | 2.44 | 1.00 | 4.09 |
| 764 | 0.33 | 2.33 | 1.05 | 3.95 |
| 768 | 0.33 | 2.21 | 1.09 | 3.79 |
| 772 | 0.33 | 2.08 | 1.12 | 3.64 |
| 776 | 0.33 | 1.97 | 1.14 | 3.49 |
| 780 | 0.34 | 1.86 | 1.15 | 3.35 |
| 784 | 0.34 | 1.76 | 1.15 << | 3.23 |
| 788 | 0.34 | 1.67 | 1.15 | 3.12 |
| 792 | 0.34 | 1.58 | 1.14 | 3.01 |
| 796 | 0.34 | 1.50 | 1.13 | 2.90 |
| 800 | 0.34 | 1.43 | 1.12 | 2.81 |
| 804 | 0.34 | 1.36 | 1.11 | 2.72 |
| 808 | 0.34 | 1.30 | 1.10 | 2.64 |
| 812 | 0.34 | 1.25 | 1.09 | 2.57 |
| 816 | 0.34 | 1.20 | 1.07 | 2.51 |
| 820 | 0.35 | 1.15 | 1.06 | 2.46 |
| 824 | 0.35 | 1.11 | 1.05 | 2.40 |
| 828 | 0.35 | 1.07 | 1.03 | 2.35 |
| 832 | 0.35 | 1.03 | 1.01 | 2.30 |
| 836 | 0.35 | 0.99 | 1.00 | 2.25 |
| 840 | 0.35 | 0.96 | 0.98 | 2.20 |

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Hydrograph Discharge Table

| Time (min) | Hyd. 11 + (cfs) | Hyd. 12 + (cfs) | Hyd. 13 = (cfs) | Outflow (cfs) |
|---------------|--------------------|--------------------|--------------------|------------------|
| 844 | 0.35 | 0.92 | 0.96 | 2.16 |
| 848 | 0.35 | 0.89 | 0.94 | 2.11 |
| 852 | 0.35 | 0.86 | 0.93 | 2.07 |
| 856 | 0.35 | 0.84 | 0.91 | 2.02 |
| 860 | 0.35 | 0.82 | 0.89 | 1.98 |
| 864 | 0.35 | 0.80 | 0.88 | 1.94 |
| 868 | 0.35 | 0.78 | 0.86 | 1.91 |
| 872 | 0.35 | 0.76 | 0.85 | 1.87 |
| 876 | 0.35 | 0.74 | 0.83 | 1.84 |
| 880 | 0.35 | 0.72 | 0.82 | 1.81 |
| 884 | 0.35 | 0.70 | 0.80 | 1.78 |
| 888 | 0.35 | 0.69 | 0.79 | 1.75 |
| 892 | 0.35 | 0.67 | 0.77 | 1.72 |
| 896 | 0.35 | 0.66 | 0.76 | 1.69 |
| 900 | 0.35 | 0.64 | 0.75 | 1.67 |
| 904 | 0.35 | 0.63 | 0.73 | 1.65 |
| 908 | 0.35 | 0.61 | 0.72 | 1.63 |
| 912 | 0.35 | 0.60 | 0.71 | 1.61 |
| 916 | 0.35 | 0.59 | 0.71 | 1.60 |
| 920 | 0.35 | 0.57 | 0.70 | 1.59 |
| 924 | 0.35 | 0.56 | 0.70 | 1.57 |
| 928 | 0.35 | 0.55 | 0.69 | 1.56 |
| 932 | 0.35 | 0.54 | 0.68 | 1.54 |
| 936 | 0.35 | 0.53 | 0.68 | 1.53 |
| 940 | 0.35 | 0.51 | 0.67 | 1.51 |
| 944 | 0.35 | 0.50 | 0.66 | 1.50 |
| 948 | 0.35 | 0.49 | 0.66 | 1.48 |
| 952 | 0.35 | 0.48 | 0.65 | 1.47 |
| 956 | 0.35 | 0.48 | 0.64 | 1.45 |
| 960 | 0.35 | 0.47 | 0.64 | 1.44 |
| 964 | 0.35 | 0.46 | 0.63 | 1.42 |
| 968 | 0.35 | 0.46 | 0.62 | 1.40 |
| 972 | 0.35 | 0.45 | 0.61 | 1.39 |
| 976 | 0.35 | 0.44 | 0.60 | 1.37 |
| 980 | 0.35 | 0.44 | 0.60 | 1.36 |
| 984 | 0.35 | 0.43 | 0.59 | 1.34 |
| 988 | 0.35 | 0.42 | 0.58 | 1.33 |
| 992 | 0.35 | 0.42 | 0.58 | 1.31 |
| 996 | 0.35 | 0.41 | 0.57 | 1.30 |
| 1000 | 0.35 | 0.41 | 0.56 | 1.28 |
| 1004 | 0.35 | 0.40 | 0.55 | 1.27 |
| 1008 | 0.35 | 0.39 | 0.55 | 1.26 |
| 1012 | 0.35 | 0.39 | 0.54 | 1.24 |
| 1016 | 0.35 | 0.38 | 0.53 | 1.23 |
| 1020 | 0.35 | 0.38 | 0.53 | 1.22 |
| 1024 | 0.34 | 0.37 | 0.53 | 1.21 |
| 1028 | 0.34 | 0.37 | 0.53 | 1.20 |
| 1032 | 0.34 | 0.36 | 0.53 | 1.20 |
| 1036 | 0.34 | 0.36 | 0.53 | 1.19 |
| 1040 | 0.34 | 0.35 | 0.53 | 1.18 |
| 1044 | 0.34 | 0.35 | 0.53 | 1.18 |

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Hydrograph Discharge Table

| Time (min) | Hyd. 11 + (cfs) | Hyd. 12 + (cfs) | Hyd. 13 = (cfs) | Outflow (cfs) |
|---------------|--------------------|--------------------|--------------------|------------------|
| 1048 | 0.34 | 0.34 | 0.52 | 1.17 |
| 1052 | 0.34 | 0.34 | 0.52 | 1.17 |
| 1056 | 0.34 | 0.33 | 0.52 | 1.16 |
| 1060 | 0.34 | 0.33 | 0.52 | 1.15 |
| 1064 | 0.34 | 0.32 | 0.52 | 1.15 |
| 1068 | 0.34 | 0.32 | 0.52 | 1.14 |
| 1072 | 0.34 | 0.31 | 0.52 | 1.14 |
| 1076 | 0.34 | 0.31 | 0.52 | 1.13 |
| 1080 | 0.34 | 0.30 | 0.52 | 1.13 |
| 1084 | 0.34 | 0.30 | 0.52 | 1.12 |
| 1088 | 0.34 | 0.29 | 0.52 | 1.12 |
| 1092 | 0.34 | 0.29 | 0.52 | 1.12 |
| 1096 | 0.34 | 0.28 | 0.52 | 1.11 |
| 1100 | 0.34 | 0.28 | 0.52 | 1.11 |
| 1104 | 0.34 | 0.27 | 0.52 | 1.11 |
| 1108 | 0.33 | 0.27 | 0.52 | 1.11 |
| 1112 | 0.33 | 0.27 | 0.51 | 1.11 |
| 1116 | 0.33 | 0.26 | 0.51 | 1.11 |
| 1120 | 0.33 | 0.26 | 0.51 | 1.10 |
| 1124 | 0.33 | 0.26 | 0.51 | 1.10 |
| 1128 | 0.33 | 0.26 | 0.51 | 1.10 |
| 1132 | 0.33 | 0.26 | 0.51 | 1.10 |
| 1136 | 0.33 | 0.26 | 0.51 | 1.10 |
| 1140 | 0.33 | 0.26 | 0.51 | 1.09 |
| 1144 | 0.33 | 0.26 | 0.51 | 1.09 |
| 1148 | 0.33 | 0.26 | 0.51 | 1.09 |
| 1152 | 0.33 | 0.26 | 0.51 | 1.09 |
| 1156 | 0.33 | 0.26 | 0.51 | 1.09 |
| 1160 | 0.33 | 0.25 | 0.51 | 1.08 |
| 1164 | 0.33 | 0.25 | 0.51 | 1.08 |
| 1168 | 0.33 | 0.25 | 0.51 | 1.08 |
| 1172 | 0.33 | 0.25 | 0.50 | 1.08 |
| 1176 | 0.33 | 0.25 | 0.50 | 1.08 |
| 1180 | 0.32 | 0.25 | 0.50 | 1.07 |
| 1184 | 0.32 | 0.25 | 0.50 | 1.07 |
| 1188 | 0.32 | 0.25 | 0.50 | 1.07 |
| 1192 | 0.32 | 0.25 | 0.50 | 1.07 |
| 1196 | 0.32 | 0.25 | 0.50 | 1.07 |
| 1200 | 0.32 | 0.25 | 0.50 | 1.06 |
| 1204 | 0.32 | 0.25 | 0.50 | 1.06 |
| 1208 | 0.32 | 0.25 | 0.50 | 1.06 |
| 1212 | 0.32 | 0.24 | 0.50 | 1.06 |
| 1216 | 0.32 | 0.24 | 0.50 | 1.05 |
| 1220 | 0.32 | 0.24 | 0.50 | 1.05 |
| 1224 | 0.32 | 0.24 | 0.49 | 1.05 |
| 1228 | 0.32 | 0.24 | 0.49 | 1.05 |
| 1232 | 0.32 | 0.24 | 0.49 | 1.05 |
| 1236 | 0.32 | 0.24 | 0.49 | 1.04 |
| 1240 | 0.32 | 0.24 | 0.49 | 1.04 |
| 1244 | 0.31 | 0.24 | 0.49 | 1.04 |
| 1248 | 0.31 | 0.24 | 0.49 | 1.04 |

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Hydrograph Discharge Table

| Time (min) | Hyd. 11 + (cfs) | Hyd. 12 + (cfs) | Hyd. 13 = (cfs) | Outflow (cfs) |
|---------------|--------------------|--------------------|--------------------|------------------|
| 1252 | 0.31 | 0.24 | 0.49 | 1.03 |
| 1256 | 0.31 | 0.24 | 0.49 | 1.03 |
| 1260 | 0.31 | 0.23 | 0.49 | 1.03 |
| 1264 | 0.31 | 0.23 | 0.49 | 1.03 |
| 1268 | 0.31 | 0.23 | 0.49 | 1.03 |
| 1272 | 0.31 | 0.23 | 0.49 | 1.02 |
| 1276 | 0.31 | 0.23 | 0.48 | 1.02 |
| 1280 | 0.31 | 0.23 | 0.48 | 1.02 |
| 1284 | 0.31 | 0.23 | 0.48 | 1.02 |
| 1288 | 0.31 | 0.23 | 0.48 | 1.01 |
| 1292 | 0.31 | 0.23 | 0.48 | 1.01 |
| 1296 | 0.31 | 0.23 | 0.48 | 1.01 |
| 1300 | 0.31 | 0.22 | 0.48 | 1.01 |
| 1304 | 0.31 | 0.22 | 0.48 | 1.00 |
| 1308 | 0.30 | 0.22 | 0.48 | 1.00 |
| 1312 | 0.30 | 0.22 | 0.48 | 1.00 |
| 1316 | 0.30 | 0.22 | 0.48 | 1.00 |
| 1320 | 0.30 | 0.22 | 0.48 | 0.99 |
| 1324 | 0.30 | 0.22 | 0.48 | 0.99 |
| 1328 | 0.30 | 0.22 | 0.47 | 0.99 |
| 1332 | 0.30 | 0.22 | 0.47 | 0.99 |
| 1336 | 0.30 | 0.22 | 0.47 | 0.99 |
| 1340 | 0.30 | 0.22 | 0.47 | 0.98 |
| 1344 | 0.30 | 0.22 | 0.47 | 0.98 |
| 1348 | 0.30 | 0.21 | 0.47 | 0.98 |
| 1352 | 0.30 | 0.21 | 0.47 | 0.98 |
| 1356 | 0.30 | 0.21 | 0.47 | 0.97 |
| 1360 | 0.30 | 0.21 | 0.47 | 0.97 |
| 1364 | 0.30 | 0.21 | 0.47 | 0.97 |
| 1368 | 0.30 | 0.21 | 0.47 | 0.97 |
| 1372 | 0.29 | 0.21 | 0.47 | 0.97 |
| 1376 | 0.29 | 0.21 | 0.46 | 0.96 |
| 1380 | 0.29 | 0.21 | 0.46 | 0.96 |
| 1384 | 0.29 | 0.21 | 0.46 | 0.96 |
| 1388 | 0.29 | 0.20 | 0.46 | 0.96 |
| 1392 | 0.29 | 0.20 | 0.46 | 0.95 |
| 1396 | 0.29 | 0.20 | 0.46 | 0.95 |
| 1400 | 0.29 | 0.20 | 0.46 | 0.95 |
| 1404 | 0.29 | 0.20 | 0.46 | 0.95 |
| 1408 | 0.29 | 0.20 | 0.46 | 0.94 |
| 1412 | 0.29 | 0.20 | 0.46 | 0.94 |
| 1416 | 0.29 | 0.20 | 0.46 | 0.94 |
| 1420 | 0.29 | 0.20 | 0.46 | 0.93 |
| 1424 | 0.29 | 0.20 | 0.45 | 0.93 |
| 1428 | 0.28 | 0.19 | 0.45 | 0.93 |
| 1432 | 0.28 | 0.19 | 0.45 | 0.93 |
| 1436 | 0.28 | 0.19 | 0.45 | 0.92 |
| 1440 | 0.28 | 0.19 | 0.45 | 0.92 |
| 1444 | 0.28 | 0.19 | 0.45 | 0.92 |
| 1448 | 0.28 | 0.19 | 0.45 | 0.92 |
| 1452 | 0.28 | 0.19 | 0.45 | 0.91 |

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Hydrograph Discharge Table

| Time (min) | Hyd. 11 + (cfs) | Hyd. 12 + (cfs) | Hyd. 13 = (cfs) | Outflow (cfs) |
|---------------|--------------------|--------------------|--------------------|------------------|
| 1456 | 0.28 | 0.19 | 0.45 | 0.91 |
| 1460 | 0.28 | 0.18 | 0.45 | 0.90 |
| 1464 | 0.28 | 0.18 | 0.44 | 0.90 |
| 1468 | 0.28 | 0.18 | 0.44 | 0.89 |
| 1472 | 0.28 | 0.18 | 0.44 | 0.89 |
| 1476 | 0.27 | 0.17 | 0.44 | 0.89 |
| 1480 | 0.27 | 0.17 | 0.44 | 0.88 |
| 1484 | 0.27 | 0.17 | 0.44 | 0.88 |
| 1488 | 0.27 | 0.17 | 0.44 | 0.87 |
| 1492 | 0.27 | 0.17 | 0.44 | 0.87 |
| 1496 | 0.27 | 0.16 | 0.43 | 0.86 |
| 1500 | 0.27 | 0.16 | 0.43 | 0.86 |
| 1504 | 0.27 | 0.16 | 0.43 | 0.86 |
| 1508 | 0.27 | 0.16 | 0.43 | 0.85 |
| 1512 | 0.27 | 0.16 | 0.43 | 0.85 |
| 1516 | 0.26 | 0.15 | 0.43 | 0.84 |
| 1520 | 0.26 | 0.15 | 0.43 | 0.84 |
| 1524 | 0.26 | 0.15 | 0.43 | 0.83 |
| 1528 | 0.26 | 0.14 | 0.42 | 0.83 |
| 1532 | 0.26 | 0.14 | 0.42 | 0.82 |
| 1536 | 0.26 | 0.14 | 0.42 | 0.82 |
| 1540 | 0.26 | 0.14 | 0.42 | 0.81 |
| 1544 | 0.26 | 0.13 | 0.42 | 0.81 |
| 1548 | 0.26 | 0.13 | 0.42 | 0.80 |
| 1552 | 0.26 | 0.13 | 0.42 | 0.80 |
| 1556 | 0.25 | 0.13 | 0.42 | 0.79 |
| 1560 | 0.25 | 0.12 | 0.41 | 0.79 |
| 1564 | 0.25 | 0.12 | 0.41 | 0.78 |
| 1568 | 0.25 | 0.12 | 0.41 | 0.78 |
| 1572 | 0.25 | 0.12 | 0.41 | 0.78 |
| 1576 | 0.25 | 0.12 | 0.41 | 0.77 |
| 1580 | 0.25 | 0.11 | 0.41 | 0.77 |
| 1584 | 0.25 | 0.11 | 0.41 | 0.76 |
| 1588 | 0.25 | 0.11 | 0.40 | 0.76 |
| 1592 | 0.25 | 0.11 | 0.40 | 0.75 |
| 1596 | 0.24 | 0.11 | 0.40 | 0.75 |
| 1600 | 0.24 | 0.10 | 0.40 | 0.74 |
| 1604 | 0.24 | 0.10 | 0.39 | 0.74 |
| 1608 | 0.24 | 0.10 | 0.39 | 0.73 |
| 1612 | 0.24 | 0.10 | 0.39 | 0.73 |
| 1616 | 0.24 | 0.10 | 0.39 | 0.72 |
| 1620 | 0.24 | 0.09 | 0.39 | 0.72 |
| 1624 | 0.24 | 0.09 | 0.38 | 0.71 |
| 1628 | 0.24 | 0.09 | 0.38 | 0.71 |
| 1632 | 0.24 | 0.09 | 0.38 | 0.70 |
| 1636 | 0.23 | 0.09 | 0.38 | 0.70 |
| 1640 | 0.23 | 0.09 | 0.37 | 0.69 |
| 1644 | 0.23 | 0.08 | 0.37 | 0.69 |
| 1648 | 0.23 | 0.08 | 0.37 | 0.68 |
| 1652 | 0.23 | 0.08 | 0.37 | 0.68 |
| 1656 | 0.23 | 0.08 | 0.37 | 0.67 |

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Hydrograph Discharge Table

| Time (min) | Hyd. 11 + (cfs) | Hyd. 12 + (cfs) | Hyd. 13 = (cfs) | Outflow (cfs) |
|---------------|--------------------|--------------------|--------------------|------------------|
| 1660 | 0.23 | 0.08 | 0.36 | 0.67 |
| 1664 | 0.23 | 0.08 | 0.36 | 0.66 |
| 1668 | 0.23 | 0.07 | 0.36 | 0.66 |
| 1672 | 0.23 | 0.07 | 0.36 | 0.65 |
| 1676 | 0.22 | 0.07 | 0.36 | 0.65 |
| 1680 | 0.22 | 0.07 | 0.35 | 0.64 |
| 1684 | 0.22 | 0.07 | 0.35 | 0.64 |
| 1688 | 0.22 | 0.07 | 0.35 | 0.64 |
| 1692 | 0.22 | 0.07 | 0.35 | 0.63 |
| 1696 | 0.22 | 0.07 | 0.34 | 0.63 |
| 1700 | 0.22 | 0.06 | 0.34 | 0.62 |
| 1704 | 0.22 | 0.06 | 0.34 | 0.62 |
| 1708 | 0.22 | 0.06 | 0.34 | 0.61 |
| 1712 | 0.22 | 0.06 | 0.34 | 0.61 |
| 1716 | 0.21 | 0.06 | 0.33 | 0.60 |
| 1720 | 0.21 | 0.06 | 0.33 | 0.60 |
| 1724 | 0.21 | 0.06 | 0.33 | 0.60 |
| 1728 | 0.21 | 0.06 | 0.33 | 0.59 |
| 1732 | 0.21 | 0.05 | 0.32 | 0.59 |
| 1736 | 0.21 | 0.05 | 0.32 | 0.58 |
| 1740 | 0.21 | 0.05 | 0.32 | 0.58 |
| 1744 | 0.21 | 0.05 | 0.32 | 0.58 |
| 1748 | 0.21 | 0.05 | 0.32 | 0.57 |
| 1752 | 0.20 | 0.05 | 0.31 | 0.57 |
| 1756 | 0.20 | 0.05 | 0.31 | 0.56 |
| 1760 | 0.20 | 0.05 | 0.31 | 0.56 |
| 1764 | 0.20 | 0.05 | 0.31 | 0.55 |
| 1768 | 0.20 | 0.05 | 0.31 | 0.55 |
| 1772 | 0.20 | 0.04 | 0.30 | 0.55 |
| 1776 | 0.20 | 0.04 | 0.30 | 0.54 |
| 1780 | 0.20 | 0.04 | 0.30 | 0.54 |
| 1784 | 0.20 | 0.04 | 0.30 | 0.53 |
| 1788 | 0.20 | 0.04 | 0.29 | 0.53 |
| 1792 | 0.20 | 0.04 | 0.29 | 0.53 |
| 1796 | 0.19 | 0.04 | 0.29 | 0.52 |
| 1800 | 0.19 | 0.04 | 0.29 | 0.52 |
| 1804 | 0.19 | 0.04 | 0.29 | 0.51 |
| 1808 | 0.19 | 0.04 | 0.28 | 0.51 |
| 1812 | 0.19 | 0.04 | 0.28 | 0.51 |
| 1816 | 0.19 | 0.04 | 0.28 | 0.50 |
| 1820 | 0.19 | 0.04 | 0.28 | 0.50 |
| 1824 | 0.19 | 0.03 | 0.27 | 0.50 |
| 1828 | 0.19 | 0.03 | 0.27 | 0.49 |
| 1832 | 0.18 | 0.03 | 0.27 | 0.49 |
| 1836 | 0.18 | 0.03 | 0.27 | 0.48 |
| 1840 | 0.18 | 0.03 | 0.27 | 0.48 |
| 1844 | 0.18 | 0.03 | 0.26 | 0.48 |
| 1848 | 0.18 | 0.03 | 0.26 | 0.47 |
| 1852 | 0.18 | 0.03 | 0.26 | 0.47 |
| 1856 | 0.18 | 0.03 | 0.26 | 0.47 |
| 1860 | 0.18 | 0.03 | 0.26 | 0.46 |

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Hydrograph Discharge Table

| Time (min) | Hyd. 11 + (cfs) | Hyd. 12 + (cfs) | Hyd. 13 = (cfs) | Outflow (cfs) |
|-----------------------|----------------------------|----------------------------|----------------------------|--------------------------|
| 1864 | 0.18 | 0.03 | 0.25 | 0.46 |
| 1868 | 0.18 | 0.03 | 0.25 | 0.46 |
| 1872 | 0.17 | 0.03 | 0.25 | 0.45 |
| 1876 | 0.17 | 0.03 | 0.25 | 0.45 |
| 1880 | 0.17 | 0.03 | 0.24 | 0.45 |
| 1884 | 0.17 | 0.03 | 0.24 | 0.44 |
| 1888 | 0.17 | 0.03 | 0.24 | 0.44 |
| 1892 | 0.17 | 0.03 | 0.24 | 0.44 |
| 1896 | 0.17 | 0.03 | 0.23 | 0.43 |
| 1900 | 0.17 | 0.03 | 0.23 | 0.42 |

...End

Hydrograph Summary Report

| Hyd. No. | Hydrograph type (origin) | Peak flow (cfs) | Time interval (min) | Time to peak (min) | Volume (cuft) | Inflow hyd(s) | Maximum elevation (ft) | Maximum storage (cuft) | Hydrograph description |
|----------|--------------------------|-----------------|---------------------|--------------------|---------------|---------------|------------------------|------------------------|------------------------|
| 1 | SCS Runoff | 12.27 | 2 | 732 | 52,906 | --- | ---- | ---- | Predevelopment |
| 2 | SCS Runoff | 7.37 | 2 | 728 | 28,594 | --- | ---- | ---- | Post Subarea 1a |
| 3 | SCS Runoff | 0.54 | 2 | 724 | 1,722 | --- | ---- | ---- | Post Subarea 1b |
| 4 | SCS Runoff | 8.53 | 2 | 730 | 35,615 | --- | ---- | ---- | Post Subarea 2a |
| 5 | SCS Runoff | 0.53 | 2 | 724 | 1,661 | --- | ---- | ---- | Post Subarea 2b |
| 6 | SCS Runoff | 13.26 | 2 | 726 | 45,970 | --- | ---- | ---- | Post Subarea 3a |
| 7 | SCS Runoff | 0.68 | 2 | 724 | 2,153 | --- | ---- | ---- | Post Subarea 3b |
| 8 | Combine | 7.79 | 2 | 728 | 30,316 | 2, 3, | ---- | ---- | Basin 1 In |
| 9 | Combine | 8.86 | 2 | 730 | 37,276 | 4, 5, | ---- | ---- | Basin 2 In |
| 10 | Combine | 13.90 | 2 | 726 | 48,122 | 6, 7, | ---- | ---- | Basin 3 In |
| 11 | Reservoir | 0.39 | 2 | 924 | 29,889 | 8 | 242.87 | 30,290 | Basin 1 Out |
| 12 | Reservoir | 3.63 | 2 | 750 | 34,040 | 9 | 233.29 | 16,862 | Basin 2 Out |
| 13 | Reservoir | 2.45 | 2 | 756 | 48,122 | 10 | 224.75 | 22,581 | Basin 3 Out |
| 14 | Combine | 7.01 | 2 | 750 | 112,061 | 11, 12, 13 | ---- | ---- | |

Hydrograph Report

Hyd. No. 1

Predevelopment

| | | | |
|-----------------|--------------|--------------------|-------------|
| Hydrograph type | = SCS Runoff | Peak discharge | = 12.27 cfs |
| Storm frequency | = 25 yrs | Time interval | = 2 min |
| Drainage area | = 8.27 ac | Curve number | = 61 |
| Basin Slope | = 0.0 % | Hydraulic length | = 0 ft |
| Tc method | = USER | Time of conc. (Tc) | = 14.4 min |
| Total precip. | = 5.70 in | Distribution | = Type III |
| Storm duration | = 24 hrs | Shape factor | = 484 |

Hydrograph Volume = 52,906 cuft

Hydrograph Discharge Table

| Time (min) | Outflow (cfs) | Time (min) | Outflow (cfs) | Time (min) | Outflow (cfs) |
|------------|---------------|------------|---------------|------------|---------------|
| 698 | 0.68 | 834 | 1.45 | 970 | 0.74 |
| 702 | 0.95 | 838 | 1.41 | 974 | 0.73 |
| 706 | 1.39 | 842 | 1.38 | 978 | 0.71 |
| 710 | 2.01 | 846 | 1.34 | 982 | 0.71 |
| 714 | 2.82 | 850 | 1.31 | 986 | 0.70 |
| 718 | 4.07 | 854 | 1.29 | 990 | 0.69 |
| 722 | 6.54 | 858 | 1.26 | 994 | 0.68 |
| 726 | 9.83 | 862 | 1.25 | 998 | 0.67 |
| 730 | 12.05 | 866 | 1.23 | 1002 | 0.66 |
| 734 | 12.03 | 870 | 1.21 | 1006 | 0.65 |
| 738 | 10.86 | 874 | 1.19 | 1010 | 0.64 |
| 742 | 9.17 | 878 | 1.18 | 1014 | 0.64 |
| 746 | 7.46 | 882 | 1.16 | 1018 | 0.63 |
| 750 | 6.20 | 886 | 1.14 | 1022 | 0.62 |
| 754 | 5.07 | 890 | 1.12 | | |
| 758 | 4.04 | 894 | 1.10 | | |
| 762 | 3.29 | 898 | 1.09 | ...End | |
| 766 | 2.82 | 902 | 1.07 | | |
| 770 | 2.55 | 906 | 1.05 | | |
| 774 | 2.39 | 910 | 1.03 | | |
| 778 | 2.26 | 914 | 1.01 | | |
| 782 | 2.13 | 918 | 0.99 | | |
| 786 | 2.00 | 922 | 0.97 | | |
| 790 | 1.90 | 926 | 0.95 | | |
| 794 | 1.82 | 930 | 0.93 | | |
| 798 | 1.77 | 934 | 0.91 | | |
| 802 | 1.73 | 938 | 0.89 | | |
| 806 | 1.70 | 942 | 0.87 | | |
| 810 | 1.66 | 946 | 0.85 | | |
| 814 | 1.63 | 950 | 0.83 | | |
| 818 | 1.59 | 954 | 0.81 | | |
| 822 | 1.56 | 958 | 0.79 | | |
| 826 | 1.52 | 962 | 0.77 | | |
| 830 | 1.49 | 966 | 0.76 | | |

Hydrograph Report

Hyd. No. 2

Post Subarea 1a

| | | | |
|-----------------|--------------|--------------------|------------|
| Hydrograph type | = SCS Runoff | Peak discharge | = 7.37 cfs |
| Storm frequency | = 25 yrs | Time interval | = 2 min |
| Drainage area | = 1.90 ac | Curve number | = 85 |
| Basin Slope | = 0.0 % | Hydraulic length | = 0 ft |
| Tc method | = USER | Time of conc. (Tc) | = 10.6 min |
| Total precip. | = 5.70 in | Distribution | = Type III |
| Storm duration | = 24 hrs | Shape factor | = 484 |

Hydrograph Volume = 28,594 cuft

Hydrograph Discharge Table

| Time (min) | Outflow (cfs) | Time (min) | Outflow (cfs) | Time (min) | Outflow (cfs) |
|------------|---------------|------------|---------------|------------|---------------|
| 636 | 0.37 | 772 | 1.00 | 908 | 0.39 |
| 640 | 0.39 | 776 | 0.94 | 912 | 0.38 |
| 644 | 0.40 | 780 | 0.88 | 916 | 0.38 |
| 648 | 0.42 | 784 | 0.82 | | |
| 652 | 0.43 | 788 | 0.77 | | |
| 656 | 0.45 | 792 | 0.74 | ...End | |
| 660 | 0.47 | 796 | 0.72 | | |
| 664 | 0.48 | 800 | 0.70 | | |
| 668 | 0.51 | 804 | 0.68 | | |
| 672 | 0.55 | 808 | 0.67 | | |
| 676 | 0.59 | 812 | 0.65 | | |
| 680 | 0.64 | 816 | 0.64 | | |
| 684 | 0.70 | 820 | 0.62 | | |
| 688 | 0.75 | 824 | 0.61 | | |
| 692 | 0.81 | 828 | 0.59 | | |
| 696 | 0.93 | 832 | 0.57 | | |
| 700 | 1.18 | 836 | 0.56 | | |
| 704 | 1.55 | 840 | 0.54 | | |
| 708 | 2.02 | 844 | 0.53 | | |
| 712 | 2.55 | 848 | 0.51 | | |
| 716 | 3.16 | 852 | 0.50 | | |
| 720 | 4.34 | 856 | 0.49 | | |
| 724 | 6.27 | 860 | 0.48 | | |
| 728 | 7.37 << | 864 | 0.48 | | |
| 732 | 6.80 | 868 | 0.47 | | |
| 736 | 5.56 | 872 | 0.46 | | |
| 740 | 4.27 | 876 | 0.45 | | |
| 744 | 3.38 | 880 | 0.45 | | |
| 748 | 2.79 | 884 | 0.44 | | |
| 752 | 2.22 | 888 | 0.43 | | |
| 756 | 1.72 | 892 | 0.42 | | |
| 760 | 1.37 | 896 | 0.41 | | |
| 764 | 1.17 | 900 | 0.41 | | |
| 768 | 1.07 | 904 | 0.40 | | |

Hydrograph Report

Hyd. No. 3

Post Subarea 1b

Hydrograph type = SCS Runoff
Storm frequency = 25 yrs
Drainage area = 0.28 ac
Basin Slope = 0.0 %
Tc method = USER
Total precip. = 5.70 in
Storm duration = 24 hrs

Peak discharge = 0.54 cfs
Time interval = 2 min
Curve number = 61
Hydraulic length = 0 ft
Time of conc. (Tc) = 6 min
Distribution = Type III
Shape factor = 484

Hydrograph Volume = 1,722 cuft

Hydrograph Discharge Table

| Time (min) | Outflow (cfs) | Time (min) | Outflow (cfs) |
|------------|---------------|------------|---------------|
| 696 | 0.03 | 832 | 0.05 |
| 700 | 0.05 | 836 | 0.04 |
| 704 | 0.07 | 840 | 0.04 |
| 708 | 0.10 | 844 | 0.04 |
| 712 | 0.13 | 848 | 0.04 |
| 716 | 0.18 | 852 | 0.04 |
| 720 | 0.36 | 856 | 0.04 |
| 724 | 0.54 << | 860 | 0.04 |
| 728 | 0.43 | 864 | 0.04 |
| 732 | 0.30 | 868 | 0.04 |
| 736 | 0.26 | 872 | 0.04 |
| 740 | 0.23 | 876 | 0.04 |
| 744 | 0.19 | 880 | 0.04 |
| 748 | 0.15 | 884 | 0.04 |
| 752 | 0.11 | 888 | 0.04 |
| 756 | 0.09 | 892 | 0.04 |
| 760 | 0.08 | 896 | 0.03 |
| 764 | 0.08 | 900 | 0.03 |
| 768 | 0.08 | 904 | 0.03 |
| 772 | 0.07 | 908 | 0.03 |
| 776 | 0.07 | 912 | 0.03 |
| 780 | 0.06 | 916 | 0.03 |
| 784 | 0.06 | 920 | 0.03 |
| 788 | 0.06 | 924 | 0.03 |
| 792 | 0.06 | 928 | 0.03 |
| 796 | 0.06 | 932 | 0.03 |
| 800 | 0.05 | 936 | 0.03 |
| 804 | 0.05 | 940 | 0.03 |
| 808 | 0.05 | | |
| 812 | 0.05 | | |
| 816 | 0.05 | ...End | |
| 820 | 0.05 | | |
| 824 | 0.05 | | |
| 828 | 0.05 | | |

Hydrograph Report

Hyd. No. 4

Post Subarea 2a

| | | | |
|-----------------|--------------|--------------------|------------|
| Hydrograph type | = SCS Runoff | Peak discharge | = 8.53 cfs |
| Storm frequency | = 25 yrs | Time interval | = 2 min |
| Drainage area | = 2.32 ac | Curve number | = 88 |
| Basin Slope | = 0.0 % | Hydraulic length | = 0 ft |
| Tc method | = USER | Time of conc. (Tc) | = 14.5 min |
| Total precip. | = 5.70 in | Distribution | = Type III |
| Storm duration | = 24 hrs | Shape factor | = 484 |

Hydrograph Volume = 35,615 cuft

Hydrograph Discharge Table

| Time -- Outflow (min cfs) | Time -- Outflow (min cfs) | Time -- Outflow (min cfs) |
|------------------------------|------------------------------|------------------------------|
| 622 0.43 | 758 2.11 | 894 0.50 |
| 626 0.45 | 762 1.69 | 898 0.49 |
| 630 0.47 | 766 1.44 | 902 0.48 |
| 634 0.49 | 770 1.29 | 906 0.47 |
| 638 0.51 | 774 1.20 | 910 0.46 |
| 642 0.53 | 778 1.13 | 914 0.46 |
| 646 0.54 | 782 1.05 | 918 0.45 |
| 650 0.56 | 786 0.99 | 922 0.44 |
| 654 0.58 | 790 0.93 | 926 0.43 |
| 658 0.60 | 794 0.89 | |
| 662 0.62 | 798 0.86 | |
| 666 0.65 | 802 0.84 | ...End |
| 670 0.68 | 806 0.82 | |
| 674 0.73 | 810 0.80 | |
| 678 0.79 | 814 0.78 | |
| 682 0.85 | 818 0.76 | |
| 686 0.92 | 822 0.74 | |
| 690 0.98 | 826 0.72 | |
| 694 1.07 | 830 0.70 | |
| 698 1.25 | 834 0.68 | |
| 702 1.57 | 838 0.66 | |
| 706 2.03 | 842 0.64 | |
| 710 2.60 | 846 0.63 | |
| 714 3.25 | 850 0.61 | |
| 718 4.12 | 854 0.60 | |
| 722 5.70 | 858 0.59 | |
| 726 7.59 | 862 0.58 | |
| 730 8.53 << | 866 0.57 | |
| 734 7.96 | 870 0.56 | |
| 738 6.76 | 874 0.55 | |
| 742 5.37 | 878 0.54 | |
| 746 4.16 | 882 0.53 | |
| 750 3.35 | 886 0.52 | |
| 754 2.68 | 890 0.51 | |

Hydrograph Report

Hyd. No. 5

Post Subarea 2b

Hydrograph type = SCS Runoff
Storm frequency = 25 yrs
Drainage area = 0.27 ac
Basin Slope = 0.0 %
Tc method = USER
Total precip. = 5.70 in
Storm duration = 24 hrs

Peak discharge = 0.53 cfs
Time interval = 2 min
Curve number = 61
Hydraulic length = 0 ft
Time of conc. (Tc) = 6 min
Distribution = Type III
Shape factor = 484

Hydrograph Volume = 1,661 cuft

Hydrograph Discharge Table

| Time (min) | Outflow (cfs) | Time (min) | Outflow (cfs) |
|------------|---------------|------------|---------------|
| 696 | 0.03 | 832 | 0.04 |
| 700 | 0.05 | 836 | 0.04 |
| 704 | 0.07 | 840 | 0.04 |
| 708 | 0.09 | 844 | 0.04 |
| 712 | 0.13 | 848 | 0.04 |
| 716 | 0.18 | 852 | 0.04 |
| 720 | 0.35 | 856 | 0.04 |
| 724 | 0.53 << | 860 | 0.04 |
| 728 | 0.41 | 864 | 0.04 |
| 732 | 0.29 | 868 | 0.04 |
| 736 | 0.25 | 872 | 0.04 |
| 740 | 0.22 | 876 | 0.04 |
| 744 | 0.19 | 880 | 0.04 |
| 748 | 0.15 | 884 | 0.04 |
| 752 | 0.11 | 888 | 0.03 |
| 756 | 0.09 | 892 | 0.03 |
| 760 | 0.08 | 896 | 0.03 |
| 764 | 0.08 | 900 | 0.03 |
| 768 | 0.07 | 904 | 0.03 |
| 772 | 0.07 | 908 | 0.03 |
| 776 | 0.07 | 912 | 0.03 |
| 780 | 0.06 | 916 | 0.03 |
| 784 | 0.06 | 920 | 0.03 |
| 788 | 0.06 | 924 | 0.03 |
| 792 | 0.05 | 928 | 0.03 |
| 796 | 0.05 | 932 | 0.03 |
| 800 | 0.05 | 936 | 0.03 |
| 804 | 0.05 | 940 | 0.03 |
| 808 | 0.05 | | |
| 812 | 0.05 | | |
| 816 | 0.05 | ...End | |
| 820 | 0.05 | | |
| 824 | 0.05 | | |
| 828 | 0.05 | | |

Hydrograph Report

Hyd. No. 6

Post Subarea 3a

Hydrograph type = SCS Runoff
Storm frequency = 25 yrs
Drainage area = 3.15 ac
Basin Slope = 0.0 %
Tc method = USER
Total precip. = 5.70 in
Storm duration = 24 hrs

Peak discharge = 13.26 cfs
Time interval = 2 min
Curve number = 85
Hydraulic length = 0 ft
Time of conc. (Tc) = 7.5 min
Distribution = Type III
Shape factor = 484

Hydrograph Volume = 45,970 cuft

Hydrograph Discharge Table

| Time -- Outflow (min cfs) | Time -- Outflow (min cfs) |
|------------------------------|------------------------------|
| 646 0.67 | 782 1.30 |
| 650 0.70 | 786 1.22 |
| 654 0.73 | 790 1.18 |
| 658 0.75 | 794 1.15 |
| 662 0.78 | 798 1.12 |
| 666 0.82 | 802 1.10 |
| 670 0.89 | 806 1.07 |
| 674 0.96 | 810 1.05 |
| 678 1.05 | 814 1.02 |
| 682 1.13 | 818 0.99 |
| 686 1.22 | 822 0.97 |
| 690 1.31 | 826 0.94 |
| 694 1.47 | 830 0.92 |
| 698 1.89 | 834 0.89 |
| 702 2.57 | 838 0.87 |
| 706 3.37 | 842 0.84 |
| 710 4.24 | 846 0.82 |
| 714 5.15 | 850 0.80 |
| 718 6.76 | 854 0.79 |
| 722 10.64 | 858 0.78 |
| 726 13.26 << | 862 0.76 |
| 730 11.33 | 866 0.75 |
| 734 8.14 | 870 0.74 |
| 738 6.21 | 874 0.73 |
| 742 5.24 | 878 0.71 |
| 746 4.33 | 882 0.70 |
| 750 3.41 | 886 0.69 |
| 754 2.56 | 890 0.68 |
| 758 2.03 | 894 0.66 |
| 762 1.80 | |
| 766 1.69 | |
| 770 1.60 | ...End |
| 774 1.50 | |
| 778 1.40 | |

Hydrograph Report

Hyd. No. 7

Post Subarea 3b

Hydrograph type = SCS Runoff
Storm frequency = 25 yrs
Drainage area = 0.35 ac
Basin Slope = 0.0 %
Tc method = USER
Total precip. = 5.70 in
Storm duration = 24 hrs

Peak discharge = 0.68 cfs
Time interval = 2 min
Curve number = 61
Hydraulic length = 0 ft
Time of conc. (Tc) = 6 min
Distribution = Type III
Shape factor = 484

Hydrograph Volume = 2,153 cuft

Hydrograph Discharge Table

| Time -- Outflow (min cfs) | Time -- Outflow (min cfs) |
|------------------------------|------------------------------|
| 696 0.04 | 832 0.06 |
| 700 0.06 | 836 0.06 |
| 704 0.09 | 840 0.05 |
| 708 0.12 | 844 0.05 |
| 712 0.16 | 848 0.05 |
| 716 0.23 | 852 0.05 |
| 720 0.45 | 856 0.05 |
| 724 0.68 << | 860 0.05 |
| 728 0.53 | 864 0.05 |
| 732 0.37 | 868 0.05 |
| 736 0.33 | 872 0.05 |
| 740 0.29 | 876 0.05 |
| 744 0.24 | 880 0.05 |
| 748 0.19 | 884 0.05 |
| 752 0.14 | 888 0.04 |
| 756 0.11 | 892 0.04 |
| 760 0.11 | 896 0.04 |
| 764 0.10 | 900 0.04 |
| 768 0.10 | 904 0.04 |
| 772 0.09 | 908 0.04 |
| 776 0.08 | 912 0.04 |
| 780 0.08 | 916 0.04 |
| 784 0.07 | 920 0.04 |
| 788 0.07 | 924 0.04 |
| 792 0.07 | 928 0.04 |
| 796 0.07 | 932 0.04 |
| 800 0.07 | 936 0.04 |
| 804 0.07 | 940 0.03 |
| 808 0.07 | |
| 812 0.06 | |
| 816 0.06 | ...End |
| 820 0.06 | |
| 824 0.06 | |
| 828 0.06 | |

Hydrograph Report

Hyd. No. 8

Basin 1 In

Hydrograph type = Combine
Storm frequency = 25 yrs
Inflow hyds. = 2, 3

Peak discharge = 7.79 cfs
Time interval = 2 min

Hydrograph Volume = 30,316 cuft

Hydrograph Discharge Table

| Time (min) | Hyd. 2 + (cfs) | Hyd. 3 + (cfs) | Outflow (cfs) |
|------------|----------------|----------------|---------------|
| 644 | 0.40 | 0.00 | 0.40 |
| 648 | 0.42 | 0.00 | 0.42 |
| 652 | 0.43 | 0.00 | 0.44 |
| 656 | 0.45 | 0.00 | 0.45 |
| 660 | 0.47 | 0.00 | 0.47 |
| 664 | 0.48 | 0.01 | 0.49 |
| 668 | 0.51 | 0.01 | 0.52 |
| 672 | 0.55 | 0.01 | 0.56 |
| 676 | 0.59 | 0.01 | 0.60 |
| 680 | 0.64 | 0.01 | 0.66 |
| 684 | 0.70 | 0.01 | 0.71 |
| 688 | 0.75 | 0.02 | 0.77 |
| 692 | 0.81 | 0.02 | 0.83 |
| 696 | 0.93 | 0.03 | 0.96 |
| 700 | 1.18 | 0.05 | 1.22 |
| 704 | 1.55 | 0.07 | 1.62 |
| 708 | 2.02 | 0.10 | 2.12 |
| 712 | 2.55 | 0.13 | 2.68 |
| 716 | 3.16 | 0.18 | 3.34 |
| 720 | 4.34 | 0.36 | 4.70 |
| 724 | 6.27 | 0.54 << | 6.81 |
| 728 | 7.37 << | 0.43 | 7.79 << |
| 732 | 6.80 | 0.30 | 7.10 |
| 736 | 5.56 | 0.26 | 5.82 |
| 740 | 4.27 | 0.23 | 4.50 |
| 744 | 3.38 | 0.19 | 3.57 |
| 748 | 2.79 | 0.15 | 2.94 |
| 752 | 2.22 | 0.11 | 2.33 |
| 756 | 1.72 | 0.09 | 1.81 |
| 760 | 1.37 | 0.08 | 1.46 |
| 764 | 1.17 | 0.08 | 1.25 |
| 768 | 1.07 | 0.08 | 1.14 |
| 772 | 1.00 | 0.07 | 1.07 |
| 776 | 0.94 | 0.07 | 1.01 |
| 780 | 0.88 | 0.06 | 0.94 |
| 784 | 0.82 | 0.06 | 0.88 |
| 788 | 0.77 | 0.06 | 0.83 |
| 792 | 0.74 | 0.06 | 0.80 |

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Hydrograph Discharge Table

| Time (min) | Hyd. 2 + (cfs) | Hyd. 3 + (cfs) | Outflow (cfs) |
|-----------------------|---------------------------|---------------------------|--------------------------|
| 796 | 0.72 | 0.06 | 0.77 |
| 800 | 0.70 | 0.05 | 0.75 |
| 804 | 0.68 | 0.05 | 0.74 |
| 808 | 0.67 | 0.05 | 0.72 |
| 812 | 0.65 | 0.05 | 0.70 |
| 816 | 0.64 | 0.05 | 0.69 |
| 820 | 0.62 | 0.05 | 0.67 |
| 824 | 0.61 | 0.05 | 0.65 |
| 828 | 0.59 | 0.05 | 0.64 |
| 832 | 0.57 | 0.05 | 0.62 |
| 836 | 0.56 | 0.04 | 0.60 |
| 840 | 0.54 | 0.04 | 0.58 |
| 844 | 0.53 | 0.04 | 0.57 |
| 848 | 0.51 | 0.04 | 0.55 |
| 852 | 0.50 | 0.04 | 0.54 |
| 856 | 0.49 | 0.04 | 0.53 |
| 860 | 0.48 | 0.04 | 0.52 |
| 864 | 0.48 | 0.04 | 0.52 |
| 868 | 0.47 | 0.04 | 0.51 |
| 872 | 0.46 | 0.04 | 0.50 |
| 876 | 0.45 | 0.04 | 0.49 |
| 880 | 0.45 | 0.04 | 0.48 |
| 884 | 0.44 | 0.04 | 0.47 |
| 888 | 0.43 | 0.04 | 0.47 |
| 892 | 0.42 | 0.04 | 0.46 |
| 896 | 0.41 | 0.03 | 0.45 |
| 900 | 0.41 | 0.03 | 0.44 |
| 904 | 0.40 | 0.03 | 0.43 |
| 908 | 0.39 | 0.03 | 0.42 |
| 912 | 0.38 | 0.03 | 0.42 |
| 916 | 0.38 | 0.03 | 0.41 |
| 920 | 0.37 | 0.03 | 0.40 |
| 924 | 0.36 | 0.03 | 0.39 |

...End

Hydrograph Report

Hyd. No. 9

Basin 2 In

Hydrograph type = Combine
Storm frequency = 25 yrs
Inflow hyds. = 4, 5

Peak discharge = 8.86 cfs
Time interval = 2 min

Hydrograph Volume = 37,276 cuft

Hydrograph Discharge Table

| Time (min) | Hyd. 4 + (cfs) | Hyd. 5 + (cfs) | Outflow (cfs) |
|------------|----------------|----------------|---------------|
| 628 | 0.46 | 0.00 | 0.46 |
| 632 | 0.48 | 0.00 | 0.48 |
| 636 | 0.50 | 0.00 | 0.50 |
| 640 | 0.52 | 0.00 | 0.52 |
| 644 | 0.53 | 0.00 | 0.54 |
| 648 | 0.55 | 0.00 | 0.56 |
| 652 | 0.57 | 0.00 | 0.58 |
| 656 | 0.59 | 0.00 | 0.60 |
| 660 | 0.61 | 0.00 | 0.62 |
| 664 | 0.64 | 0.00 | 0.64 |
| 668 | 0.66 | 0.01 | 0.67 |
| 672 | 0.70 | 0.01 | 0.71 |
| 676 | 0.76 | 0.01 | 0.77 |
| 680 | 0.82 | 0.01 | 0.83 |
| 684 | 0.88 | 0.01 | 0.90 |
| 688 | 0.95 | 0.02 | 0.97 |
| 692 | 1.02 | 0.02 | 1.04 |
| 696 | 1.15 | 0.03 | 1.17 |
| 700 | 1.39 | 0.05 | 1.43 |
| 704 | 1.78 | 0.07 | 1.85 |
| 708 | 2.30 | 0.09 | 2.40 |
| 712 | 2.92 | 0.13 | 3.04 |
| 716 | 3.62 | 0.18 | 3.80 |
| 720 | 4.81 | 0.35 | 5.16 |
| 724 | 6.68 | 0.53 << | 7.20 |
| 728 | 8.26 | 0.41 | 8.67 |
| 732 | 8.38 | 0.29 | 8.67 |
| 736 | 7.39 | 0.25 | 7.64 |
| 740 | 6.07 | 0.22 | 6.29 |
| 744 | 4.71 | 0.19 | 4.89 |
| 748 | 3.72 | 0.15 | 3.87 |
| 752 | 3.01 | 0.11 | 3.12 |
| 756 | 2.38 | 0.09 | 2.47 |
| 760 | 1.88 | 0.08 | 1.96 |
| 764 | 1.55 | 0.08 | 1.63 |
| 768 | 1.35 | 0.07 | 1.43 |
| 772 | 1.24 | 0.07 | 1.31 |
| 776 | 1.16 | 0.07 | 1.23 |

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Hydrograph Discharge Table

| Time (min) | Hyd. 4 + (cfs) | Hyd. 5 + (cfs) | Outflow (cfs) |
|-----------------------|---------------------------|---------------------------|--------------------------|
| 780 | 1.09 | 0.06 | 1.15 |
| 784 | 1.02 | 0.06 | 1.08 |
| 788 | 0.96 | 0.06 | 1.01 |
| 792 | 0.91 | 0.05 | 0.96 |
| 796 | 0.87 | 0.05 | 0.93 |
| 800 | 0.85 | 0.05 | 0.90 |
| 804 | 0.83 | 0.05 | 0.88 |
| 808 | 0.81 | 0.05 | 0.86 |
| 812 | 0.79 | 0.05 | 0.84 |
| 816 | 0.77 | 0.05 | 0.82 |
| 820 | 0.75 | 0.05 | 0.80 |
| 824 | 0.73 | 0.05 | 0.78 |
| 828 | 0.71 | 0.05 | 0.76 |
| 832 | 0.69 | 0.04 | 0.74 |
| 836 | 0.67 | 0.04 | 0.72 |
| 840 | 0.65 | 0.04 | 0.70 |
| 844 | 0.63 | 0.04 | 0.68 |
| 848 | 0.62 | 0.04 | 0.66 |
| 852 | 0.60 | 0.04 | 0.64 |
| 856 | 0.59 | 0.04 | 0.63 |
| 860 | 0.58 | 0.04 | 0.62 |
| 864 | 0.57 | 0.04 | 0.61 |
| 868 | 0.56 | 0.04 | 0.60 |
| 872 | 0.55 | 0.04 | 0.59 |
| 876 | 0.54 | 0.04 | 0.58 |
| 880 | 0.53 | 0.04 | 0.57 |
| 884 | 0.52 | 0.04 | 0.56 |
| 888 | 0.52 | 0.03 | 0.55 |
| 892 | 0.51 | 0.03 | 0.54 |
| 896 | 0.50 | 0.03 | 0.53 |
| 900 | 0.49 | 0.03 | 0.52 |
| 904 | 0.48 | 0.03 | 0.51 |
| 908 | 0.47 | 0.03 | 0.50 |
| 912 | 0.46 | 0.03 | 0.49 |
| 916 | 0.45 | 0.03 | 0.48 |
| 920 | 0.44 | 0.03 | 0.47 |
| 924 | 0.43 | 0.03 | 0.46 |
| 928 | 0.42 | 0.03 | 0.45 |

...End

Hydrograph Report

Hyd. No. 10

Basin 3 In

Hydrograph type = Combine
Storm frequency = 25 yrs
Inflow hyds. = 6, 7

Peak discharge = 13.90 cfs
Time interval = 2 min

Hydrograph Volume = 48,122 cuft

Hydrograph Discharge Table

| Time (min) | Hyd. 6 + (cfs) | Hyd. 7 + (cfs) | Outflow (cfs) |
|------------|----------------|----------------|---------------|
| 652 | 0.71 | 0.00 | 0.72 |
| 656 | 0.74 | 0.00 | 0.74 |
| 660 | 0.77 | 0.00 | 0.77 |
| 664 | 0.80 | 0.01 | 0.81 |
| 668 | 0.85 | 0.01 | 0.86 |
| 672 | 0.92 | 0.01 | 0.93 |
| 676 | 1.01 | 0.01 | 1.02 |
| 680 | 1.09 | 0.02 | 1.11 |
| 684 | 1.18 | 0.02 | 1.20 |
| 688 | 1.27 | 0.02 | 1.29 |
| 692 | 1.37 | 0.03 | 1.40 |
| 696 | 1.65 | 0.04 | 1.68 |
| 700 | 2.21 | 0.06 | 2.26 |
| 704 | 2.96 | 0.09 | 3.05 |
| 708 | 3.80 | 0.12 | 3.92 |
| 712 | 4.69 | 0.16 | 4.85 |
| 716 | 5.75 | 0.23 | 5.98 |
| 720 | 8.47 | 0.45 | 8.91 |
| 724 | 12.50 | 0.68 << | 13.18 |
| 728 | 12.71 | 0.53 | 13.25 |
| 732 | 9.66 | 0.37 | 10.03 |
| 736 | 6.98 | 0.33 | 7.30 |
| 740 | 5.69 | 0.29 | 5.97 |
| 744 | 4.79 | 0.24 | 5.03 |
| 748 | 3.87 | 0.19 | 4.06 |
| 752 | 2.96 | 0.14 | 3.10 |
| 756 | 2.25 | 0.11 | 2.36 |
| 760 | 1.89 | 0.11 | 2.00 |
| 764 | 1.74 | 0.10 | 1.84 |
| 768 | 1.64 | 0.10 | 1.74 |
| 772 | 1.55 | 0.09 | 1.64 |
| 776 | 1.45 | 0.08 | 1.53 |
| 780 | 1.35 | 0.08 | 1.43 |
| 784 | 1.26 | 0.07 | 1.33 |
| 788 | 1.20 | 0.07 | 1.27 |
| 792 | 1.16 | 0.07 | 1.23 |
| 796 | 1.13 | 0.07 | 1.20 |
| 800 | 1.11 | 0.07 | 1.18 |

Continues on next page...

Hydrograph Discharge Table

| Time (min) | Hyd. 6 + (cfs) | Hyd. 7 + (cfs) | Outflow (cfs) |
|-----------------------|---------------------------|---------------------------|--------------------------|
| 804 | 1.08 | 0.07 | 1.15 |
| 808 | 1.06 | 0.07 | 1.12 |
| 812 | 1.03 | 0.06 | 1.10 |
| 816 | 1.01 | 0.06 | 1.07 |
| 820 | 0.98 | 0.06 | 1.04 |
| 824 | 0.96 | 0.06 | 1.02 |
| 828 | 0.93 | 0.06 | 0.99 |
| 832 | 0.90 | 0.06 | 0.96 |
| 836 | 0.88 | 0.06 | 0.93 |
| 840 | 0.85 | 0.05 | 0.91 |
| 844 | 0.83 | 0.05 | 0.88 |
| 848 | 0.81 | 0.05 | 0.86 |
| 852 | 0.79 | 0.05 | 0.85 |
| 856 | 0.78 | 0.05 | 0.83 |
| 860 | 0.77 | 0.05 | 0.82 |
| 864 | 0.76 | 0.05 | 0.81 |
| 868 | 0.74 | 0.05 | 0.79 |
| 872 | 0.73 | 0.05 | 0.78 |
| 876 | 0.72 | 0.05 | 0.77 |
| 880 | 0.71 | 0.05 | 0.75 |
| 884 | 0.70 | 0.05 | 0.74 |
| 888 | 0.68 | 0.04 | 0.73 |
| 892 | 0.67 | 0.04 | 0.71 |
| 896 | 0.66 | 0.04 | 0.70 |

...End

Hydrograph Report

Hyd. No. 11

Basin 1 Out

Hydrograph type = Reservoir
 Storm frequency = 25 yrs
 Inflow hyd. No. = 8
 Max. Elevation = 242.87 ft

Peak discharge = 0.39 cfs
 Time interval = 2 min
 Reservoir name = Retention Basin N
 Max. Storage = 30,290 cuft

Storage Indication method used.

Outflow hydrograph volume = 29,889 cuft

Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 520 | 0.12 | 240.06 | 23.09 | 0.02 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.02 |
| 524 | 0.12 | 240.07 | 23.09 | 0.02 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.02 |
| 528 | 0.13 | 240.07 | 23.09 | 0.02 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.02 |
| 532 | 0.13 | 240.07 | 23.09 | 0.02 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.02 |
| 536 | 0.14 | 240.08 | 23.09 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.03 |
| 540 | 0.15 | 240.08 | 23.09 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.03 |
| 544 | 0.15 | 240.09 | 23.09 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.03 |
| 548 | 0.16 | 240.09 | 23.09 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.03 |
| 552 | 0.17 | 240.10 | 23.09 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.03 |
| 556 | 0.17 | 240.10 | 23.09 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.03 |
| 560 | 0.18 | 240.11 | 23.09 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.03 |
| 564 | 0.19 | 240.11 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 568 | 0.19 | 240.12 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 572 | 0.20 | 240.12 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 576 | 0.21 | 240.13 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 580 | 0.22 | 240.13 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 584 | 0.22 | 240.14 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 588 | 0.23 | 240.15 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 592 | 0.24 | 240.15 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 596 | 0.25 | 240.16 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 600 | 0.26 | 240.17 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 604 | 0.26 | 240.18 | 23.09 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |
| 608 | 0.27 | 240.18 | 23.09 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |
| 612 | 0.29 | 240.19 | 23.09 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |
| 616 | 0.30 | 240.20 | 23.09 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |
| 620 | 0.31 | 240.21 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 624 | 0.33 | 240.22 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 628 | 0.34 | 240.23 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 632 | 0.36 | 240.24 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 636 | 0.37 | 240.25 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 640 | 0.39 | 240.26 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 644 | 0.40 | 240.27 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 648 | 0.42 | 240.28 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 652 | 0.44 | 240.29 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 656 | 0.45 | 240.30 | 23.09 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 660 | 0.47 | 240.32 | 23.09 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 664 | 0.49 | 240.33 | 23.09 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 668 | 0.52 | 240.34 | 23.09 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.11 |

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Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 672 | 0.56 | 240.36 | 23.09 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.11 |
| 676 | 0.60 | 240.38 | 23.09 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.12 |
| 680 | 0.66 | 240.40 | 23.09 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.12 |
| 684 | 0.71 | 240.42 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 688 | 0.77 | 240.44 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 692 | 0.83 | 240.46 | 23.09 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 696 | 0.96 | 240.49 | 23.09 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 700 | 1.22 | 240.52 | 23.09 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 704 | 1.62 | 240.57 | 23.09 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |
| 708 | 2.12 | 240.63 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 712 | 2.68 | 240.71 | 23.09 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 716 | 3.34 | 240.81 | 23.09 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 720 | 4.70 | 240.94 | 23.09 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 724 | 6.81 | 241.14 | 23.09 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 728 | 7.79 << | 241.40 | 23.09 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 732 | 7.10 | 241.66 | 23.09 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 736 | 5.82 | 241.88 | 23.09 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 740 | 4.50 | 242.06 | 23.09 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 744 | 3.57 | 242.19 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 748 | 2.94 | 242.29 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 752 | 2.33 | 242.37 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 756 | 1.81 | 242.44 | 23.09 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 760 | 1.46 | 242.48 | 23.09 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 764 | 1.25 | 242.52 | 23.09 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 768 | 1.14 | 242.55 | 23.09 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 772 | 1.07 | 242.57 | 23.09 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 776 | 1.01 | 242.60 | 23.09 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 780 | 0.94 | 242.62 | 23.09 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 784 | 0.88 | 242.64 | 23.09 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 788 | 0.83 | 242.65 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 792 | 0.80 | 242.67 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 796 | 0.77 | 242.68 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 800 | 0.75 | 242.70 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 804 | 0.74 | 242.71 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 808 | 0.72 | 242.72 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 812 | 0.70 | 242.74 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 816 | 0.69 | 242.75 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 820 | 0.67 | 242.76 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 824 | 0.65 | 242.77 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 828 | 0.64 | 242.78 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 832 | 0.62 | 242.79 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 836 | 0.60 | 242.79 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 840 | 0.58 | 242.80 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 844 | 0.57 | 242.81 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 848 | 0.55 | 242.81 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 852 | 0.54 | 242.82 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 856 | 0.53 | 242.83 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 860 | 0.52 | 242.83 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 864 | 0.52 | 242.84 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 868 | 0.51 | 242.84 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 872 | 0.50 | 242.84 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |

Continues on next page...

Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 876 | 0.49 | 242.85 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 880 | 0.48 | 242.85 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 884 | 0.47 | 242.85 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 888 | 0.47 | 242.86 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 892 | 0.46 | 242.86 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 896 | 0.45 | 242.86 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 900 | 0.44 | 242.86 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 904 | 0.43 | 242.87 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 908 | 0.42 | 242.87 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 912 | 0.42 | 242.87 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 916 | 0.41 | 242.87 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 920 | 0.40 | 242.87 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 924 | 0.39 | 242.87 << | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 << |
| 928 | 0.38 | 242.87 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 932 | 0.37 | 242.87 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 936 | 0.36 | 242.87 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 940 | 0.36 | 242.87 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 944 | 0.35 | 242.86 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 948 | 0.34 | 242.86 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 952 | 0.33 | 242.86 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 956 | 0.32 | 242.86 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 960 | 0.31 | 242.86 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 964 | 0.30 | 242.85 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 968 | 0.30 | 242.85 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 972 | 0.29 | 242.85 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 976 | 0.29 | 242.84 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 980 | 0.28 | 242.84 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 984 | 0.28 | 242.84 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 988 | 0.28 | 242.83 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 992 | 0.27 | 242.83 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 996 | 0.27 | 242.82 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1000 | 0.27 | 242.82 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1004 | 0.26 | 242.81 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1008 | 0.26 | 242.81 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1012 | 0.25 | 242.81 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1016 | 0.25 | 242.80 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1020 | 0.25 | 242.80 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1024 | 0.24 | 242.79 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1028 | 0.24 | 242.79 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1032 | 0.24 | 242.78 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1036 | 0.23 | 242.77 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1040 | 0.23 | 242.77 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1044 | 0.22 | 242.76 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1048 | 0.22 | 242.76 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1052 | 0.22 | 242.75 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1056 | 0.21 | 242.75 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1060 | 0.21 | 242.74 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1064 | 0.21 | 242.73 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1068 | 0.20 | 242.73 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1072 | 0.20 | 242.72 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1076 | 0.19 | 242.71 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |

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Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 1080 | 0.19 | 242.71 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1084 | 0.19 | 242.70 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1088 | 0.18 | 242.69 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1092 | 0.18 | 242.69 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1096 | 0.18 | 242.68 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1100 | 0.18 | 242.67 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1104 | 0.18 | 242.66 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1108 | 0.18 | 242.66 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1112 | 0.18 | 242.65 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1116 | 0.18 | 242.64 | 23.09 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1120 | 0.17 | 242.64 | 23.09 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1124 | 0.17 | 242.63 | 23.09 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1128 | 0.17 | 242.62 | 23.09 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1132 | 0.17 | 242.61 | 23.09 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1136 | 0.17 | 242.61 | 23.09 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1140 | 0.17 | 242.60 | 23.09 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1144 | 0.17 | 242.59 | 23.09 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1148 | 0.17 | 242.59 | 23.09 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1152 | 0.17 | 242.58 | 23.09 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1156 | 0.16 | 242.57 | 23.09 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1160 | 0.16 | 242.56 | 23.09 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1164 | 0.16 | 242.56 | 23.09 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1168 | 0.16 | 242.55 | 23.09 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1172 | 0.16 | 242.54 | 23.09 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1176 | 0.16 | 242.53 | 23.09 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1180 | 0.16 | 242.53 | 23.09 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1184 | 0.16 | 242.52 | 23.09 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1188 | 0.15 | 242.51 | 23.09 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1192 | 0.15 | 242.50 | 23.09 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1196 | 0.15 | 242.50 | 23.09 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1200 | 0.15 | 242.49 | 23.09 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1204 | 0.15 | 242.48 | 23.09 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1208 | 0.15 | 242.47 | 23.09 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1212 | 0.15 | 242.47 | 23.09 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1216 | 0.15 | 242.46 | 23.09 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1220 | 0.15 | 242.45 | 23.09 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1224 | 0.14 | 242.44 | 23.09 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1228 | 0.14 | 242.43 | 23.09 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1232 | 0.14 | 242.43 | 23.09 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1236 | 0.14 | 242.42 | 23.09 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1240 | 0.14 | 242.41 | 23.09 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1244 | 0.14 | 242.40 | 23.09 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1248 | 0.14 | 242.40 | 23.09 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1252 | 0.14 | 242.39 | 23.09 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1256 | 0.14 | 242.38 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1260 | 0.13 | 242.37 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1264 | 0.13 | 242.36 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1268 | 0.13 | 242.36 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1272 | 0.13 | 242.35 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1276 | 0.13 | 242.34 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1280 | 0.13 | 242.33 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |

Continues on next page...

Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 1284 | 0.13 | 242.32 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1288 | 0.13 | 242.32 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1292 | 0.13 | 242.31 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1296 | 0.12 | 242.30 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1300 | 0.12 | 242.29 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1304 | 0.12 | 242.28 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1308 | 0.12 | 242.28 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1312 | 0.12 | 242.27 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1316 | 0.12 | 242.26 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1320 | 0.12 | 242.25 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1324 | 0.15 | 242.24 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1328 | 0.17 | 242.24 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1332 | 0.15 | 242.23 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1336 | 0.14 | 242.22 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1340 | 0.13 | 242.22 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1344 | 0.12 | 242.21 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1348 | 0.12 | 242.20 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1352 | 0.12 | 242.19 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1356 | 0.12 | 242.18 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1360 | 0.12 | 242.18 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1364 | 0.12 | 242.17 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1368 | 0.12 | 242.16 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1372 | 0.11 | 242.15 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1376 | 0.11 | 242.14 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1380 | 0.11 | 242.14 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1384 | 0.11 | 242.13 | 23.09 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1388 | 0.11 | 242.12 | 23.09 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1392 | 0.11 | 242.11 | 23.09 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1396 | 0.11 | 242.10 | 23.09 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1400 | 0.11 | 242.10 | 23.09 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1404 | 0.11 | 242.09 | 23.09 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1408 | 0.11 | 242.08 | 23.09 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1412 | 0.11 | 242.07 | 23.09 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1416 | 0.11 | 242.06 | 23.09 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1420 | 0.10 | 242.06 | 23.09 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1424 | 0.10 | 242.05 | 23.09 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1428 | 0.10 | 242.04 | 23.09 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1432 | 0.10 | 242.03 | 23.09 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1436 | 0.10 | 242.02 | 23.09 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1440 | 0.10 | 242.02 | 23.09 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1444 | 0.08 | 242.01 | 23.09 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1448 | 0.05 | 242.00 | 23.09 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1452 | 0.02 | 241.99 | 23.09 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1456 | 0.01 | 241.98 | 23.09 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1460 | 0.00 | 241.97 | 23.09 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1464 | 0.00 | 241.95 | 23.09 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1468 | 0.00 | 241.94 | 23.09 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1472 | 0.00 | 241.93 | 23.09 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1476 | 0.00 | 241.92 | 23.09 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1480 | 0.00 | 241.91 | 23.09 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1484 | 0.00 | 241.90 | 23.09 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |

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Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 1488 | 0.00 | 241.89 | 23.09 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1492 | 0.00 | 241.87 | 23.09 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1496 | 0.00 | 241.86 | 23.09 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1500 | 0.00 | 241.85 | 23.09 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1504 | 0.00 | 241.84 | 23.09 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1508 | 0.00 | 241.83 | 23.09 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1512 | 0.00 | 241.82 | 23.09 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1516 | 0.00 | 241.81 | 23.09 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1520 | 0.00 | 241.80 | 23.09 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1524 | 0.00 | 241.79 | 23.09 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1528 | 0.00 | 241.78 | 23.09 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1532 | 0.00 | 241.76 | 23.09 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1536 | 0.00 | 241.75 | 23.09 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1540 | 0.00 | 241.74 | 23.09 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1544 | 0.00 | 241.73 | 23.09 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1548 | 0.00 | 241.72 | 23.09 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1552 | 0.00 | 241.71 | 23.09 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1556 | 0.00 | 241.70 | 23.09 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1560 | 0.00 | 241.69 | 23.09 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1564 | 0.00 | 241.68 | 23.09 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1568 | 0.00 | 241.67 | 23.09 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1572 | 0.00 | 241.66 | 23.09 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1576 | 0.00 | 241.65 | 23.09 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1580 | 0.00 | 241.64 | 23.09 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1584 | 0.00 | 241.63 | 23.09 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1588 | 0.00 | 241.62 | 23.09 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1592 | 0.00 | 241.61 | 23.09 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1596 | 0.00 | 241.59 | 23.09 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1600 | 0.00 | 241.58 | 23.09 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1604 | 0.00 | 241.57 | 23.09 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 1608 | 0.00 | 241.56 | 23.09 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 1612 | 0.00 | 241.55 | 23.09 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 1616 | 0.00 | 241.54 | 23.09 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 1620 | 0.00 | 241.53 | 23.09 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 1624 | 0.00 | 241.52 | 23.09 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 1628 | 0.00 | 241.51 | 23.09 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 1632 | 0.00 | 241.50 | 23.09 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 1636 | 0.00 | 241.49 | 23.09 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 1640 | 0.00 | 241.48 | 23.09 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 1644 | 0.00 | 241.47 | 23.09 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 1648 | 0.00 | 241.46 | 23.09 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 1652 | 0.00 | 241.45 | 23.09 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 1656 | 0.00 | 241.44 | 23.09 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 1660 | 0.00 | 241.43 | 23.09 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 1664 | 0.00 | 241.43 | 23.09 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 1668 | 0.00 | 241.42 | 23.09 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 1672 | 0.00 | 241.41 | 23.09 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 1676 | 0.00 | 241.40 | 23.09 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 1680 | 0.00 | 241.39 | 23.09 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 1684 | 0.00 | 241.38 | 23.09 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 1688 | 0.00 | 241.37 | 23.09 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |

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Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 1692 | 0.00 | 241.36 | 23.09 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 1696 | 0.00 | 241.35 | 23.09 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 1700 | 0.00 | 241.34 | 23.09 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 1704 | 0.00 | 241.33 | 23.09 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 1708 | 0.00 | 241.32 | 23.09 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 1712 | 0.00 | 241.31 | 23.09 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 1716 | 0.00 | 241.30 | 23.09 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 1720 | 0.00 | 241.29 | 23.09 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 1724 | 0.00 | 241.28 | 23.09 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 1728 | 0.00 | 241.27 | 23.09 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 1732 | 0.00 | 241.27 | 23.09 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 1736 | 0.00 | 241.26 | 23.09 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 1740 | 0.00 | 241.25 | 23.09 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 1744 | 0.00 | 241.24 | 23.09 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 1748 | 0.00 | 241.23 | 23.09 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 1752 | 0.00 | 241.22 | 23.09 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 1756 | 0.00 | 241.21 | 23.09 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 1760 | 0.00 | 241.20 | 23.09 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 1764 | 0.00 | 241.19 | 23.09 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 1768 | 0.00 | 241.19 | 23.09 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 1772 | 0.00 | 241.18 | 23.09 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 1776 | 0.00 | 241.17 | 23.09 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 1780 | 0.00 | 241.16 | 23.09 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 1784 | 0.00 | 241.15 | 23.09 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 1788 | 0.00 | 241.14 | 23.09 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 1792 | 0.00 | 241.13 | 23.09 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 1796 | 0.00 | 241.13 | 23.09 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 1800 | 0.00 | 241.12 | 23.09 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 1804 | 0.00 | 241.11 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 1808 | 0.00 | 241.10 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 1812 | 0.00 | 241.09 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 1816 | 0.00 | 241.08 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 1820 | 0.00 | 241.08 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 1824 | 0.00 | 241.07 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 1828 | 0.00 | 241.06 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 1832 | 0.00 | 241.05 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 1836 | 0.00 | 241.04 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 1840 | 0.00 | 241.03 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 1844 | 0.00 | 241.03 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 1848 | 0.00 | 241.02 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 1852 | 0.00 | 241.01 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 1856 | 0.00 | 241.00 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 1860 | 0.00 | 240.99 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 1864 | 0.00 | 240.99 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 1868 | 0.00 | 240.98 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 1872 | 0.00 | 240.97 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 1876 | 0.00 | 240.96 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 1880 | 0.00 | 240.96 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 1884 | 0.00 | 240.95 | 23.09 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 1888 | 0.00 | 240.94 | 23.09 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 1892 | 0.00 | 240.93 | 23.09 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |

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Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 1896 | 0.00 | 240.92 | 23.09 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 1900 | 0.00 | 240.92 | 23.09 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 1904 | 0.00 | 240.91 | 23.09 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 1908 | 0.00 | 240.90 | 23.09 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 1912 | 0.00 | 240.89 | 23.09 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 1916 | 0.00 | 240.89 | 23.09 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 1920 | 0.00 | 240.88 | 23.09 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 1924 | 0.00 | 240.87 | 23.09 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 1928 | 0.00 | 240.87 | 23.09 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 1932 | 0.00 | 240.86 | 23.09 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 1936 | 0.00 | 240.85 | 23.09 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 1940 | 0.00 | 240.84 | 23.09 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 1944 | 0.00 | 240.84 | 23.09 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 1948 | 0.00 | 240.83 | 23.09 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 1952 | 0.00 | 240.82 | 23.09 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 1956 | 0.00 | 240.81 | 23.09 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 1960 | 0.00 | 240.81 | 23.09 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 1964 | 0.00 | 240.80 | 23.09 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 1968 | 0.00 | 240.79 | 23.09 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 1972 | 0.00 | 240.79 | 23.09 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 1976 | 0.00 | 240.78 | 23.09 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 1980 | 0.00 | 240.77 | 23.09 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 1984 | 0.00 | 240.77 | 23.09 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 1988 | 0.00 | 240.76 | 23.09 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 1992 | 0.00 | 240.75 | 23.09 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 1996 | 0.00 | 240.75 | 23.09 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 2000 | 0.00 | 240.74 | 23.09 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 2004 | 0.00 | 240.73 | 23.09 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 2008 | 0.00 | 240.73 | 23.09 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 2012 | 0.00 | 240.72 | 23.09 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 2016 | 0.00 | 240.71 | 23.09 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 2020 | 0.00 | 240.71 | 23.09 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 2024 | 0.00 | 240.70 | 23.09 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 2028 | 0.00 | 240.69 | 23.09 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 2032 | 0.00 | 240.69 | 23.09 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 2036 | 0.00 | 240.68 | 23.09 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 2040 | 0.00 | 240.68 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 2044 | 0.00 | 240.67 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 2048 | 0.00 | 240.66 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 2052 | 0.00 | 240.66 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 2056 | 0.00 | 240.65 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 2060 | 0.00 | 240.64 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 2064 | 0.00 | 240.64 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 2068 | 0.00 | 240.63 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 2072 | 0.00 | 240.63 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 2076 | 0.00 | 240.62 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 2080 | 0.00 | 240.61 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 2084 | 0.00 | 240.61 | 23.09 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |
| 2088 | 0.00 | 240.60 | 23.09 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |
| 2092 | 0.00 | 240.60 | 23.09 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |
| 2096 | 0.00 | 240.59 | 23.09 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |

Continues on next page...

Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Civ A cfs | Civ B cfs | Civ C cfs | Civ D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 2100 | 0.00 | 240.58 | 23.09 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |
| 2104 | 0.00 | 240.58 | 23.09 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |
| 2108 | 0.00 | 240.57 | 23.09 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |
| 2112 | 0.00 | 240.57 | 23.09 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |
| 2116 | 0.00 | 240.56 | 23.09 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |
| 2120 | 0.00 | 240.56 | 23.09 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 2124 | 0.00 | 240.55 | 23.09 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 2128 | 0.00 | 240.55 | 23.09 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 2132 | 0.00 | 240.54 | 23.09 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 2136 | 0.00 | 240.53 | 23.09 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 2140 | 0.00 | 240.53 | 23.09 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 2144 | 0.00 | 240.52 | 23.09 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 2148 | 0.00 | 240.52 | 23.09 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 2152 | 0.00 | 240.51 | 23.09 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 2156 | 0.00 | 240.51 | 23.09 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 2160 | 0.00 | 240.50 | 23.09 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 2164 | 0.00 | 240.50 | 23.09 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 2168 | 0.00 | 240.49 | 23.09 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 2172 | 0.00 | 240.49 | 23.09 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 2176 | 0.00 | 240.48 | 23.09 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 2180 | 0.00 | 240.48 | 23.09 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 2184 | 0.00 | 240.47 | 23.09 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 2188 | 0.00 | 240.47 | 23.09 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 2192 | 0.00 | 240.46 | 23.09 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 2196 | 0.00 | 240.46 | 23.09 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 2200 | 0.00 | 240.45 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 2204 | 0.00 | 240.45 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 2208 | 0.00 | 240.44 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 2212 | 0.00 | 240.44 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 2216 | 0.00 | 240.43 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 2220 | 0.00 | 240.43 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 2224 | 0.00 | 240.42 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 2228 | 0.00 | 240.42 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 2232 | 0.00 | 240.42 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 2236 | 0.00 | 240.41 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 2240 | 0.00 | 240.41 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 2244 | 0.00 | 240.40 | 23.09 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.12 |
| 2248 | 0.00 | 240.40 | 23.09 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.12 |
| 2252 | 0.00 | 240.39 | 23.09 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.12 |
| 2256 | 0.00 | 240.39 | 23.09 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.12 |
| 2260 | 0.00 | 240.38 | 23.09 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.12 |
| 2264 | 0.00 | 240.38 | 23.09 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.12 |
| 2268 | 0.00 | 240.38 | 23.09 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.12 |
| 2272 | 0.00 | 240.37 | 23.09 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.12 |
| 2276 | 0.00 | 240.37 | 23.09 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.11 |
| 2280 | 0.00 | 240.36 | 23.09 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.11 |
| 2284 | 0.00 | 240.36 | 23.09 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.11 |
| 2288 | 0.00 | 240.36 | 23.09 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.11 |
| 2292 | 0.00 | 240.35 | 23.09 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.11 |
| 2296 | 0.00 | 240.35 | 23.09 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.11 |
| 2300 | 0.00 | 240.34 | 23.09 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.11 |

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Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 2304 | 0.00 | 240.34 | 23.09 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.11 |
| 2308 | 0.00 | 240.34 | 23.09 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.11 |
| 2312 | 0.00 | 240.33 | 23.09 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 2316 | 0.00 | 240.33 | 23.09 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 2320 | 0.00 | 240.33 | 23.09 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 2324 | 0.00 | 240.32 | 23.09 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 2328 | 0.00 | 240.32 | 23.09 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 2332 | 0.00 | 240.31 | 23.09 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 2336 | 0.00 | 240.31 | 23.09 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 2340 | 0.00 | 240.31 | 23.09 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 2344 | 0.00 | 240.30 | 23.09 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 2348 | 0.00 | 240.30 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 2352 | 0.00 | 240.30 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 2356 | 0.00 | 240.29 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 2360 | 0.00 | 240.29 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 2364 | 0.00 | 240.29 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 2368 | 0.00 | 240.28 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 2372 | 0.00 | 240.28 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 2376 | 0.00 | 240.28 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 2380 | 0.00 | 240.27 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 2384 | 0.00 | 240.27 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 2388 | 0.00 | 240.27 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 2392 | 0.00 | 240.27 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 2396 | 0.00 | 240.26 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 2400 | 0.00 | 240.26 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 2404 | 0.00 | 240.26 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 2408 | 0.00 | 240.25 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 2412 | 0.00 | 240.25 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 2416 | 0.00 | 240.25 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 2420 | 0.00 | 240.24 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 2424 | 0.00 | 240.24 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 2428 | 0.00 | 240.24 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 2432 | 0.00 | 240.24 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 2436 | 0.00 | 240.23 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 2440 | 0.00 | 240.23 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 2444 | 0.00 | 240.23 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 2448 | 0.00 | 240.23 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 2452 | 0.00 | 240.22 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 2456 | 0.00 | 240.22 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 2460 | 0.00 | 240.22 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 2464 | 0.00 | 240.22 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 2468 | 0.00 | 240.21 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 2472 | 0.00 | 240.21 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 2476 | 0.00 | 240.21 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 2480 | 0.00 | 240.21 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 2484 | 0.00 | 240.20 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 2488 | 0.00 | 240.20 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 2492 | 0.00 | 240.20 | 23.09 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |
| 2496 | 0.00 | 240.20 | 23.09 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |
| 2500 | 0.00 | 240.19 | 23.09 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |
| 2504 | 0.00 | 240.19 | 23.09 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |

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Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 2508 | 0.00 | 240.19 | 23.09 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |
| 2512 | 0.00 | 240.19 | 23.09 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |
| 2516 | 0.00 | 240.19 | 23.09 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |
| 2520 | 0.00 | 240.18 | 23.09 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |
| 2524 | 0.00 | 240.18 | 23.09 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |
| 2528 | 0.00 | 240.18 | 23.09 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |
| 2532 | 0.00 | 240.18 | 23.09 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |
| 2536 | 0.00 | 240.17 | 23.09 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |
| 2540 | 0.00 | 240.17 | 23.09 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |
| 2544 | 0.00 | 240.17 | 23.09 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |
| 2548 | 0.00 | 240.17 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 2552 | 0.00 | 240.17 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 2556 | 0.00 | 240.17 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 2560 | 0.00 | 240.16 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 2564 | 0.00 | 240.16 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 2568 | 0.00 | 240.16 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 2572 | 0.00 | 240.16 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 2576 | 0.00 | 240.16 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 2580 | 0.00 | 240.15 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 2584 | 0.00 | 240.15 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 2588 | 0.00 | 240.15 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 2592 | 0.00 | 240.15 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 2596 | 0.00 | 240.15 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 2600 | 0.00 | 240.15 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 2604 | 0.00 | 240.14 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 2608 | 0.00 | 240.14 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 2612 | 0.00 | 240.14 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 2616 | 0.00 | 240.14 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 2620 | 0.00 | 240.14 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 2624 | 0.00 | 240.14 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 2628 | 0.00 | 240.13 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 2632 | 0.00 | 240.13 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 2636 | 0.00 | 240.13 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 2640 | 0.00 | 240.13 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 2644 | 0.00 | 240.13 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 2648 | 0.00 | 240.13 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 2652 | 0.00 | 240.12 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 2656 | 0.00 | 240.12 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 2660 | 0.00 | 240.12 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 2664 | 0.00 | 240.12 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 2668 | 0.00 | 240.12 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 2672 | 0.00 | 240.12 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 2676 | 0.00 | 240.12 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 2680 | 0.00 | 240.12 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 2684 | 0.00 | 240.11 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 2688 | 0.00 | 240.11 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 2692 | 0.00 | 240.11 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 2696 | 0.00 | 240.11 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 2700 | 0.00 | 240.11 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 2704 | 0.00 | 240.11 | 23.09 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.03 |
| 2708 | 0.00 | 240.11 | 23.09 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.03 |

Continues on next page...

Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 2712 | 0.00 | 240.10 | 23.09 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.03 |
| 2716 | 0.00 | 240.10 | 23.09 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.03 |
| 2720 | 0.00 | 240.10 | 23.09 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.03 |
| 2724 | 0.00 | 240.10 | 23.09 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.03 |
| 2728 | 0.00 | 240.10 | 23.09 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.03 |
| 2732 | 0.00 | 240.10 | 23.09 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.03 |
| 2736 | 0.00 | 240.10 | 23.09 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.03 |
| 2740 | 0.00 | 240.10 | 23.09 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.03 |
| 2744 | 0.00 | 240.10 | 23.09 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.03 |
| 2748 | 0.00 | 240.09 | 23.09 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.03 |
| 2752 | 0.00 | 240.09 | 23.09 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.03 |
| 2756 | 0.00 | 240.09 | 23.09 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.03 |
| 2760 | 0.00 | 240.09 | 23.09 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.03 |
| 2764 | 0.00 | 240.09 | 23.09 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.03 |
| 2768 | 0.00 | 240.09 | 23.09 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.03 |
| 2772 | 0.00 | 240.09 | 23.09 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.03 |
| 2776 | 0.00 | 240.09 | 23.09 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.03 |
| 2780 | 0.00 | 240.09 | 23.09 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.03 |
| 2784 | 0.00 | 240.08 | 23.09 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.03 |
| 2788 | 0.00 | 240.08 | 23.09 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.03 |
| 2792 | 0.00 | 240.08 | 23.09 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.03 |
| 2796 | 0.00 | 240.08 | 23.09 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.03 |
| 2800 | 0.00 | 240.08 | 23.09 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.03 |
| 2804 | 0.00 | 240.08 | 23.09 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.03 |
| 2808 | 0.00 | 240.08 | 23.09 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.03 |
| 2812 | 0.00 | 240.08 | 23.09 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.03 |
| 2816 | 0.00 | 240.08 | 23.09 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.03 |
| 2820 | 0.00 | 240.08 | 23.09 | 0.02 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.02 |
| 2824 | 0.00 | 240.08 | 23.09 | 0.02 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.02 |
| 2828 | 0.00 | 240.07 | 23.09 | 0.02 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.02 |
| 2832 | 0.00 | 240.07 | 23.09 | 0.02 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.02 |
| 2836 | 0.00 | 240.07 | 23.09 | 0.02 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.02 |
| 2840 | 0.00 | 240.07 | 23.09 | 0.02 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.02 |
| 2844 | 0.00 | 240.07 | 23.09 | 0.02 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.02 |
| 2848 | 0.00 | 240.07 | 23.09 | 0.02 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.02 |
| 2852 | 0.00 | 240.07 | 23.09 | 0.02 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.02 |
| 2856 | 0.00 | 240.07 | 23.09 | 0.02 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.02 |
| 2860 | 0.00 | 240.07 | 23.09 | 0.02 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.02 |
| 2864 | 0.00 | 240.07 | 23.09 | 0.02 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.02 |
| 2868 | 0.00 | 240.07 | 23.09 | 0.02 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.02 |
| 2872 | 0.00 | 240.07 | 23.09 | 0.02 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.02 |
| 2876 | 0.00 | 240.07 | 23.09 | 0.02 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.02 |
| 2880 | 0.00 | 240.06 | 23.09 | 0.02 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.02 |

...End

Reservoir Report

Reservoir No. 1 - Retention Basin No. 1

Hydraflow Hydrographs by Intelisolve

Pond Data

Pond storage is based on known contour areas. Average end area method used.

Stage / Storage Table

| Stage (ft) | Elevation (ft) | Contour area (sqft) | Incr. Storage (cuft) | Total storage (cuft) |
|------------|----------------|---------------------|----------------------|----------------------|
| 0.00 | 238.00 | 4,449 | 0 | 0 |
| 2.00 | 240.00 | 6,679 | 11,128 | 11,128 |
| 4.00 | 242.00 | 6,679 | 13,358 | 24,486 |
| 6.00 | 244.00 | 6,679 | 13,358 | 37,844 |
| 8.00 | 246.00 | 6,679 | 13,358 | 51,202 |
| 8.50 | 246.50 | 6,679 | 3,340 | 54,542 |

Culvert / Orifice Structures

| | [A] | [B] | [C] | [D] |
|---------------|----------|--------|------|------|
| Rise in | = 6.0 | 3.0 | 0.0 | 0.0 |
| Span in | = 6.0 | 3.0 | 0.0 | 0.0 |
| No. Barrels | = 10 | 1 | 0 | 0 |
| Invert El. ft | = 227.00 | 240.00 | 0.00 | 0.00 |
| Length ft | = 68.0 | 1.0 | 0.0 | 0.0 |
| Slope % | = 6.03 | 0.00 | 0.00 | 0.00 |
| N-Value | = .013 | .013 | .000 | .000 |
| Orif. Coeff. | = 0.60 | 0.60 | 0.00 | 0.00 |
| Multi-Stage | = n/a | Yes | No | No |

Weir Structures

| | [A] | [B] | [C] | [D] |
|--------------|----------|--------|--------|------|
| Crest Len ft | = 1.00 | 40.00 | 16.00 | 0.00 |
| Crest El. ft | = 243.00 | 244.50 | 244.00 | 0.00 |
| Weir Coeff. | = 3.33 | 2.60 | 3.33 | 0.00 |
| Weir Type | = Rect | Broad | Rect | — |
| Multi-Stage | = Yes | Yes | Yes | No |

Exfiltration Rate = 0.00 in/hr/sqft Tailwater Elev. = 0.00 ft

Stage / Storage / Discharge Table

Note: All outflows have been analyzed under inlet and outlet control.

| Stage ft | Storage cuft | Elevation ft | Civ A cfs | Civ B cfs | Civ C cfs | Civ D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Total cfs |
|----------|--------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-----------|
| 0.00 | 0 | 238.00 | 0.00 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.00 |
| 0.20 | 1,113 | 238.20 | 23.09 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.00 |
| 0.40 | 2,226 | 238.40 | 23.09 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.00 |
| 0.60 | 3,338 | 238.60 | 23.09 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.00 |
| 0.80 | 4,451 | 238.80 | 23.09 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.00 |
| 1.00 | 5,564 | 239.00 | 23.09 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.00 |
| 1.20 | 6,677 | 239.20 | 23.09 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.00 |
| 1.40 | 7,790 | 239.40 | 23.09 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.00 |
| 1.60 | 8,902 | 239.60 | 23.09 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.00 |
| 1.80 | 10,015 | 239.80 | 23.09 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.00 |
| 2.00 | 11,128 | 240.00 | 23.09 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.00 |
| 2.20 | 12,464 | 240.20 | 23.09 | 0.06 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.06 |
| 2.40 | 13,800 | 240.40 | 23.09 | 0.12 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.12 |
| 2.60 | 15,135 | 240.60 | 23.09 | 0.16 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.16 |
| 2.80 | 16,471 | 240.80 | 23.09 | 0.19 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.19 |
| 3.00 | 17,807 | 241.00 | 23.09 | 0.22 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.22 |
| 3.20 | 19,143 | 241.20 | 23.09 | 0.25 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.25 |
| 3.40 | 20,479 | 241.40 | 23.09 | 0.27 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.27 |
| 3.60 | 21,814 | 241.60 | 23.09 | 0.29 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.29 |
| 3.80 | 23,150 | 241.80 | 23.09 | 0.31 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.31 |
| 4.00 | 24,486 | 242.00 | 23.09 | 0.32 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.32 |
| 4.20 | 25,822 | 242.20 | 23.09 | 0.34 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.34 |
| 4.40 | 27,158 | 242.40 | 23.09 | 0.36 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.36 |
| 4.60 | 28,493 | 242.60 | 23.09 | 0.37 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.37 |
| 4.80 | 29,829 | 242.80 | 23.09 | 0.39 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.39 |
| 5.00 | 31,165 | 243.00 | 23.09 | 0.40 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.40 |
| 5.20 | 32,501 | 243.20 | 23.09 | 0.41 | --- | --- | 0.30 | 0.00 | 0.00 | --- | --- | 0.71 |
| 5.40 | 33,837 | 243.40 | 23.09 | 0.43 | --- | --- | 0.84 | 0.00 | 0.00 | --- | --- | 1.27 |
| 5.60 | 35,172 | 243.60 | 23.09 | 0.44 | --- | --- | 1.55 | 0.00 | 0.00 | --- | --- | 1.99 |
| 5.80 | 36,508 | 243.80 | 23.09 | 0.45 | --- | --- | 2.38 | 0.00 | 0.00 | --- | --- | 2.84 |
| 6.00 | 37,844 | 244.00 | 23.09 | 0.47 | --- | --- | 3.33 | 0.00 | 0.00 | --- | --- | 3.80 |
| 6.20 | 39,180 | 244.20 | 23.09 | 0.48 | --- | --- | 4.38 | 0.00 | 4.77 | --- | --- | 9.62 |

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Stage / Storage / Discharge Table

| Stage ft | Storage cuft | Elevation ft | Civ A cfs | Civ B cfs | Civ C cfs | Civ D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Total cfs |
|-------------|-----------------|-----------------|--------------|--------------|--------------|--------------|-------------|-------------|-------------|-------------|--------------|--------------|
| 6.40 | 40,516 | 244.40 | 23.09 | 0.49 | --- | --- | 5.52 | 0.00 | 13.48 | --- | --- | 19.48 |
| 6.60 | 41,851 | 244.60 | 27.65 | 0.12 | --- | --- | 3.92 | 3.29 | 20.31 | --- | --- | 27.64 |
| 6.80 | 43,187 | 244.80 | 27.92 | 0.05 | --- | --- | 2.40 | 10.00 | 15.47 | --- | --- | 27.92 |
| 7.00 | 44,523 | 245.00 | 28.07 | 0.03 | --- | --- | 1.86 | 12.37 | 13.75 | --- | --- | 28.02 |
| 7.20 | 45,859 | 245.20 | 28.21 | 0.02 | --- | --- | 1.58 | 13.73 | 12.83 | --- | --- | 28.16 |
| 7.40 | 47,195 | 245.40 | 28.34 | 0.02 | --- | --- | 1.40 | 14.64 | 12.28 | --- | --- | 28.34 |
| 7.60 | 48,530 | 245.60 | 28.47 | 0.01 | --- | --- | 1.28 | 15.27 | 11.88 | --- | --- | 28.43 |
| 7.80 | 49,866 | 245.80 | 28.60 | 0.01 | --- | --- | 1.18 | 15.60 | 11.49 | --- | --- | 28.28 |
| 8.00 | 51,202 | 246.00 | 28.73 | 0.01 | --- | --- | 1.11 | 15.96 | 11.27 | --- | --- | 28.34 |
| 8.05 | 51,536 | 246.05 | 28.76 | 0.01 | --- | --- | 1.10 | 16.14 | 11.30 | --- | --- | 28.55 |
| 8.10 | 51,870 | 246.10 | 28.79 | 0.01 | --- | --- | 1.09 | 16.28 | 11.29 | --- | --- | 28.67 |
| 8.15 | 52,204 | 246.15 | 28.82 | 0.01 | --- | --- | 1.08 | 16.37 | 11.27 | --- | --- | 28.72 |
| 8.20 | 52,538 | 246.20 | 28.86 | 0.01 | --- | --- | 1.06 | 16.40 | 11.20 | --- | --- | 28.68 |
| 8.25 | 52,872 | 246.25 | 28.89 | 0.01 | --- | --- | 1.05 | 16.38 | 11.10 | --- | --- | 28.53 |
| 8.30 | 53,206 | 246.30 | 28.92 | 0.01 | --- | --- | 1.02 | 16.28 | 10.96 | --- | --- | 28.28 |
| 8.35 | 53,540 | 246.35 | 28.95 | 0.01 | --- | --- | 1.00 | 16.06 | 10.74 | --- | --- | 27.80 |
| 8.40 | 53,874 | 246.40 | 28.98 | 0.01 | --- | --- | 1.01 | 16.54 | 11.00 | --- | --- | 28.56 |
| 8.45 | 54,208 | 246.45 | 29.01 | 0.01 | --- | --- | 0.98 | 16.25 | 10.74 | --- | --- | 27.98 |
| 8.50 | 54,542 | 246.50 | 29.05 | 0.01 | --- | --- | 0.98 | 16.46 | 10.82 | --- | --- | 28.27 |

...End

Hydrograph Report

Hyd. No. 12

Basin 2 Out

Hydrograph type = Reservoir
Storm frequency = 25 yrs
Inflow hyd. No. = 9
Max. Elevation = 233.29 ft

Peak discharge = 3.63 cfs
Time interval = 2 min
Reservoir name = Detention Basin 2
Max. Storage = 16,862 cuft

Storage Indication method used.

Outflow hydrograph volume = 34,040 cuft

Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 724 | 7.20 | 232.21 | 6.68 | 0.25 | ---- | ---- | 0.22 | ---- | ---- | ---- | 0.043 | 0.51 |
| 728 | 8.67 | 232.50 | 6.68 | 0.28 | ---- | ---- | 0.78 | ---- | ---- | ---- | 0.044 | 1.10 |
| 732 | 8.67 | 232.78 | 6.68 | 0.30 | ---- | ---- | 1.53 | ---- | ---- | ---- | 0.045 | 1.87 |
| 736 | 7.64 | 233.02 | 6.68 | 0.32 | ---- | ---- | 2.25 | ---- | ---- | ---- | 0.045 | 2.62 |
| 740 | 6.29 | 233.18 | 6.68 | 0.34 | ---- | ---- | 2.80 | ---- | ---- | ---- | 0.046 | 3.19 |
| 744 | 4.89 | 233.26 | 6.68 | 0.35 | ---- | ---- | 3.12 | ---- | ---- | ---- | 0.046 | 3.52 |
| 748 | 3.87 | 233.29 | 6.68 | 0.35 | ---- | ---- | 3.24 | ---- | ---- | ---- | 0.046 | 3.63 |
| 752 | 3.12 | 233.29 | 6.68 | 0.35 | ---- | ---- | 3.22 | ---- | ---- | ---- | 0.046 | 3.61 |
| 756 | 2.47 | 233.26 | 6.68 | 0.34 | ---- | ---- | 3.10 | ---- | ---- | ---- | 0.046 | 3.49 |
| 760 | 1.96 | 233.21 | 6.68 | 0.34 | ---- | ---- | 2.92 | ---- | ---- | ---- | 0.046 | 3.31 |
| 764 | 1.63 | 233.15 | 6.68 | 0.34 | ---- | ---- | 2.73 | ---- | ---- | ---- | 0.046 | 3.11 |
| 768 | 1.43 | 233.09 | 6.68 | 0.33 | ---- | ---- | 2.53 | ---- | ---- | ---- | 0.046 | 2.90 |
| 772 | 1.31 | 233.04 | 6.68 | 0.33 | ---- | ---- | 2.33 | ---- | ---- | ---- | 0.045 | 2.70 |
| 776 | 1.23 | 232.99 | 6.68 | 0.32 | ---- | ---- | 2.15 | ---- | ---- | ---- | 0.045 | 2.52 |
| 780 | 1.15 | 232.94 | 6.68 | 0.32 | ---- | ---- | 2.00 | ---- | ---- | ---- | 0.045 | 2.36 |
| 784 | 1.08 | 232.89 | 6.68 | 0.31 | ---- | ---- | 1.86 | ---- | ---- | ---- | 0.045 | 2.21 |
| 788 | 1.01 | 232.85 | 6.68 | 0.31 | ---- | ---- | 1.72 | ---- | ---- | ---- | 0.045 | 2.07 |
| 792 | 0.96 | 232.81 | 6.68 | 0.31 | ---- | ---- | 1.59 | ---- | ---- | ---- | 0.045 | 1.95 |
| 796 | 0.93 | 232.77 | 6.68 | 0.30 | ---- | ---- | 1.49 | ---- | ---- | ---- | 0.045 | 1.84 |
| 800 | 0.90 | 232.74 | 6.68 | 0.30 | ---- | ---- | 1.39 | ---- | ---- | ---- | 0.044 | 1.74 |
| 804 | 0.88 | 232.70 | 6.68 | 0.30 | ---- | ---- | 1.31 | ---- | ---- | ---- | 0.044 | 1.65 |
| 808 | 0.86 | 232.67 | 6.68 | 0.29 | ---- | ---- | 1.23 | ---- | ---- | ---- | 0.044 | 1.57 |
| 812 | 0.84 | 232.65 | 6.68 | 0.29 | ---- | ---- | 1.15 | ---- | ---- | ---- | 0.044 | 1.49 |
| 816 | 0.82 | 232.62 | 6.68 | 0.29 | ---- | ---- | 1.09 | ---- | ---- | ---- | 0.044 | 1.42 |
| 820 | 0.80 | 232.60 | 6.68 | 0.29 | ---- | ---- | 1.02 | ---- | ---- | ---- | 0.044 | 1.35 |
| 824 | 0.78 | 232.58 | 6.68 | 0.28 | ---- | ---- | 0.97 | ---- | ---- | ---- | 0.044 | 1.30 |
| 828 | 0.76 | 232.56 | 6.68 | 0.28 | ---- | ---- | 0.93 | ---- | ---- | ---- | 0.044 | 1.25 |
| 832 | 0.74 | 232.54 | 6.68 | 0.28 | ---- | ---- | 0.88 | ---- | ---- | ---- | 0.044 | 1.21 |
| 836 | 0.72 | 232.52 | 6.68 | 0.28 | ---- | ---- | 0.84 | ---- | ---- | ---- | 0.044 | 1.16 |
| 840 | 0.70 | 232.51 | 6.68 | 0.28 | ---- | ---- | 0.80 | ---- | ---- | ---- | 0.044 | 1.12 |
| 844 | 0.68 | 232.49 | 6.68 | 0.28 | ---- | ---- | 0.76 | ---- | ---- | ---- | 0.044 | 1.08 |
| 848 | 0.66 | 232.47 | 6.68 | 0.27 | ---- | ---- | 0.73 | ---- | ---- | ---- | 0.044 | 1.04 |
| 852 | 0.64 | 232.46 | 6.68 | 0.27 | ---- | ---- | 0.69 | ---- | ---- | ---- | 0.044 | 1.01 |
| 856 | 0.63 | 232.44 | 6.68 | 0.27 | ---- | ---- | 0.66 | ---- | ---- | ---- | 0.044 | 0.97 |
| 860 | 0.62 | 232.43 | 6.68 | 0.27 | ---- | ---- | 0.63 | ---- | ---- | ---- | 0.043 | 0.94 |
| 864 | 0.61 | 232.42 | 6.68 | 0.27 | ---- | ---- | 0.60 | ---- | ---- | ---- | 0.043 | 0.91 |
| 868 | 0.60 | 232.41 | 6.68 | 0.27 | ---- | ---- | 0.57 | ---- | ---- | ---- | 0.043 | 0.88 |
| 872 | 0.59 | 232.40 | 6.68 | 0.27 | ---- | ---- | 0.55 | ---- | ---- | ---- | 0.043 | 0.86 |

Continues on next page...

Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Civ A cfs | Civ B cfs | Civ C cfs | Civ D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 876 | 0.58 | 232.39 | 6.68 | 0.27 | ---- | ---- | 0.53 | ---- | ---- | ---- | 0.043 | 0.84 |
| 880 | 0.57 | 232.38 | 6.68 | 0.26 | ---- | ---- | 0.51 | ---- | ---- | ---- | 0.043 | 0.82 |
| 884 | 0.56 | 232.37 | 6.68 | 0.26 | ---- | ---- | 0.50 | ---- | ---- | ---- | 0.043 | 0.80 |
| 888 | 0.55 | 232.36 | 6.68 | 0.26 | ---- | ---- | 0.48 | ---- | ---- | ---- | 0.043 | 0.78 |
| 892 | 0.54 | 232.35 | 6.68 | 0.26 | ---- | ---- | 0.46 | ---- | ---- | ---- | 0.043 | 0.77 |
| 896 | 0.53 | 232.34 | 6.68 | 0.26 | ---- | ---- | 0.45 | ---- | ---- | ---- | 0.043 | 0.75 |
| 900 | 0.52 | 232.33 | 6.68 | 0.26 | ---- | ---- | 0.43 | ---- | ---- | ---- | 0.043 | 0.73 |
| 904 | 0.51 | 232.32 | 6.68 | 0.26 | ---- | ---- | 0.42 | ---- | ---- | ---- | 0.043 | 0.72 |
| 908 | 0.50 | 232.31 | 6.68 | 0.26 | ---- | ---- | 0.40 | ---- | ---- | ---- | 0.043 | 0.70 |
| 912 | 0.49 | 232.31 | 6.68 | 0.26 | ---- | ---- | 0.39 | ---- | ---- | ---- | 0.043 | 0.69 |
| 916 | 0.48 | 232.30 | 6.68 | 0.26 | ---- | ---- | 0.37 | ---- | ---- | ---- | 0.043 | 0.67 |
| 920 | 0.47 | 232.29 | 6.68 | 0.25 | ---- | ---- | 0.36 | ---- | ---- | ---- | 0.043 | 0.66 |
| 924 | 0.46 | 232.28 | 6.68 | 0.25 | ---- | ---- | 0.35 | ---- | ---- | ---- | 0.043 | 0.64 |
| 928 | 0.45 | 232.28 | 6.68 | 0.25 | ---- | ---- | 0.33 | ---- | ---- | ---- | 0.043 | 0.63 |
| 932 | 0.44 | 232.27 | 6.68 | 0.25 | ---- | ---- | 0.32 | ---- | ---- | ---- | 0.043 | 0.62 |
| 936 | 0.43 | 232.26 | 6.68 | 0.25 | ---- | ---- | 0.31 | ---- | ---- | ---- | 0.043 | 0.60 |
| 940 | 0.42 | 232.26 | 6.68 | 0.25 | ---- | ---- | 0.30 | ---- | ---- | ---- | 0.043 | 0.59 |
| 944 | 0.41 | 232.25 | 6.68 | 0.25 | ---- | ---- | 0.29 | ---- | ---- | ---- | 0.043 | 0.58 |
| 948 | 0.40 | 232.24 | 6.68 | 0.25 | ---- | ---- | 0.27 | ---- | ---- | ---- | 0.043 | 0.57 |
| 952 | 0.39 | 232.24 | 6.68 | 0.25 | ---- | ---- | 0.26 | ---- | ---- | ---- | 0.043 | 0.55 |
| 956 | 0.38 | 232.23 | 6.68 | 0.25 | ---- | ---- | 0.25 | ---- | ---- | ---- | 0.043 | 0.54 |
| 960 | 0.37 | 232.22 | 6.68 | 0.25 | ---- | ---- | 0.24 | ---- | ---- | ---- | 0.043 | 0.53 |
| 964 | 0.36 | 232.22 | 6.68 | 0.25 | ---- | ---- | 0.23 | ---- | ---- | ---- | 0.043 | 0.52 |
| 968 | 0.35 | 232.21 | 6.68 | 0.25 | ---- | ---- | 0.22 | ---- | ---- | ---- | 0.043 | 0.51 |
| 972 | 0.34 | 232.21 | 6.68 | 0.25 | ---- | ---- | 0.21 | ---- | ---- | ---- | 0.043 | 0.49 |
| 976 | 0.34 | 232.20 | 6.68 | 0.24 | ---- | ---- | 0.20 | ---- | ---- | ---- | 0.043 | 0.48 |
| 980 | 0.33 | 232.19 | 6.68 | 0.24 | ---- | ---- | 0.19 | ---- | ---- | ---- | 0.043 | 0.48 |
| 984 | 0.33 | 232.19 | 6.68 | 0.24 | ---- | ---- | 0.19 | ---- | ---- | ---- | 0.043 | 0.47 |
| 988 | 0.33 | 232.18 | 6.68 | 0.24 | ---- | ---- | 0.18 | ---- | ---- | ---- | 0.043 | 0.47 |
| 992 | 0.32 | 232.18 | 6.68 | 0.24 | ---- | ---- | 0.17 | ---- | ---- | ---- | 0.043 | 0.46 |
| 996 | 0.32 | 232.17 | 6.68 | 0.24 | ---- | ---- | 0.17 | ---- | ---- | ---- | 0.043 | 0.45 |
| 1000 | 0.31 | 232.17 | 6.68 | 0.24 | ---- | ---- | 0.16 | ---- | ---- | ---- | 0.043 | 0.45 |
| 1004 | 0.31 | 232.16 | 6.68 | 0.24 | ---- | ---- | 0.16 | ---- | ---- | ---- | 0.043 | 0.44 |
| 1008 | 0.30 | 232.16 | 6.68 | 0.24 | ---- | ---- | 0.15 | ---- | ---- | ---- | 0.043 | 0.44 |
| 1012 | 0.30 | 232.15 | 6.68 | 0.24 | ---- | ---- | 0.15 | ---- | ---- | ---- | 0.043 | 0.43 |
| 1016 | 0.29 | 232.15 | 6.68 | 0.24 | ---- | ---- | 0.14 | ---- | ---- | ---- | 0.043 | 0.42 |
| 1020 | 0.29 | 232.14 | 6.68 | 0.24 | ---- | ---- | 0.14 | ---- | ---- | ---- | 0.043 | 0.42 |
| 1024 | 0.29 | 232.14 | 6.68 | 0.24 | ---- | ---- | 0.13 | ---- | ---- | ---- | 0.043 | 0.41 |
| 1028 | 0.28 | 232.13 | 6.68 | 0.24 | ---- | ---- | 0.13 | ---- | ---- | ---- | 0.043 | 0.41 |
| 1032 | 0.28 | 232.13 | 6.68 | 0.24 | ---- | ---- | 0.12 | ---- | ---- | ---- | 0.043 | 0.40 |
| 1036 | 0.27 | 232.12 | 6.68 | 0.24 | ---- | ---- | 0.12 | ---- | ---- | ---- | 0.043 | 0.40 |
| 1040 | 0.27 | 232.12 | 6.68 | 0.23 | ---- | ---- | 0.11 | ---- | ---- | ---- | 0.042 | 0.39 |
| 1044 | 0.26 | 232.11 | 6.68 | 0.23 | ---- | ---- | 0.11 | ---- | ---- | ---- | 0.042 | 0.39 |
| 1048 | 0.26 | 232.11 | 6.68 | 0.23 | ---- | ---- | 0.10 | ---- | ---- | ---- | 0.042 | 0.38 |
| 1052 | 0.26 | 232.10 | 6.68 | 0.23 | ---- | ---- | 0.10 | ---- | ---- | ---- | 0.042 | 0.38 |
| 1056 | 0.25 | 232.10 | 6.68 | 0.23 | ---- | ---- | 0.10 | ---- | ---- | ---- | 0.042 | 0.37 |
| 1060 | 0.25 | 232.09 | 6.68 | 0.23 | ---- | ---- | 0.09 | ---- | ---- | ---- | 0.042 | 0.37 |

...End

Reservoir Report

Reservoir No. 2 - Detention Basin 2

Hydraflow Hydrographs by Intelisolve

Pond Data

Pond storage is based on known contour areas. Average end area method used.

Stage / Storage Table

| Stage (ft) | Elevation (ft) | Contour area (sqft) | Incr. Storage (cuft) | Total storage (cuft) |
|------------|----------------|---------------------|----------------------|----------------------|
| 0.00 | 229.33 | 00 | 0 | 0 |
| 0.67 | 230.00 | 2,454 | 822 | 822 |
| 2.67 | 232.00 | 5,689 | 8,143 | 8,965 |
| 4.67 | 234.00 | 6,522 | 12,211 | 21,176 |
| 6.67 | 236.00 | 7,413 | 13,935 | 35,111 |
| 8.67 | 238.00 | 9,192 | 16,605 | 51,716 |

Culvert / Orifice Structures

| | [A] | [B] | [C] | [D] |
|---------------|----------|--------|------|------|
| Rise in | = 6.0 | 3.0 | 0.0 | 0.0 |
| Span in | = 6.0 | 3.0 | 0.0 | 0.0 |
| No. Barrels | = 10 | 1 | 0 | 0 |
| Invert El. ft | = 228.40 | 231.00 | 0.00 | 0.00 |
| Length ft | = 40.0 | 1.0 | 0.0 | 0.0 |
| Slope % | = 1.00 | 0.00 | 0.00 | 0.00 |
| N-Value | = .013 | .013 | .000 | .000 |
| Orif. Coeff. | = 0.60 | 0.60 | 0.00 | 0.00 |
| Multi-Stage | = n/a | Yes | No | No |

Weir Structures

| | [A] | [B] | [C] | [D] |
|--------------|----------|--------|--------|------|
| Crest Len ft | = 0.66 | 20.00 | 16.00 | 0.00 |
| Crest El. ft | = 232.00 | 236.00 | 235.50 | 0.00 |
| Weir Coeff. | = 3.33 | 2.60 | 3.33 | 0.00 |
| Weir Type | = Rect | Broad | Rect | --- |
| Multi-Stage | = Yes | No | Yes | No |

Exfiltration Rate = 0.32 in/hr/sqft Tailwater Elev. = 0.00 ft

Stage / Storage / Discharge Table

Note: All outflows have been analyzed under inlet and outlet control.

| Stage ft | Storage cuft | Elevation ft | Civ A cfs | Civ B cfs | Civ C cfs | Civ D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Total cfs |
|----------|--------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-----------|
| 0.00 | 0 | 229.33 | 0.00 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.000 | 0.00 |
| 0.07 | 82 | 229.40 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.002 | 0.00 |
| 0.13 | 164 | 229.46 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.004 | 0.00 |
| 0.20 | 247 | 229.53 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.005 | 0.01 |
| 0.27 | 329 | 229.60 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.007 | 0.01 |
| 0.34 | 411 | 229.67 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.009 | 0.01 |
| 0.40 | 493 | 229.73 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.011 | 0.01 |
| 0.47 | 575 | 229.80 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.013 | 0.01 |
| 0.54 | 658 | 229.87 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.015 | 0.01 |
| 0.60 | 740 | 229.93 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.016 | 0.02 |
| 0.67 | 822 | 230.00 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.018 | 0.02 |
| 0.87 | 1,636 | 230.20 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.021 | 0.02 |
| 1.07 | 2,451 | 230.40 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.023 | 0.02 |
| 1.27 | 3,265 | 230.60 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.025 | 0.03 |
| 1.47 | 4,079 | 230.80 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.028 | 0.03 |
| 1.67 | 4,894 | 231.00 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.030 | 0.03 |
| 1.87 | 5,708 | 231.20 | 6.68 | 0.06 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.033 | 0.10 |
| 2.07 | 6,522 | 231.40 | 6.68 | 0.12 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.035 | 0.16 |
| 2.27 | 7,336 | 231.60 | 6.68 | 0.16 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.037 | 0.20 |
| 2.47 | 8,151 | 231.80 | 6.68 | 0.19 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.040 | 0.23 |
| 2.67 | 8,965 | 232.00 | 6.68 | 0.22 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.042 | 0.26 |
| 2.87 | 10,186 | 232.20 | 6.68 | 0.25 | --- | --- | 0.20 | 0.00 | 0.00 | --- | 0.043 | 0.48 |
| 3.07 | 11,407 | 232.40 | 6.68 | 0.27 | --- | --- | 0.56 | 0.00 | 0.00 | --- | 0.043 | 0.87 |
| 3.27 | 12,628 | 232.60 | 6.68 | 0.29 | --- | --- | 1.02 | 0.00 | 0.00 | --- | 0.044 | 1.35 |
| 3.47 | 13,849 | 232.80 | 6.68 | 0.31 | --- | --- | 1.57 | 0.00 | 0.00 | --- | 0.045 | 1.92 |
| 3.67 | 15,071 | 233.00 | 6.68 | 0.32 | --- | --- | 2.20 | 0.00 | 0.00 | --- | 0.045 | 2.57 |
| 3.87 | 16,292 | 233.20 | 6.68 | 0.34 | --- | --- | 2.89 | 0.00 | 0.00 | --- | 0.046 | 3.28 |
| 4.07 | 17,513 | 233.40 | 6.68 | 0.36 | --- | --- | 3.64 | 0.00 | 0.00 | --- | 0.046 | 4.04 |
| 4.27 | 18,734 | 233.60 | 6.68 | 0.37 | --- | --- | 4.45 | 0.00 | 0.00 | --- | 0.047 | 4.87 |
| 4.47 | 19,955 | 233.80 | 6.68 | 0.39 | --- | --- | 5.31 | 0.00 | 0.00 | --- | 0.048 | 5.74 |
| 4.67 | 21,176 | 234.00 | 6.68 | 0.40 | --- | --- | 6.22 | 0.00 | 0.00 | --- | 0.048 | 6.67 |
| 4.87 | 22,570 | 234.20 | 7.59 | 0.41 | --- | --- | 7.17 | 0.00 | 0.00 | --- | 0.049 | 7.64 |

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Detention Basin 2

Stage / Storage / Discharge Table

| Stage ft | Storage cuft | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Total cfs |
|-------------|-----------------|-----------------|--------------|--------------|--------------|--------------|-------------|-------------|-------------|-------------|--------------|--------------|
| 5.07 | 23,963 | 234.40 | 8.60 | 0.43 | --- | --- | 8.17 | 0.00 | 0.00 | --- | 0.050 | 8.65 |
| 5.27 | 25,357 | 234.60 | 9.65 | 0.44 | --- | --- | 9.21 | 0.00 | 0.00 | --- | 0.050 | 9.70 |
| 5.47 | 26,750 | 234.80 | 10.75 | 0.45 | --- | --- | 10.30 | 0.00 | 0.00 | --- | 0.051 | 10.80 |
| 5.67 | 28,144 | 235.00 | 11.89 | 0.47 | --- | --- | 11.42 | 0.00 | 0.00 | --- | 0.052 | 11.94 |
| 5.87 | 29,537 | 235.20 | 13.03 | 0.44 | --- | --- | 12.58 | 0.00 | 0.00 | --- | 0.052 | 13.08 |
| 6.07 | 30,931 | 235.40 | 14.12 | 0.42 | --- | --- | 13.70 | 0.00 | 0.00 | --- | 0.053 | 14.17 |
| 6.27 | 32,324 | 235.60 | 15.89 | 0.37 | --- | --- | 13.84 | 0.00 | 1.68 | --- | 0.054 | 15.94 |
| 6.47 | 33,718 | 235.80 | 18.81 | 0.20 | --- | --- | 9.85 | 0.00 | 8.75 | --- | 0.054 | 18.86 |
| 6.67 | 35,111 | 236.00 | 19.86 | 0.10 | --- | --- | 5.97 | 0.00 | 13.80 | --- | 0.055 | 19.92 |
| 6.87 | 36,772 | 236.20 | 20.25 | 0.07 | --- | --- | 4.74 | 4.65 | 15.44 | --- | 0.056 | 24.95 |
| 7.07 | 38,432 | 236.40 | 20.56 | 0.05 | --- | --- | 4.01 | 13.15 | 16.50 | --- | 0.058 | 33.77 |
| 7.27 | 40,093 | 236.60 | 20.84 | 0.04 | --- | --- | 3.52 | 24.17 | 17.27 | --- | 0.059 | 45.05 |
| 7.47 | 41,753 | 236.80 | 21.10 | 0.03 | --- | --- | 3.17 | 37.21 | 17.88 | --- | 0.060 | 58.35 |
| 7.67 | 43,414 | 237.00 | 21.36 | 0.03 | --- | --- | 2.91 | 52.00 | 18.41 | --- | 0.061 | 73.40 |
| 7.87 | 45,074 | 237.20 | 21.62 | 0.02 | --- | --- | 2.71 | 68.35 | 18.85 | --- | 0.063 | 90.00 |
| 8.07 | 46,735 | 237.40 | 21.87 | 0.02 | --- | --- | 2.54 | 86.14 | 19.22 | --- | 0.064 | 107.99 |
| 8.27 | 48,395 | 237.60 | 22.12 | 0.02 | --- | --- | 2.41 | 105.24 | 19.56 | --- | 0.065 | 127.29 |
| 8.47 | 50,056 | 237.80 | 22.36 | 0.02 | --- | --- | 2.31 | 125.57 | 19.95 | --- | 0.067 | 147.91 |
| 8.67 | 51,716 | 238.00 | 22.60 | 0.01 | --- | --- | 2.21 | 147.08 | 20.20 | --- | 0.068 | 169.58 |

...End

Hydrograph Report

Hyd. No. 13

Basin 3 Out

Hydrograph type = Reservoir
 Storm frequency = 25 yrs
 Inflow hyd. No. = 10
 Max. Elevation = 224.75 ft

Peak discharge = 2.45 cfs
 Time interval = 2 min
 Reservoir name = Basin 3 (Hotel)
 Max. Storage = 22,581 cuft

Storage Indication method used.

Outflow hydrograph volume = 48,122 cuft

Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 616 | 0.49 | 220.09 | 10.70 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 620 | 0.52 | 220.11 | 10.70 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 624 | 0.54 | 220.13 | 10.70 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 628 | 0.56 | 220.15 | 10.70 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 632 | 0.59 | 220.18 | 10.70 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 636 | 0.61 | 220.20 | 10.70 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 640 | 0.64 | 220.23 | 10.70 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 644 | 0.66 | 220.26 | 10.70 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 648 | 0.69 | 220.29 | 10.70 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 652 | 0.72 | 220.33 | 10.70 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 656 | 0.74 | 220.36 | 10.70 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 660 | 0.77 | 220.40 | 10.70 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 664 | 0.81 | 220.44 | 10.70 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 668 | 0.86 | 220.48 | 10.70 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 672 | 0.93 | 220.53 | 10.70 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 676 | 1.02 | 220.58 | 10.70 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 680 | 1.11 | 220.64 | 10.70 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 684 | 1.20 | 220.70 | 10.70 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 688 | 1.29 | 220.78 | 10.70 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 692 | 1.40 | 220.86 | 10.70 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 696 | 1.68 | 220.95 | 10.70 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 700 | 2.26 | 221.08 | 10.70 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 704 | 3.05 | 221.25 | 10.70 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 708 | 3.92 | 221.50 | 10.70 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 712 | 4.85 | 221.81 | 10.70 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 716 | 5.98 | 222.11 | 10.70 | 0.42 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.42 |
| 720 | 8.91 | 222.42 | 10.70 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.44 |
| 724 | 13.18 | 222.89 | 10.70 | 0.47 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.47 |
| 728 | 13.25 | 223.48 | 10.70 | 0.50 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.50 |
| 732 | 10.03 | 223.98 | 10.70 | 0.53 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.53 |
| 736 | 7.30 | 224.27 | 10.70 | 0.54 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | 0.87 |
| 740 | 5.97 | 224.46 | 10.70 | 0.55 | 0.86 | ---- | ---- | ---- | ---- | ---- | ---- | 1.42 |
| 744 | 5.03 | 224.60 | 10.70 | 0.56 | 1.35 | ---- | ---- | ---- | ---- | ---- | ---- | 1.91 |
| 748 | 4.06 | 224.69 | 10.70 | 0.56 | 1.68 | ---- | ---- | ---- | ---- | ---- | ---- | 2.24 |
| 752 | 3.10 | 224.74 | 10.70 | 0.57 | 1.84 | ---- | ---- | ---- | ---- | ---- | ---- | 2.41 |
| 756 | 2.36 | 224.75 << | 10.70 | 0.57 | 1.88 | ---- | ---- | ---- | ---- | ---- | ---- | 2.45 << |
| 760 | 2.00 | 224.74 | 10.70 | 0.57 | 1.84 | ---- | ---- | ---- | ---- | ---- | ---- | 2.41 |
| 764 | 1.84 | 224.72 | 10.70 | 0.57 | 1.78 | ---- | ---- | ---- | ---- | ---- | ---- | 2.35 |

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Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 768 | 1.74 | 224.70 | 10.70 | 0.56 | 1.71 | ---- | ---- | ---- | ---- | ---- | ---- | 2.28 |
| 772 | 1.64 | 224.68 | 10.70 | 0.56 | 1.64 | ---- | ---- | ---- | ---- | ---- | ---- | 2.20 |
| 776 | 1.53 | 224.66 | 10.70 | 0.56 | 1.56 | ---- | ---- | ---- | ---- | ---- | ---- | 2.12 |
| 780 | 1.43 | 224.64 | 10.70 | 0.56 | 1.48 | ---- | ---- | ---- | ---- | ---- | ---- | 2.04 |
| 784 | 1.33 | 224.62 | 10.70 | 0.56 | 1.40 | ---- | ---- | ---- | ---- | ---- | ---- | 1.96 |
| 788 | 1.27 | 224.59 | 10.70 | 0.56 | 1.32 | ---- | ---- | ---- | ---- | ---- | ---- | 1.88 |
| 792 | 1.23 | 224.57 | 10.70 | 0.56 | 1.24 | ---- | ---- | ---- | ---- | ---- | ---- | 1.80 |
| 796 | 1.20 | 224.55 | 10.70 | 0.56 | 1.17 | ---- | ---- | ---- | ---- | ---- | ---- | 1.73 |
| 800 | 1.18 | 224.53 | 10.70 | 0.56 | 1.11 | ---- | ---- | ---- | ---- | ---- | ---- | 1.66 |
| 804 | 1.15 | 224.52 | 10.70 | 0.56 | 1.05 | ---- | ---- | ---- | ---- | ---- | ---- | 1.60 |
| 808 | 1.12 | 224.50 | 10.70 | 0.55 | 0.99 | ---- | ---- | ---- | ---- | ---- | ---- | 1.55 |
| 812 | 1.10 | 224.49 | 10.70 | 0.55 | 0.94 | ---- | ---- | ---- | ---- | ---- | ---- | 1.49 |
| 816 | 1.07 | 224.47 | 10.70 | 0.55 | 0.89 | ---- | ---- | ---- | ---- | ---- | ---- | 1.44 |
| 820 | 1.04 | 224.46 | 10.70 | 0.55 | 0.85 | ---- | ---- | ---- | ---- | ---- | ---- | 1.40 |
| 824 | 1.02 | 224.45 | 10.70 | 0.55 | 0.80 | ---- | ---- | ---- | ---- | ---- | ---- | 1.35 |
| 828 | 0.99 | 224.43 | 10.70 | 0.55 | 0.76 | ---- | ---- | ---- | ---- | ---- | ---- | 1.31 |
| 832 | 0.96 | 224.42 | 10.70 | 0.55 | 0.72 | ---- | ---- | ---- | ---- | ---- | ---- | 1.27 |
| 836 | 0.93 | 224.41 | 10.70 | 0.55 | 0.68 | ---- | ---- | ---- | ---- | ---- | ---- | 1.23 |
| 840 | 0.91 | 224.40 | 10.70 | 0.55 | 0.64 | ---- | ---- | ---- | ---- | ---- | ---- | 1.19 |
| 844 | 0.88 | 224.39 | 10.70 | 0.55 | 0.62 | ---- | ---- | ---- | ---- | ---- | ---- | 1.17 |
| 848 | 0.86 | 224.38 | 10.70 | 0.55 | 0.59 | ---- | ---- | ---- | ---- | ---- | ---- | 1.14 |
| 852 | 0.85 | 224.37 | 10.70 | 0.55 | 0.57 | ---- | ---- | ---- | ---- | ---- | ---- | 1.12 |
| 856 | 0.83 | 224.36 | 10.70 | 0.55 | 0.55 | ---- | ---- | ---- | ---- | ---- | ---- | 1.10 |
| 860 | 0.82 | 224.35 | 10.70 | 0.55 | 0.53 | ---- | ---- | ---- | ---- | ---- | ---- | 1.07 |
| 864 | 0.81 | 224.34 | 10.70 | 0.55 | 0.51 | ---- | ---- | ---- | ---- | ---- | ---- | 1.05 |
| 868 | 0.79 | 224.33 | 10.70 | 0.55 | 0.49 | ---- | ---- | ---- | ---- | ---- | ---- | 1.03 |
| 872 | 0.78 | 224.33 | 10.70 | 0.55 | 0.47 | ---- | ---- | ---- | ---- | ---- | ---- | 1.01 |
| 876 | 0.77 | 224.32 | 10.70 | 0.54 | 0.45 | ---- | ---- | ---- | ---- | ---- | ---- | 0.99 |
| 880 | 0.75 | 224.31 | 10.70 | 0.54 | 0.43 | ---- | ---- | ---- | ---- | ---- | ---- | 0.97 |
| 884 | 0.74 | 224.30 | 10.70 | 0.54 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | 0.95 |
| 888 | 0.73 | 224.29 | 10.70 | 0.54 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | 0.94 |
| 892 | 0.71 | 224.29 | 10.70 | 0.54 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | 0.92 |
| 896 | 0.70 | 224.28 | 10.70 | 0.54 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | 0.90 |
| 900 | 0.69 | 224.27 | 10.70 | 0.54 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | 0.88 |
| 904 | 0.67 | 224.26 | 10.70 | 0.54 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | 0.87 |
| 908 | 0.66 | 224.26 | 10.70 | 0.54 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | 0.85 |
| 912 | 0.65 | 224.25 | 10.70 | 0.54 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | 0.84 |
| 916 | 0.63 | 224.24 | 10.70 | 0.54 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | 0.82 |
| 920 | 0.62 | 224.24 | 10.70 | 0.54 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | 0.80 |
| 924 | 0.61 | 224.23 | 10.70 | 0.54 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | 0.79 |
| 928 | 0.59 | 224.22 | 10.70 | 0.54 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | 0.77 |
| 932 | 0.58 | 224.22 | 10.70 | 0.54 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | 0.76 |
| 936 | 0.57 | 224.21 | 10.70 | 0.54 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | 0.74 |
| 940 | 0.55 | 224.21 | 10.70 | 0.54 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | 0.73 |
| 944 | 0.54 | 224.20 | 10.70 | 0.54 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | 0.72 |
| 948 | 0.53 | 224.19 | 10.70 | 0.54 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | 0.71 |
| 952 | 0.51 | 224.19 | 10.70 | 0.54 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | 0.70 |
| 956 | 0.50 | 224.18 | 10.70 | 0.54 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | 0.70 |
| 960 | 0.49 | 224.17 | 10.70 | 0.54 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | 0.69 |
| 964 | 0.47 | 224.16 | 10.70 | 0.54 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | 0.68 |
| 968 | 0.46 | 224.16 | 10.70 | 0.54 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | 0.68 |

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Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 972 | 0.46 | 224.15 | 10.70 | 0.54 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | 0.67 |
| 976 | 0.45 | 224.14 | 10.70 | 0.54 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | 0.66 |
| 980 | 0.45 | 224.13 | 10.70 | 0.54 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | 0.65 |
| 984 | 0.44 | 224.13 | 10.70 | 0.54 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | 0.65 |
| 988 | 0.43 | 224.12 | 10.70 | 0.53 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | 0.64 |
| 992 | 0.43 | 224.11 | 10.70 | 0.53 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | 0.63 |
| 996 | 0.42 | 224.10 | 10.70 | 0.53 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | 0.63 |
| 1000 | 0.42 | 224.10 | 10.70 | 0.53 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | 0.62 |
| 1004 | 0.41 | 224.09 | 10.70 | 0.53 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | 0.61 |
| 1008 | 0.40 | 224.08 | 10.70 | 0.53 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | 0.60 |
| 1012 | 0.40 | 224.07 | 10.70 | 0.53 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | 0.60 |
| 1016 | 0.39 | 224.07 | 10.70 | 0.53 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | 0.59 |
| 1020 | 0.39 | 224.06 | 10.70 | 0.53 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | 0.58 |
| 1024 | 0.38 | 224.05 | 10.70 | 0.53 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | 0.58 |
| 1028 | 0.37 | 224.05 | 10.70 | 0.53 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | 0.57 |
| 1032 | 0.37 | 224.04 | 10.70 | 0.53 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | 0.56 |
| 1036 | 0.36 | 224.03 | 10.70 | 0.53 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | 0.56 |
| 1040 | 0.36 | 224.02 | 10.70 | 0.53 | 0.02 | ---- | ---- | ---- | ---- | ---- | ---- | 0.55 |
| 1044 | 0.35 | 224.02 | 10.70 | 0.53 | 0.02 | ---- | ---- | ---- | ---- | ---- | ---- | 0.54 |
| 1048 | 0.35 | 224.01 | 10.70 | 0.53 | 0.01 | ---- | ---- | ---- | ---- | ---- | ---- | 0.54 |
| 1052 | 0.34 | 224.00 | 10.70 | 0.53 | 0.00 | ---- | ---- | ---- | ---- | ---- | ---- | 0.53 |
| 1056 | 0.33 | 224.00 | 10.70 | 0.53 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.53 |
| 1060 | 0.33 | 223.99 | 10.70 | 0.53 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.53 |
| 1064 | 0.32 | 223.98 | 10.70 | 0.53 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.53 |
| 1068 | 0.32 | 223.97 | 10.70 | 0.53 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.53 |
| 1072 | 0.31 | 223.96 | 10.70 | 0.53 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.53 |
| 1076 | 0.30 | 223.95 | 10.70 | 0.53 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.53 |
| 1080 | 0.30 | 223.94 | 10.70 | 0.53 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.53 |
| 1084 | 0.29 | 223.93 | 10.70 | 0.52 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.52 |
| 1088 | 0.29 | 223.92 | 10.70 | 0.52 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.52 |
| 1092 | 0.29 | 223.91 | 10.70 | 0.52 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.52 |
| 1096 | 0.28 | 223.90 | 10.70 | 0.52 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.52 |
| 1100 | 0.28 | 223.89 | 10.70 | 0.52 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.52 |
| 1104 | 0.28 | 223.88 | 10.70 | 0.52 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.52 |
| 1108 | 0.28 | 223.86 | 10.70 | 0.52 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.52 |
| 1112 | 0.28 | 223.85 | 10.70 | 0.52 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.52 |
| 1116 | 0.28 | 223.84 | 10.70 | 0.52 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.52 |
| 1120 | 0.27 | 223.83 | 10.70 | 0.52 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.52 |
| 1124 | 0.27 | 223.82 | 10.70 | 0.52 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.52 |
| 1128 | 0.27 | 223.81 | 10.70 | 0.52 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.52 |
| 1132 | 0.27 | 223.80 | 10.70 | 0.52 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.52 |
| 1136 | 0.27 | 223.79 | 10.70 | 0.52 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.52 |
| 1140 | 0.26 | 223.78 | 10.70 | 0.52 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.52 |
| 1144 | 0.26 | 223.76 | 10.70 | 0.52 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.52 |
| 1148 | 0.26 | 223.75 | 10.70 | 0.52 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.52 |
| 1152 | 0.26 | 223.74 | 10.70 | 0.51 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.51 |
| 1156 | 0.26 | 223.73 | 10.70 | 0.51 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.51 |
| 1160 | 0.26 | 223.72 | 10.70 | 0.51 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.51 |
| 1164 | 0.25 | 223.71 | 10.70 | 0.51 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.51 |
| 1168 | 0.25 | 223.70 | 10.70 | 0.51 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.51 |
| 1172 | 0.25 | 223.68 | 10.70 | 0.51 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.51 |

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Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 1176 | 0.25 | 223.67 | 10.70 | 0.51 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.51 |
| 1180 | 0.25 | 223.66 | 10.70 | 0.51 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.51 |
| 1184 | 0.25 | 223.65 | 10.70 | 0.51 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.51 |
| 1188 | 0.24 | 223.64 | 10.70 | 0.51 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.51 |
| 1192 | 0.24 | 223.63 | 10.70 | 0.51 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.51 |
| 1196 | 0.24 | 223.61 | 10.70 | 0.51 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.51 |
| 1200 | 0.24 | 223.60 | 10.70 | 0.51 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.51 |
| 1204 | 0.24 | 223.59 | 10.70 | 0.51 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.51 |
| 1208 | 0.23 | 223.58 | 10.70 | 0.51 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.51 |
| 1212 | 0.23 | 223.57 | 10.70 | 0.50 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.50 |
| 1216 | 0.23 | 223.55 | 10.70 | 0.50 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.50 |
| 1220 | 0.23 | 223.54 | 10.70 | 0.50 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.50 |
| 1224 | 0.23 | 223.53 | 10.70 | 0.50 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.50 |
| 1228 | 0.23 | 223.52 | 10.70 | 0.50 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.50 |
| 1232 | 0.22 | 223.50 | 10.70 | 0.50 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.50 |
| 1236 | 0.22 | 223.49 | 10.70 | 0.50 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.50 |
| 1240 | 0.22 | 223.48 | 10.70 | 0.50 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.50 |
| 1244 | 0.22 | 223.47 | 10.70 | 0.50 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.50 |
| 1248 | 0.22 | 223.45 | 10.70 | 0.50 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.50 |
| 1252 | 0.21 | 223.44 | 10.70 | 0.50 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.50 |
| 1256 | 0.21 | 223.43 | 10.70 | 0.50 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.50 |
| 1260 | 0.21 | 223.42 | 10.70 | 0.50 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.50 |
| 1264 | 0.21 | 223.40 | 10.70 | 0.50 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.50 |
| 1268 | 0.21 | 223.39 | 10.70 | 0.50 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.50 |
| 1272 | 0.21 | 223.38 | 10.70 | 0.49 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.49 |
| 1276 | 0.20 | 223.36 | 10.70 | 0.49 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.49 |
| 1280 | 0.20 | 223.35 | 10.70 | 0.49 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.49 |
| 1284 | 0.20 | 223.34 | 10.70 | 0.49 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.49 |
| 1288 | 0.20 | 223.33 | 10.70 | 0.49 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.49 |
| 1292 | 0.20 | 223.31 | 10.70 | 0.49 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.49 |
| 1296 | 0.20 | 223.30 | 10.70 | 0.49 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.49 |
| 1300 | 0.19 | 223.29 | 10.70 | 0.49 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.49 |
| 1304 | 0.19 | 223.27 | 10.70 | 0.49 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.49 |
| 1308 | 0.19 | 223.26 | 10.70 | 0.49 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.49 |
| 1312 | 0.19 | 223.25 | 10.70 | 0.49 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.49 |
| 1316 | 0.19 | 223.23 | 10.70 | 0.49 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.49 |
| 1320 | 0.18 | 223.22 | 10.70 | 0.49 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.49 |
| 1324 | 0.26 | 223.21 | 10.70 | 0.48 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.48 |
| 1328 | 0.27 | 223.20 | 10.70 | 0.48 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.48 |
| 1332 | 0.23 | 223.19 | 10.70 | 0.48 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.48 |
| 1336 | 0.19 | 223.18 | 10.70 | 0.48 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.48 |
| 1340 | 0.19 | 223.16 | 10.70 | 0.48 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.48 |
| 1344 | 0.19 | 223.15 | 10.70 | 0.48 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.48 |
| 1348 | 0.19 | 223.14 | 10.70 | 0.48 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.48 |
| 1352 | 0.19 | 223.12 | 10.70 | 0.48 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.48 |
| 1356 | 0.19 | 223.11 | 10.70 | 0.48 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.48 |
| 1360 | 0.18 | 223.10 | 10.70 | 0.48 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.48 |
| 1364 | 0.18 | 223.08 | 10.70 | 0.48 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.48 |
| 1368 | 0.18 | 223.07 | 10.70 | 0.48 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.48 |
| 1372 | 0.18 | 223.06 | 10.70 | 0.48 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.48 |
| 1376 | 0.18 | 223.04 | 10.70 | 0.48 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.48 |

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Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|---------------|---------------|-----------------|--------------|--------------|--------------|--------------|-------------|-------------|-------------|-------------|--------------|----------------|
| 1380 | 0.18 | 223.03 | 10.70 | 0.47 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.47 |
| 1384 | 0.18 | 223.02 | 10.70 | 0.47 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.47 |
| 1388 | 0.17 | 223.01 | 10.70 | 0.47 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.47 |
| 1392 | 0.17 | 222.99 | 10.70 | 0.47 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.47 |
| 1396 | 0.17 | 222.98 | 10.70 | 0.47 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.47 |
| 1400 | 0.17 | 222.96 | 10.70 | 0.47 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.47 |
| 1404 | 0.17 | 222.95 | 10.70 | 0.47 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.47 |
| 1408 | 0.17 | 222.94 | 10.70 | 0.47 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.47 |
| 1412 | 0.17 | 222.92 | 10.70 | 0.47 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.47 |
| 1416 | 0.17 | 222.91 | 10.70 | 0.47 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.47 |
| 1420 | 0.16 | 222.90 | 10.70 | 0.47 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.47 |
| 1424 | 0.16 | 222.88 | 10.70 | 0.47 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.47 |
| 1428 | 0.16 | 222.87 | 10.70 | 0.46 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.46 |
| 1432 | 0.16 | 222.86 | 10.70 | 0.46 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.46 |
| 1436 | 0.16 | 222.84 | 10.70 | 0.46 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.46 |
| 1440 | 0.16 | 222.83 | 10.70 | 0.46 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.46 |
| 1444 | 0.11 | 222.82 | 10.70 | 0.46 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.46 |
| 1448 | 0.04 | 222.80 | 10.70 | 0.46 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.46 |
| 1452 | 0.01 | 222.78 | 10.70 | 0.46 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.46 |
| 1456 | 0.00 | 222.76 | 10.70 | 0.46 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.46 |
| 1460 | 0.00 | 222.74 | 10.70 | 0.46 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.46 |
| 1464 | 0.00 | 222.72 | 10.70 | 0.46 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.46 |
| 1468 | 0.00 | 222.70 | 10.70 | 0.45 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.45 |
| 1472 | 0.00 | 222.68 | 10.70 | 0.45 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.45 |
| 1476 | 0.00 | 222.66 | 10.70 | 0.45 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.45 |
| 1480 | 0.00 | 222.64 | 10.70 | 0.45 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.45 |
| 1484 | 0.00 | 222.62 | 10.70 | 0.45 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.45 |
| 1488 | 0.00 | 222.60 | 10.70 | 0.45 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.45 |
| 1492 | 0.00 | 222.58 | 10.70 | 0.45 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.45 |
| 1496 | 0.00 | 222.56 | 10.70 | 0.45 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.45 |
| 1500 | 0.00 | 222.54 | 10.70 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.44 |
| 1504 | 0.00 | 222.52 | 10.70 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.44 |
| 1508 | 0.00 | 222.50 | 10.70 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.44 |
| 1512 | 0.00 | 222.48 | 10.70 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.44 |
| 1516 | 0.00 | 222.46 | 10.70 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.44 |
| 1520 | 0.00 | 222.44 | 10.70 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.44 |
| 1524 | 0.00 | 222.42 | 10.70 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.44 |
| 1528 | 0.00 | 222.40 | 10.70 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.44 |
| 1532 | 0.00 | 222.38 | 10.70 | 0.43 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.43 |
| 1536 | 0.00 | 222.36 | 10.70 | 0.43 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.43 |
| 1540 | 0.00 | 222.34 | 10.70 | 0.43 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.43 |
| 1544 | 0.00 | 222.32 | 10.70 | 0.43 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.43 |
| 1548 | 0.00 | 222.30 | 10.70 | 0.43 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.43 |
| 1552 | 0.00 | 222.28 | 10.70 | 0.43 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.43 |
| 1556 | 0.00 | 222.26 | 10.70 | 0.43 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.43 |
| 1560 | 0.00 | 222.24 | 10.70 | 0.43 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.43 |
| 1564 | 0.00 | 222.23 | 10.70 | 0.42 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.42 |
| 1568 | 0.00 | 222.21 | 10.70 | 0.42 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.42 |
| 1572 | 0.00 | 222.19 | 10.70 | 0.42 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.42 |
| 1576 | 0.00 | 222.17 | 10.70 | 0.42 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.42 |
| 1580 | 0.00 | 222.15 | 10.70 | 0.42 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.42 |

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Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 1584 | 0.00 | 222.13 | 10.70 | 0.42 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.42 |
| 1588 | 0.00 | 222.11 | 10.70 | 0.42 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.42 |
| 1592 | 0.00 | 222.09 | 10.70 | 0.42 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.42 |
| 1596 | 0.00 | 222.08 | 10.70 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.41 |
| 1600 | 0.00 | 222.06 | 10.70 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.41 |
| 1604 | 0.00 | 222.04 | 10.70 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.41 |
| 1608 | 0.00 | 222.02 | 10.70 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.41 |
| 1612 | 0.00 | 222.00 | 10.70 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.41 |
| 1616 | 0.00 | 221.97 | 10.70 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.41 |
| 1620 | 0.00 | 221.94 | 10.70 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.41 |
| 1624 | 0.00 | 221.91 | 10.70 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 1628 | 0.00 | 221.88 | 10.70 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 1632 | 0.00 | 221.85 | 10.70 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 1636 | 0.00 | 221.82 | 10.70 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 1640 | 0.00 | 221.79 | 10.70 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1644 | 0.00 | 221.76 | 10.70 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1648 | 0.00 | 221.72 | 10.70 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1652 | 0.00 | 221.69 | 10.70 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1656 | 0.00 | 221.66 | 10.70 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1660 | 0.00 | 221.63 | 10.70 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1664 | 0.00 | 221.61 | 10.70 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1668 | 0.00 | 221.58 | 10.70 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1672 | 0.00 | 221.55 | 10.70 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1676 | 0.00 | 221.52 | 10.70 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1680 | 0.00 | 221.49 | 10.70 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1684 | 0.00 | 221.46 | 10.70 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1688 | 0.00 | 221.43 | 10.70 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1692 | 0.00 | 221.40 | 10.70 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1696 | 0.00 | 221.37 | 10.70 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1700 | 0.00 | 221.35 | 10.70 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1704 | 0.00 | 221.32 | 10.70 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1708 | 0.00 | 221.29 | 10.70 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1712 | 0.00 | 221.26 | 10.70 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1716 | 0.00 | 221.23 | 10.70 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1720 | 0.00 | 221.21 | 10.70 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1724 | 0.00 | 221.18 | 10.70 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1728 | 0.00 | 221.15 | 10.70 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1732 | 0.00 | 221.13 | 10.70 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1736 | 0.00 | 221.10 | 10.70 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1740 | 0.00 | 221.07 | 10.70 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1744 | 0.00 | 221.05 | 10.70 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1748 | 0.00 | 221.02 | 10.70 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1752 | 0.00 | 220.99 | 10.70 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1756 | 0.00 | 220.97 | 10.70 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1760 | 0.00 | 220.94 | 10.70 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1764 | 0.00 | 220.92 | 10.70 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1768 | 0.00 | 220.89 | 10.70 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1772 | 0.00 | 220.87 | 10.70 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1776 | 0.00 | 220.84 | 10.70 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1780 | 0.00 | 220.82 | 10.70 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1784 | 0.00 | 220.79 | 10.70 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |

Continues on next page...

Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|---------------|---------------|-----------------|--------------|--------------|--------------|--------------|-------------|-------------|-------------|-------------|--------------|----------------|
| 1788 | 0.00 | 220.77 | 10.70 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1792 | 0.00 | 220.74 | 10.70 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1796 | 0.00 | 220.72 | 10.70 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1800 | 0.00 | 220.70 | 10.70 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1804 | 0.00 | 220.67 | 10.70 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1808 | 0.00 | 220.65 | 10.70 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1812 | 0.00 | 220.62 | 10.70 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1816 | 0.00 | 220.60 | 10.70 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1820 | 0.00 | 220.58 | 10.70 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1824 | 0.00 | 220.56 | 10.70 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1828 | 0.00 | 220.53 | 10.70 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1832 | 0.00 | 220.51 | 10.70 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1836 | 0.00 | 220.49 | 10.70 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1840 | 0.00 | 220.47 | 10.70 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1844 | 0.00 | 220.44 | 10.70 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 1848 | 0.00 | 220.42 | 10.70 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 1852 | 0.00 | 220.40 | 10.70 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 1856 | 0.00 | 220.38 | 10.70 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 1860 | 0.00 | 220.36 | 10.70 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 1864 | 0.00 | 220.34 | 10.70 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 1868 | 0.00 | 220.31 | 10.70 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 1872 | 0.00 | 220.29 | 10.70 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 1876 | 0.00 | 220.27 | 10.70 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 1880 | 0.00 | 220.25 | 10.70 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 1884 | 0.00 | 220.23 | 10.70 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 1888 | 0.00 | 220.21 | 10.70 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 1892 | 0.00 | 220.19 | 10.70 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 1896 | 0.00 | 220.17 | 10.70 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 1900 | 0.00 | 220.15 | 10.70 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 1904 | 0.00 | 220.13 | 10.70 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 1908 | 0.00 | 220.11 | 10.70 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 1912 | 0.00 | 220.09 | 10.70 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |

...End

Reservoir Report

Reservoir No. 3 - Basin 3 (Hotel)

Hydraflow Hydrographs by Intelisolve

Pond Data

Pond storage is based on known contour areas. Average end area method used.

Stage / Storage Table

| Stage (ft) | Elevation (ft) | Contour area (sqft) | Incr. Storage (cuft) | Total storage (cuft) |
|------------|----------------|---------------------|----------------------|----------------------|
| 0.00 | 219.00 | 00 | 0 | 0 |
| 1.00 | 220.00 | 1,406 | 703 | 703 |
| 3.00 | 222.00 | 4,776 | 6,182 | 6,885 |
| 5.00 | 224.00 | 5,971 | 10,747 | 17,632 |
| 7.00 | 226.00 | 7,278 | 13,249 | 30,881 |
| 9.00 | 228.00 | 8,709 | 15,987 | 46,868 |
| 9.50 | 228.50 | 9,086 | 4,449 | 51,317 |

Culvert / Orifice Structures

| | [A] | [B] | [C] | [D] |
|---------------|----------|--------|--------|------|
| Rise in | = 24.0 | 3.0 | 12.0 | 0.0 |
| Span in | = 24.0 | 3.0 | 12.0 | 0.0 |
| No. Barrels | = 1 | 1 | 1 | 0 |
| Invert El. ft | = 217.50 | 217.90 | 224.00 | 0.00 |
| Length ft | = 48.0 | 1.0 | 1.0 | 0.0 |
| Slope % | = 10.00 | 0.00 | 0.00 | 0.00 |
| N-Value | = .013 | .013 | .013 | .000 |
| Orif. Coeff. | = 0.60 | 0.60 | 0.60 | 0.00 |
| Multi-Stage | = n/a | Yes | Yes | No |

Weir Structures

| | [A] | [B] | [C] | [D] |
|--------------|----------|--------|--------|--------|
| Crest Len ft | = 1.00 | 2.00 | 16.00 | 90.00 |
| Crest El. ft | = 225.25 | 226.00 | 227.00 | 227.00 |
| Weir Coeff. | = 3.33 | 3.33 | 3.33 | 2.60 |
| Weir Type | = Rect | Rect | Rect | Broad |
| Multi-Stage | = Yes | Yes | Yes | Yes |

Exfiltration Rate = 0.00 in/hr/sqft Tailwater Elev. = 0.00 ft

Stage / Storage / Discharge Table

Note: All outflows have been analyzed under inlet and outlet control.

| Stage ft | Storage cuft | Elevation ft | Civ A cfs | Civ B cfs | Civ C cfs | Civ D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Total cfs |
|----------|--------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-----------|
| 0.00 | 0 | 219.00 | 0.00 | 0.00 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.00 |
| 0.10 | 70 | 219.10 | 10.70 | 0.07 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.07 |
| 0.20 | 141 | 219.20 | 10.70 | 0.11 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.11 |
| 0.30 | 211 | 219.30 | 10.70 | 0.13 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.13 |
| 0.40 | 281 | 219.40 | 10.70 | 0.15 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.15 |
| 0.50 | 352 | 219.50 | 10.70 | 0.17 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.17 |
| 0.60 | 422 | 219.60 | 10.70 | 0.18 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.18 |
| 0.70 | 492 | 219.70 | 10.70 | 0.20 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.20 |
| 0.80 | 562 | 219.80 | 10.70 | 0.21 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.21 |
| 0.90 | 633 | 219.90 | 10.70 | 0.22 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.22 |
| 1.00 | 703 | 220.00 | 10.70 | 0.24 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.24 |
| 1.20 | 1,321 | 220.20 | 10.70 | 0.26 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.26 |
| 1.40 | 1,939 | 220.40 | 10.70 | 0.28 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.28 |
| 1.60 | 2,558 | 220.60 | 10.70 | 0.30 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.30 |
| 1.80 | 3,176 | 220.80 | 10.70 | 0.32 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.32 |
| 2.00 | 3,794 | 221.00 | 10.70 | 0.33 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.33 |
| 2.20 | 4,412 | 221.20 | 10.70 | 0.35 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.35 |
| 2.40 | 5,030 | 221.40 | 10.70 | 0.37 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.37 |
| 2.60 | 5,649 | 221.60 | 10.70 | 0.38 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.38 |
| 2.80 | 6,267 | 221.80 | 10.70 | 0.40 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.40 |
| 3.00 | 6,885 | 222.00 | 10.70 | 0.41 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.41 |
| 3.20 | 7,960 | 222.20 | 10.70 | 0.42 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.42 |
| 3.40 | 9,034 | 222.40 | 10.70 | 0.44 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.44 |
| 3.60 | 10,109 | 222.60 | 10.70 | 0.45 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.45 |
| 3.80 | 11,184 | 222.80 | 10.70 | 0.46 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.46 |
| 4.00 | 12,259 | 223.00 | 10.70 | 0.47 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.47 |
| 4.20 | 13,333 | 223.20 | 10.70 | 0.48 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.48 |
| 4.40 | 14,408 | 223.40 | 10.70 | 0.50 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.50 |
| 4.60 | 15,483 | 223.60 | 10.70 | 0.51 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.51 |
| 4.80 | 16,557 | 223.80 | 10.70 | 0.52 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.52 |
| 5.00 | 17,632 | 224.00 | 10.70 | 0.53 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.53 |

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Stage / Storage / Discharge Table

| Stage ft | Storage cuft | Elevation ft | Civ A cfs | Civ B cfs | Civ C cfs | Civ D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Total cfs |
|----------|--------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-----------|
| 5.20 | 18,957 | 224.20 | 10.70 | 0.54 | 0.18 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.72 |
| 5.40 | 20,282 | 224.40 | 10.70 | 0.55 | 0.64 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 1.19 |
| 5.60 | 21,607 | 224.60 | 10.70 | 0.56 | 1.34 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 1.90 |
| 5.80 | 22,932 | 224.80 | 10.70 | 0.57 | 2.07 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 2.64 |
| 6.00 | 24,257 | 225.00 | 10.70 | 0.58 | 2.67 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 3.25 |
| 6.20 | 25,581 | 225.20 | 10.70 | 0.59 | 3.16 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 3.75 |
| 6.40 | 26,906 | 225.40 | 10.70 | 0.60 | 3.59 | --- | 0.19 | 0.00 | 0.00 | 0.00 | --- | 4.38 |
| 6.60 | 28,231 | 225.60 | 10.70 | 0.61 | 3.97 | --- | 0.69 | 0.00 | 0.00 | 0.00 | --- | 5.26 |
| 6.80 | 29,556 | 225.80 | 10.70 | 0.62 | 4.31 | --- | 1.36 | 0.00 | 0.00 | 0.00 | --- | 6.29 |
| 7.00 | 30,881 | 226.00 | 10.70 | 0.63 | 4.63 | --- | 2.16 | 0.00 | 0.00 | 0.00 | --- | 7.42 |
| 7.20 | 32,480 | 226.20 | 10.70 | 0.63 | 4.93 | --- | 3.08 | 0.60 | 0.00 | 0.00 | --- | 9.24 |
| 7.40 | 34,078 | 226.40 | 11.69 | 0.64 | 5.21 | --- | 4.11 | 1.68 | 0.00 | 0.00 | --- | 11.64 |
| 7.60 | 35,677 | 226.60 | 14.47 | 0.63 | 5.48 | --- | 5.22 | 3.10 | 0.00 | 0.00 | --- | 14.43 |
| 7.80 | 37,276 | 226.80 | 17.55 | 0.62 | 5.73 | --- | 6.43 | 4.77 | 0.00 | 0.00 | --- | 17.55 |
| 8.00 | 38,875 | 227.00 | 20.95 | 0.61 | 5.98 | --- | 7.71 | 6.66 | 0.00 | 0.00 | --- | 20.95 |
| 8.20 | 40,473 | 227.20 | 42.98 | 0.19 | 2.99 | --- | 6.61 | 7.50 | 4.76 | 20.93 | --- | 42.98 |
| 8.40 | 42,072 | 227.40 | 45.00 | 0.05 | 0.84 | --- | 2.87 | 3.56 | 6.98 | 30.65 | --- | 44.96 |
| 8.60 | 43,671 | 227.60 | 45.58 | 0.03 | 0.50 | --- | 2.13 | 2.78 | 7.43 | 32.62 | --- | 45.49 |
| 8.80 | 45,269 | 227.80 | 46.10 | 0.02 | 0.35 | --- | 1.75 | 2.38 | 7.69 | 33.77 | --- | 45.95 |
| 9.00 | 46,868 | 228.00 | 46.61 | 0.02 | 0.26 | --- | 1.53 | 2.14 | 7.90 | 34.69 | --- | 46.53 |
| 9.05 | 47,313 | 228.05 | 46.73 | 0.02 | 0.24 | --- | 1.48 | 2.09 | 7.91 | 34.75 | --- | 46.48 |
| 9.10 | 47,758 | 228.10 | 46.85 | 0.01 | 0.23 | --- | 1.43 | 2.04 | 7.92 | 34.79 | --- | 46.41 |
| 9.15 | 48,203 | 228.15 | 46.98 | 0.01 | 0.21 | --- | 1.39 | 2.00 | 7.95 | 34.93 | --- | 46.50 |
| 9.20 | 48,648 | 228.20 | 47.10 | 0.01 | 0.20 | --- | 1.37 | 1.97 | 8.02 | 35.22 | --- | 46.79 |
| 9.25 | 49,092 | 228.25 | 47.22 | 0.01 | 0.19 | --- | 1.33 | 1.94 | 8.04 | 35.33 | --- | 46.85 |
| 9.30 | 49,537 | 228.30 | 47.34 | 0.01 | 0.18 | --- | 1.30 | 1.89 | 8.01 | 35.19 | --- | 46.59 |
| 9.35 | 49,982 | 228.35 | 47.46 | 0.01 | 0.17 | --- | 1.27 | 1.87 | 8.07 | 35.43 | --- | 46.82 |
| 9.40 | 50,427 | 228.40 | 47.58 | 0.01 | 0.16 | --- | 1.25 | 1.84 | 8.07 | 35.43 | --- | 46.76 |
| 9.45 | 50,872 | 228.45 | 47.70 | 0.01 | 0.16 | --- | 1.24 | 1.84 | 8.21 | 36.07 | --- | 47.54 |
| 9.50 | 51,317 | 228.50 | 47.83 | 0.01 | 0.15 | --- | 1.20 | 1.79 | 8.08 | 35.50 | --- | 46.73 |

...End

Hydrograph Report

Hyd. No. 14

Hydrograph type = Combine
Storm frequency = 25 yrs
Inflow hyds. = 11, 12, 13

Peak discharge = 7.01 cfs
Time interval = 2 min

Hydrograph Volume = 112,061 cuft

Hydrograph Discharge Table

| Time (min) | Hyd. 11 + (cfs) | Hyd. 12 + (cfs) | Hyd. 13 = (cfs) | Outflow (cfs) |
|------------|-----------------|-----------------|-----------------|---------------|
| 712 | 0.18 | 0.19 | 0.40 | 0.76 |
| 716 | 0.20 | 0.22 | 0.42 | 0.83 |
| 720 | 0.21 | 0.26 | 0.44 | 0.91 |
| 724 | 0.24 | 0.51 | 0.47 | 1.32 |
| 728 | 0.27 | 1.10 | 0.50 | 2.23 |
| 732 | 0.29 | 1.87 | 0.53 | 3.35 |
| 736 | 0.31 | 2.62 | 0.87 | 4.67 |
| 740 | 0.33 | 3.19 | 1.42 | 5.87 |
| 744 | 0.34 | 3.52 | 1.91 | 6.64 |
| 748 | 0.35 | 3.63 | 2.24 | 6.97 |
| 752 | 0.35 | 3.61 | 2.41 | 6.98 |
| 756 | 0.36 | 3.49 | 2.45 << | 6.75 |
| 760 | 0.36 | 3.31 | 2.41 | 6.39 |
| 764 | 0.37 | 3.11 | 2.35 | 6.01 |
| 768 | 0.37 | 2.90 | 2.28 | 5.64 |
| 772 | 0.37 | 2.70 | 2.20 | 5.29 |
| 776 | 0.37 | 2.52 | 2.12 | 4.99 |
| 780 | 0.37 | 2.36 | 2.04 | 4.70 |
| 784 | 0.37 | 2.21 | 1.96 | 4.44 |
| 788 | 0.38 | 2.07 | 1.88 | 4.20 |
| 792 | 0.38 | 1.95 | 1.80 | 3.98 |
| 796 | 0.38 | 1.84 | 1.73 | 3.80 |
| 800 | 0.38 | 1.74 | 1.66 | 3.63 |
| 804 | 0.38 | 1.65 | 1.60 | 3.48 |
| 808 | 0.38 | 1.57 | 1.55 | 3.34 |
| 812 | 0.38 | 1.49 | 1.49 | 3.21 |
| 816 | 0.38 | 1.42 | 1.44 | 3.10 |
| 820 | 0.38 | 1.35 | 1.40 | 2.99 |
| 824 | 0.38 | 1.30 | 1.35 | 2.89 |
| 828 | 0.38 | 1.25 | 1.31 | 2.81 |
| 832 | 0.39 | 1.21 | 1.27 | 2.73 |
| 836 | 0.39 | 1.16 | 1.23 | 2.65 |
| 840 | 0.39 | 1.12 | 1.19 | 2.58 |
| 844 | 0.39 | 1.08 | 1.17 | 2.52 |
| 848 | 0.39 | 1.04 | 1.14 | 2.47 |
| 852 | 0.39 | 1.01 | 1.12 | 2.41 |
| 856 | 0.39 | 0.97 | 1.10 | 2.36 |
| 860 | 0.39 | 0.94 | 1.07 | 2.31 |

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Hydrograph Discharge Table

| Time (min) | Hyd. 11 + (cfs) | Hyd. 12 + (cfs) | Hyd. 13 = (cfs) | Outflow (cfs) |
|---------------|--------------------|--------------------|--------------------|------------------|
| 864 | 0.39 | 0.91 | 1.05 | 2.27 |
| 868 | 0.39 | 0.88 | 1.03 | 2.22 |
| 872 | 0.39 | 0.86 | 1.01 | 2.18 |
| 876 | 0.39 | 0.84 | 0.99 | 2.14 |
| 880 | 0.39 | 0.82 | 0.97 | 2.10 |
| 884 | 0.39 | 0.80 | 0.95 | 2.07 |
| 888 | 0.39 | 0.78 | 0.94 | 2.03 |
| 892 | 0.39 | 0.77 | 0.92 | 2.00 |
| 896 | 0.39 | 0.75 | 0.90 | 1.96 |
| 900 | 0.39 | 0.73 | 0.88 | 1.93 |
| 904 | 0.39 | 0.72 | 0.87 | 1.90 |
| 908 | 0.39 | 0.70 | 0.85 | 1.87 |
| 912 | 0.39 | 0.69 | 0.84 | 1.84 |
| 916 | 0.39 | 0.67 | 0.82 | 1.81 |
| 920 | 0.39 | 0.66 | 0.80 | 1.78 |
| 924 | 0.39 << | 0.64 | 0.79 | 1.76 |
| 928 | 0.39 | 0.63 | 0.77 | 1.74 |
| 932 | 0.39 | 0.62 | 0.76 | 1.71 |
| 936 | 0.39 | 0.60 | 0.74 | 1.69 |
| 940 | 0.39 | 0.59 | 0.73 | 1.67 |
| 944 | 0.39 | 0.58 | 0.72 | 1.65 |
| 948 | 0.39 | 0.57 | 0.71 | 1.63 |
| 952 | 0.39 | 0.55 | 0.70 | 1.62 |
| 956 | 0.39 | 0.54 | 0.70 | 1.60 |
| 960 | 0.39 | 0.53 | 0.69 | 1.59 |
| 964 | 0.39 | 0.52 | 0.68 | 1.57 |
| 968 | 0.39 | 0.51 | 0.68 | 1.55 |
| 972 | 0.39 | 0.49 | 0.67 | 1.54 |
| 976 | 0.39 | 0.48 | 0.66 | 1.52 |
| 980 | 0.39 | 0.48 | 0.65 | 1.51 |
| 984 | 0.39 | 0.47 | 0.65 | 1.49 |
| 988 | 0.39 | 0.47 | 0.64 | 1.48 |
| 992 | 0.39 | 0.46 | 0.63 | 1.46 |
| 996 | 0.39 | 0.45 | 0.63 | 1.45 |
| 1000 | 0.39 | 0.45 | 0.62 | 1.43 |
| 1004 | 0.39 | 0.44 | 0.61 | 1.42 |
| 1008 | 0.39 | 0.44 | 0.60 | 1.40 |
| 1012 | 0.39 | 0.43 | 0.60 | 1.39 |
| 1016 | 0.39 | 0.42 | 0.59 | 1.38 |
| 1020 | 0.39 | 0.42 | 0.58 | 1.36 |
| 1024 | 0.39 | 0.41 | 0.58 | 1.35 |
| 1028 | 0.39 | 0.41 | 0.57 | 1.34 |
| 1032 | 0.39 | 0.40 | 0.56 | 1.32 |
| 1036 | 0.38 | 0.40 | 0.56 | 1.31 |
| 1040 | 0.38 | 0.39 | 0.55 | 1.30 |
| 1044 | 0.38 | 0.39 | 0.54 | 1.28 |
| 1048 | 0.38 | 0.38 | 0.54 | 1.27 |
| 1052 | 0.38 | 0.38 | 0.53 | 1.26 |
| 1056 | 0.38 | 0.37 | 0.53 | 1.25 |
| 1060 | 0.38 | 0.37 | 0.53 | 1.24 |
| 1064 | 0.38 | 0.36 | 0.53 | 1.24 |

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Hydrograph Discharge Table

| Time (min) | Hyd. 11 + (cfs) | Hyd. 12 + (cfs) | Hyd. 13 = (cfs) | Outflow (cfs) |
|---------------|--------------------|--------------------|--------------------|------------------|
| 1068 | 0.38 | 0.36 | 0.53 | 1.23 |
| 1072 | 0.38 | 0.35 | 0.53 | 1.22 |
| 1076 | 0.38 | 0.34 | 0.53 | 1.22 |
| 1080 | 0.38 | 0.34 | 0.53 | 1.21 |
| 1084 | 0.38 | 0.33 | 0.52 | 1.20 |
| 1088 | 0.38 | 0.33 | 0.52 | 1.20 |
| 1092 | 0.38 | 0.33 | 0.52 | 1.19 |
| 1096 | 0.38 | 0.32 | 0.52 | 1.19 |
| 1100 | 0.38 | 0.32 | 0.52 | 1.18 |
| 1104 | 0.38 | 0.31 | 0.52 | 1.18 |
| 1108 | 0.38 | 0.31 | 0.52 | 1.17 |
| 1112 | 0.38 | 0.30 | 0.52 | 1.16 |
| 1116 | 0.37 | 0.30 | 0.52 | 1.16 |
| 1120 | 0.37 | 0.29 | 0.52 | 1.16 |
| 1124 | 0.37 | 0.29 | 0.52 | 1.16 |
| 1128 | 0.37 | 0.29 | 0.52 | 1.15 |
| 1132 | 0.37 | 0.28 | 0.52 | 1.15 |
| 1136 | 0.37 | 0.28 | 0.52 | 1.15 |
| 1140 | 0.37 | 0.28 | 0.52 | 1.15 |
| 1144 | 0.37 | 0.27 | 0.52 | 1.15 |
| 1148 | 0.37 | 0.27 | 0.52 | 1.15 |
| 1152 | 0.37 | 0.27 | 0.51 | 1.14 |
| 1156 | 0.37 | 0.26 | 0.51 | 1.14 |
| 1160 | 0.37 | 0.26 | 0.51 | 1.14 |
| 1164 | 0.37 | 0.26 | 0.51 | 1.14 |
| 1168 | 0.37 | 0.26 | 0.51 | 1.14 |
| 1172 | 0.37 | 0.26 | 0.51 | 1.13 |
| 1176 | 0.37 | 0.26 | 0.51 | 1.13 |
| 1180 | 0.37 | 0.26 | 0.51 | 1.13 |
| 1184 | 0.37 | 0.26 | 0.51 | 1.13 |
| 1188 | 0.36 | 0.26 | 0.51 | 1.13 |
| 1192 | 0.36 | 0.26 | 0.51 | 1.13 |
| 1196 | 0.36 | 0.26 | 0.51 | 1.12 |
| 1200 | 0.36 | 0.26 | 0.51 | 1.12 |
| 1204 | 0.36 | 0.26 | 0.51 | 1.12 |
| 1208 | 0.36 | 0.25 | 0.51 | 1.12 |
| 1212 | 0.36 | 0.25 | 0.50 | 1.12 |
| 1216 | 0.36 | 0.25 | 0.50 | 1.11 |
| 1220 | 0.36 | 0.25 | 0.50 | 1.11 |
| 1224 | 0.36 | 0.25 | 0.50 | 1.11 |
| 1228 | 0.36 | 0.25 | 0.50 | 1.11 |
| 1232 | 0.36 | 0.25 | 0.50 | 1.11 |
| 1236 | 0.36 | 0.25 | 0.50 | 1.10 |
| 1240 | 0.36 | 0.25 | 0.50 | 1.10 |
| 1244 | 0.36 | 0.25 | 0.50 | 1.10 |
| 1248 | 0.36 | 0.25 | 0.50 | 1.10 |
| 1252 | 0.36 | 0.25 | 0.50 | 1.10 |
| 1256 | 0.35 | 0.25 | 0.50 | 1.09 |
| 1260 | 0.35 | 0.25 | 0.50 | 1.09 |
| 1264 | 0.35 | 0.24 | 0.50 | 1.09 |
| 1268 | 0.35 | 0.24 | 0.50 | 1.09 |

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Hydrograph Discharge Table

| Time (min) | Hyd. 11 + (cfs) | Hyd. 12 + (cfs) | Hyd. 13 = (cfs) | Outflow (cfs) |
|---------------|--------------------|--------------------|--------------------|------------------|
| 1272 | 0.35 | 0.24 | 0.49 | 1.09 |
| 1276 | 0.35 | 0.24 | 0.49 | 1.08 |
| 1280 | 0.35 | 0.24 | 0.49 | 1.08 |
| 1284 | 0.35 | 0.24 | 0.49 | 1.08 |
| 1288 | 0.35 | 0.24 | 0.49 | 1.08 |
| 1292 | 0.35 | 0.24 | 0.49 | 1.07 |
| 1296 | 0.35 | 0.24 | 0.49 | 1.07 |
| 1300 | 0.35 | 0.24 | 0.49 | 1.07 |
| 1304 | 0.35 | 0.24 | 0.49 | 1.07 |
| 1308 | 0.35 | 0.24 | 0.49 | 1.07 |
| 1312 | 0.35 | 0.23 | 0.49 | 1.06 |
| 1316 | 0.35 | 0.23 | 0.49 | 1.06 |
| 1320 | 0.34 | 0.23 | 0.49 | 1.06 |
| 1324 | 0.34 | 0.23 | 0.48 | 1.06 |
| 1328 | 0.34 | 0.23 | 0.48 | 1.06 |
| 1332 | 0.34 | 0.23 | 0.48 | 1.05 |
| 1336 | 0.34 | 0.23 | 0.48 | 1.05 |
| 1340 | 0.34 | 0.23 | 0.48 | 1.05 |
| 1344 | 0.34 | 0.23 | 0.48 | 1.05 |
| 1348 | 0.34 | 0.23 | 0.48 | 1.05 |
| 1352 | 0.34 | 0.23 | 0.48 | 1.04 |
| 1356 | 0.34 | 0.23 | 0.48 | 1.04 |
| 1360 | 0.34 | 0.23 | 0.48 | 1.04 |
| 1364 | 0.34 | 0.22 | 0.48 | 1.04 |
| 1368 | 0.34 | 0.22 | 0.48 | 1.03 |
| 1372 | 0.34 | 0.22 | 0.48 | 1.03 |
| 1376 | 0.34 | 0.22 | 0.48 | 1.03 |
| 1380 | 0.34 | 0.22 | 0.47 | 1.03 |
| 1384 | 0.33 | 0.22 | 0.47 | 1.02 |
| 1388 | 0.33 | 0.22 | 0.47 | 1.02 |
| 1392 | 0.33 | 0.22 | 0.47 | 1.02 |
| 1396 | 0.33 | 0.22 | 0.47 | 1.02 |
| 1400 | 0.33 | 0.22 | 0.47 | 1.02 |
| 1404 | 0.33 | 0.22 | 0.47 | 1.01 |
| 1408 | 0.33 | 0.21 | 0.47 | 1.01 |
| 1412 | 0.33 | 0.21 | 0.47 | 1.01 |
| 1416 | 0.33 | 0.21 | 0.47 | 1.01 |
| 1420 | 0.33 | 0.21 | 0.47 | 1.00 |
| 1424 | 0.33 | 0.21 | 0.47 | 1.00 |
| 1428 | 0.33 | 0.21 | 0.46 | 1.00 |
| 1432 | 0.33 | 0.21 | 0.46 | 1.00 |
| 1436 | 0.33 | 0.21 | 0.46 | 0.99 |
| 1440 | 0.32 | 0.21 | 0.46 | 0.99 |
| 1444 | 0.32 | 0.21 | 0.46 | 0.99 |
| 1448 | 0.32 | 0.21 | 0.46 | 0.99 |
| 1452 | 0.32 | 0.20 | 0.46 | 0.98 |
| 1456 | 0.32 | 0.20 | 0.46 | 0.98 |
| 1460 | 0.32 | 0.20 | 0.46 | 0.97 |
| 1464 | 0.32 | 0.20 | 0.46 | 0.97 |
| 1468 | 0.32 | 0.20 | 0.45 | 0.97 |
| 1472 | 0.32 | 0.19 | 0.45 | 0.96 |

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Hydrograph Discharge Table

| Time (min) | Hyd. 11 + (cfs) | Hyd. 12 + (cfs) | Hyd. 13 = (cfs) | Outflow (cfs) |
|---------------|--------------------|--------------------|--------------------|------------------|
| 1476 | 0.32 | 0.19 | 0.45 | 0.96 |
| 1480 | 0.32 | 0.19 | 0.45 | 0.95 |
| 1484 | 0.31 | 0.19 | 0.45 | 0.95 |
| 1488 | 0.31 | 0.18 | 0.45 | 0.94 |
| 1492 | 0.31 | 0.18 | 0.45 | 0.94 |
| 1496 | 0.31 | 0.18 | 0.45 | 0.93 |
| 1500 | 0.31 | 0.18 | 0.44 | 0.93 |
| 1504 | 0.31 | 0.18 | 0.44 | 0.93 |
| 1508 | 0.31 | 0.17 | 0.44 | 0.92 |
| 1512 | 0.31 | 0.17 | 0.44 | 0.92 |
| 1516 | 0.31 | 0.17 | 0.44 | 0.91 |
| 1520 | 0.31 | 0.17 | 0.44 | 0.91 |
| 1524 | 0.30 | 0.17 | 0.44 | 0.90 |
| 1528 | 0.30 | 0.16 | 0.44 | 0.90 |
| 1532 | 0.30 | 0.16 | 0.43 | 0.90 |
| 1536 | 0.30 | 0.16 | 0.43 | 0.89 |
| 1540 | 0.30 | 0.16 | 0.43 | 0.88 |
| 1544 | 0.30 | 0.15 | 0.43 | 0.88 |
| 1548 | 0.30 | 0.15 | 0.43 | 0.87 |
| 1552 | 0.30 | 0.15 | 0.43 | 0.87 |
| 1556 | 0.30 | 0.15 | 0.43 | 0.87 |
| 1560 | 0.30 | 0.14 | 0.43 | 0.86 |
| 1564 | 0.29 | 0.14 | 0.42 | 0.86 |
| 1568 | 0.29 | 0.14 | 0.42 | 0.85 |
| 1572 | 0.29 | 0.14 | 0.42 | 0.85 |
| 1576 | 0.29 | 0.13 | 0.42 | 0.84 |
| 1580 | 0.29 | 0.13 | 0.42 | 0.84 |
| 1584 | 0.29 | 0.13 | 0.42 | 0.83 |
| 1588 | 0.29 | 0.13 | 0.42 | 0.83 |
| 1592 | 0.29 | 0.12 | 0.42 | 0.82 |
| 1596 | 0.29 | 0.12 | 0.41 | 0.82 |
| 1600 | 0.29 | 0.12 | 0.41 | 0.81 |
| 1604 | 0.28 | 0.12 | 0.41 | 0.81 |
| 1608 | 0.28 | 0.12 | 0.41 | 0.81 |
| 1612 | 0.28 | 0.11 | 0.41 | 0.80 |
| 1616 | 0.28 | 0.11 | 0.41 | 0.80 |
| 1620 | 0.28 | 0.11 | 0.41 | 0.79 |
| 1624 | 0.28 | 0.11 | 0.40 | 0.79 |
| 1628 | 0.28 | 0.11 | 0.40 | 0.78 |
| 1632 | 0.28 | 0.10 | 0.40 | 0.78 |
| 1636 | 0.28 | 0.10 | 0.40 | 0.77 |
| 1640 | 0.28 | 0.10 | 0.39 | 0.77 |
| 1644 | 0.27 | 0.10 | 0.39 | 0.76 |
| 1648 | 0.27 | 0.10 | 0.39 | 0.76 |
| 1652 | 0.27 | 0.09 | 0.39 | 0.75 |
| 1656 | 0.27 | 0.09 | 0.39 | 0.75 |
| 1660 | 0.27 | 0.09 | 0.38 | 0.74 |
| 1664 | 0.27 | 0.09 | 0.38 | 0.74 |
| 1668 | 0.27 | 0.09 | 0.38 | 0.73 |
| 1672 | 0.27 | 0.09 | 0.38 | 0.73 |
| 1676 | 0.27 | 0.08 | 0.37 | 0.72 |

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Hydrograph Discharge Table

| Time (min) | Hyd. 11 + (cfs) | Hyd. 12 + (cfs) | Hyd. 13 = (cfs) | Outflow (cfs) |
|-----------------------|----------------------------|----------------------------|----------------------------|--------------------------|
| 1680 | 0.27 | 0.08 | 0.37 | 0.72 |
| 1684 | 0.26 | 0.08 | 0.37 | 0.71 |
| 1688 | 0.26 | 0.08 | 0.37 | 0.71 |
| 1692 | 0.26 | 0.08 | 0.37 | 0.70 |

...End

Hydrograph Summary Report

| Hyd. No. | Hydrograph type (origin) | Peak flow (cfs) | Time interval (min) | Time to peak (min) | Volume (cuft) | Inflow hyd(s) | Maximum elevation (ft) | Maximum storage (cuft) | Hydrograph description |
|--------------------------------------|--------------------------|-----------------|---------------------|--------------------|---------------|---------------|------------------------|------------------------|------------------------|
| 1 | SCS Runoff | 16.30 | 2 | 732 | 68,701 | --- | ---- | ---- | Predevelopment |
| 2 | SCS Runoff | 8.70 | 2 | 728 | 33,969 | --- | ---- | ---- | Post Subarea 1a |
| 3 | SCS Runoff | 0.72 | 2 | 724 | 2,237 | --- | ---- | ---- | Post Subarea 1b |
| 4 | SCS Runoff | 9.96 | 2 | 730 | 41,947 | --- | ---- | ---- | Post Subarea 2a |
| 5 | SCS Runoff | 0.70 | 2 | 724 | 2,157 | --- | ---- | ---- | Post Subarea 2b |
| 6 | SCS Runoff | 15.64 | 2 | 726 | 54,611 | --- | ---- | ---- | Post Subarea 3a |
| 7 | SCS Runoff | 0.91 | 2 | 724 | 2,796 | --- | ---- | ---- | Post Subarea 3b |
| 8 | Combine | 9.25 | 2 | 728 | 36,206 | 2, 3, | --- | ---- | Basin 1 In |
| 9 | Combine | 10.39 | 2 | 730 | 44,104 | 4, 5, | --- | ---- | Basin 2 In |
| 10 | Combine | 16.49 | 2 | 726 | 57,407 | 6, 7, | --- | ---- | Basin 3 In |
| 11 | Reservoir | 0.76 | 2 | 824 | 35,669 | 8 | 243.22 | 32,617 | Basin 1 Out |
| 12 | Reservoir | 4.95 | 2 | 746 | 40,824 | 9 | 233.62 | 18,845 | Basin 2 Out |
| 13 | Reservoir | 3.80 | 2 | 752 | 57,407 | 10 | 225.21 | 25,675 | Basin 3 Out |
| 14 | Combine | 9.95 | 2 | 746 | 133,908 | 11, 12, 13 | ---- | ---- | |
| Proj. file: ansuya.basin.9-30-04.gpw | | | | | | | Return Period: 50 yr | | Run date: 10-08-2004 |

Hydrograph Report

Hyd. No. 1

Predevelopment

| | | | |
|-----------------|--------------|--------------------|-------------|
| Hydrograph type | = SCS Runoff | Peak discharge | = 16.30 cfs |
| Storm frequency | = 50 yrs | Time interval | = 2 min |
| Drainage area | = 8.27 ac | Curve number | = 61 |
| Basin Slope | = 0.0 % | Hydraulic length | = 0 ft |
| Tc method | = USER | Time of conc. (Tc) | = 14.4 min |
| Total precip. | = 6.50 in | Distribution | = Type III |
| Storm duration | = 24 hrs | Shape factor | = 484 |

Hydrograph Volume = 68,701 cuft

Hydrograph Discharge Table

| Time (min) | Outflow (cfs) | Time (min) | Outflow (cfs) | Time (min) | Outflow (cfs) |
|------------|---------------|------------|---------------|------------|---------------|
| 692 | 0.86 | 828 | 1.88 | 964 | 0.94 |
| 696 | 1.03 | 832 | 1.83 | 968 | 0.92 |
| 700 | 1.34 | 836 | 1.79 | 972 | 0.90 |
| 704 | 1.87 | 840 | 1.74 | 976 | 0.89 |
| 708 | 2.62 | 844 | 1.69 | 980 | 0.88 |
| 712 | 3.61 | 848 | 1.65 | 984 | 0.86 |
| 716 | 4.90 | 852 | 1.61 | 988 | 0.85 |
| 720 | 7.26 | 856 | 1.59 | 992 | 0.84 |
| 724 | 11.25 | 860 | 1.56 | 996 | 0.83 |
| 728 | 15.10 | 864 | 1.54 | 1000 | 0.82 |
| 732 | 16.30 << | 868 | 1.52 | | |
| 736 | 15.13 | 872 | 1.49 | | |
| 740 | 13.08 | 876 | 1.47 | ...End | |
| 744 | 10.64 | 880 | 1.45 | | |
| 748 | 8.68 | 884 | 1.43 | | |
| 752 | 7.17 | 888 | 1.40 | | |
| 756 | 5.75 | 892 | 1.38 | | |
| 760 | 4.60 | 896 | 1.36 | | |
| 764 | 3.83 | 900 | 1.33 | | |
| 768 | 3.37 | 904 | 1.31 | | |
| 772 | 3.11 | 908 | 1.29 | | |
| 776 | 2.93 | 912 | 1.26 | | |
| 780 | 2.76 | 916 | 1.24 | | |
| 784 | 2.59 | 920 | 1.22 | | |
| 788 | 2.44 | 924 | 1.19 | | |
| 792 | 2.33 | 928 | 1.17 | | |
| 796 | 2.25 | 932 | 1.14 | | |
| 800 | 2.19 | 936 | 1.12 | | |
| 804 | 2.14 | 940 | 1.09 | | |
| 808 | 2.10 | 944 | 1.07 | | |
| 812 | 2.06 | 948 | 1.04 | | |
| 816 | 2.01 | 952 | 1.02 | | |
| 820 | 1.97 | 956 | 0.99 | | |
| 824 | 1.92 | 960 | 0.97 | | |

Hydrograph Report

Hyd. No. 2

Post Subarea 1a

| | | | |
|-----------------|--------------|--------------------|------------|
| Hydrograph type | = SCS Runoff | Peak discharge | = 8.70 cfs |
| Storm frequency | = 50 yrs | Time interval | = 2 min |
| Drainage area | = 1.90 ac | Curve number | = 85 |
| Basin Slope | = 0.0 % | Hydraulic length | = 0 ft |
| Tc method | = USER | Time of conc. (Tc) | = 10.6 min |
| Total precip. | = 6.50 in | Distribution | = Type III |
| Storm duration | = 24 hrs | Shape factor | = 484 |

Hydrograph Volume = 33,969 cuft

Hydrograph Discharge Table

| Time -- Outflow (min cfs) | Time -- Outflow (min cfs) | Time -- Outflow (min cfs) |
|------------------------------|------------------------------|------------------------------|
| 630 0.44 | 766 1.29 | 902 0.47 |
| 634 0.45 | 770 1.20 | 906 0.46 |
| 638 0.47 | 774 1.13 | 910 0.45 |
| 642 0.49 | 778 1.06 | 914 0.44 |
| 646 0.51 | 782 0.99 | |
| 650 0.53 | 786 0.93 | |
| 654 0.55 | 790 0.88 | ...End |
| 658 0.57 | 794 0.85 | |
| 662 0.59 | 798 0.82 | |
| 666 0.61 | 802 0.80 | |
| 670 0.65 | 806 0.79 | |
| 674 0.70 | 810 0.77 | |
| 678 0.76 | 814 0.75 | |
| 682 0.82 | 818 0.73 | |
| 686 0.89 | 822 0.71 | |
| 690 0.95 | 826 0.69 | |
| 694 1.05 | 830 0.67 | |
| 698 1.26 | 834 0.66 | |
| 702 1.64 | 838 0.64 | |
| 706 2.15 | 842 0.62 | |
| 710 2.75 | 846 0.60 | |
| 714 3.39 | 850 0.59 | |
| 718 4.33 | 854 0.58 | |
| 722 6.27 | 858 0.57 | |
| 726 8.32 | 862 0.56 | |
| 730 8.53 | 866 0.55 | |
| 734 7.30 | 870 0.54 | |
| 738 5.73 | 874 0.53 | |
| 742 4.39 | 878 0.52 | |
| 746 3.58 | 882 0.51 | |
| 750 2.92 | 886 0.50 | |
| 754 2.28 | 890 0.49 | |
| 758 1.77 | 894 0.48 | |
| 762 1.46 | 898 0.48 | |

Hydrograph Report

Hyd. No. 3

Post Subarea 1b

Hydrograph type = SCS Runoff
Storm frequency = 50 yrs
Drainage area = 0.28 ac
Basin Slope = 0.0 %
Tc method = USER
Total precip. = 6.50 in
Storm duration = 24 hrs

Peak discharge = 0.72 cfs
Time interval = 2 min
Curve number = 61
Hydraulic length = 0 ft
Time of conc. (Tc) = 6 min
Distribution = Type III
Shape factor = 484

Hydrograph Volume = 2,237 cuft

Hydrograph Discharge Table

| Time -- Outflow (min cfs) | Time -- Outflow (min cfs) |
|------------------------------|------------------------------|
| 694 0.04 | 830 0.06 |
| 698 0.06 | 834 0.06 |
| 702 0.09 | 838 0.05 |
| 706 0.12 | 842 0.05 |
| 710 0.17 | 846 0.05 |
| 714 0.22 | 850 0.05 |
| 718 0.34 | 854 0.05 |
| 722 0.65 | 858 0.05 |
| 726 0.68 | 862 0.05 |
| 730 0.45 | 866 0.05 |
| 734 0.36 | 870 0.05 |
| 738 0.31 | 874 0.05 |
| 742 0.27 | 878 0.05 |
| 746 0.22 | 882 0.05 |
| 750 0.17 | 886 0.04 |
| 754 0.12 | 890 0.04 |
| 758 0.11 | 894 0.04 |
| 762 0.10 | 898 0.04 |
| 766 0.10 | 902 0.04 |
| 770 0.09 | 906 0.04 |
| 774 0.09 | 910 0.04 |
| 778 0.08 | 914 0.04 |
| 782 0.08 | 918 0.04 |
| 786 0.07 | 922 0.04 |
| 790 0.07 | 926 0.04 |
| 794 0.07 | |
| 798 0.07 | |
| 802 0.07 | ...End |
| 806 0.07 | |
| 810 0.07 | |
| 814 0.06 | |
| 818 0.06 | |
| 822 0.06 | |
| 826 0.06 | |

Hydrograph Report

Hyd. No. 4

Post Subarea 2a

Hydrograph type = SCS Runoff
Storm frequency = 50 yrs
Drainage area = 2.32 ac
Basin Slope = 0.0 %
Tc method = USER
Total precip. = 6.50 in
Storm duration = 24 hrs

Peak discharge = 9.96 cfs
Time interval = 2 min
Curve number = 88
Hydraulic length = 0 ft
Time of conc. (Tc) = 14.5 min
Distribution = Type III
Shape factor = 484

Hydrograph Volume = 41,947 cuft

Hydrograph Discharge Table

| Time -- Outflow (min cfs) | Time -- Outflow (min cfs) | Time -- Outflow (min cfs) |
|------------------------------|------------------------------|------------------------------|
| 616 0.50 | 752 3.49 | 888 0.59 |
| 620 0.52 | 756 2.75 | 892 0.58 |
| 624 0.54 | 760 2.17 | 896 0.57 |
| 628 0.56 | 764 1.79 | 900 0.56 |
| 632 0.59 | 768 1.56 | 904 0.55 |
| 636 0.61 | 772 1.43 | 908 0.54 |
| 640 0.63 | 776 1.35 | 912 0.53 |
| 644 0.65 | 780 1.26 | 916 0.52 |
| 648 0.67 | 784 1.18 | 920 0.51 |
| 652 0.70 | 788 1.10 | |
| 656 0.72 | 792 1.05 | |
| 660 0.74 | 796 1.01 | ...End |
| 664 0.77 | 800 0.98 | |
| 668 0.80 | 804 0.95 | |
| 672 0.85 | 808 0.93 | |
| 676 0.91 | 812 0.91 | |
| 680 0.98 | 816 0.89 | |
| 684 1.06 | 820 0.87 | |
| 688 1.14 | 824 0.84 | |
| 692 1.23 | 828 0.82 | |
| 696 1.37 | 832 0.80 | |
| 700 1.65 | 836 0.78 | |
| 704 2.12 | 840 0.75 | |
| 708 2.74 | 844 0.73 | |
| 712 3.46 | 848 0.71 | |
| 716 4.28 | 852 0.70 | |
| 720 5.67 | 856 0.68 | |
| 724 7.84 | 860 0.67 | |
| 728 9.66 | 864 0.66 | |
| 732 9.78 | 868 0.65 | |
| 736 8.61 | 872 0.64 | |
| 740 7.06 | 876 0.63 | |
| 744 5.47 | 880 0.62 | |
| 748 4.31 | 884 0.61 | |

Hydrograph Report

Hyd. No. 5

Post Subarea 2b

Hydrograph type = SCS Runoff
Storm frequency = 50 yrs
Drainage area = 0.27 ac
Basin Slope = 0.0 %
Tc method = USER
Total precip. = 6.50 in
Storm duration = 24 hrs

Peak discharge = 0.70 cfs
Time interval = 2 min
Curve number = 61
Hydraulic length = 0 ft
Time of conc. (Tc) = 6 min
Distribution = Type III
Shape factor = 484

Hydrograph Volume = 2,157 cuft

Hydrograph Discharge Table

| Time (min) | Outflow (cfs) | Time (min) | Outflow (cfs) |
|------------|---------------|------------|---------------|
| 694 | 0.04 | 830 | 0.06 |
| 698 | 0.06 | 834 | 0.05 |
| 702 | 0.09 | 838 | 0.05 |
| 706 | 0.12 | 842 | 0.05 |
| 710 | 0.16 | 846 | 0.05 |
| 714 | 0.21 | 850 | 0.05 |
| 718 | 0.33 | 854 | 0.05 |
| 722 | 0.62 | 858 | 0.05 |
| 726 | 0.65 | 862 | 0.05 |
| 730 | 0.43 | 866 | 0.05 |
| 734 | 0.34 | 870 | 0.05 |
| 738 | 0.30 | 874 | 0.05 |
| 742 | 0.26 | 878 | 0.04 |
| 746 | 0.21 | 882 | 0.04 |
| 750 | 0.16 | 886 | 0.04 |
| 754 | 0.12 | 890 | 0.04 |
| 758 | 0.11 | 894 | 0.04 |
| 762 | 0.10 | 898 | 0.04 |
| 766 | 0.10 | 902 | 0.04 |
| 770 | 0.09 | 906 | 0.04 |
| 774 | 0.08 | 910 | 0.04 |
| 778 | 0.08 | 914 | 0.04 |
| 782 | 0.07 | 918 | 0.04 |
| 786 | 0.07 | 922 | 0.04 |
| 790 | 0.07 | 926 | 0.04 |
| 794 | 0.07 | | |
| 798 | 0.07 | | |
| 802 | 0.07 | ...End | |
| 806 | 0.06 | | |
| 810 | 0.06 | | |
| 814 | 0.06 | | |
| 818 | 0.06 | | |
| 822 | 0.06 | | |
| 826 | 0.06 | | |

Hydrograph Report

Hyd. No. 6

Post Subarea 3a

Hydrograph type = SCS Runoff
Storm frequency = 50 yrs
Drainage area = 3.15 ac
Basin Slope = 0.0 %
Tc method = USER
Total precip. = 6.50 in
Storm duration = 24 hrs

Peak discharge = 15.64 cfs
Time interval = 2 min
Curve number = 85
Hydraulic length = 0 ft
Time of conc. (Tc) = 7.5 min
Distribution = Type III
Shape factor = 484

Hydrograph Volume = 54,611 cuft

Hydrograph Discharge Table

| Time -- Outflow (min cfs) | Time -- Outflow (min cfs) |
|------------------------------|------------------------------|
| 640 0.79 | 776 1.69 |
| 644 0.82 | 780 1.57 |
| 648 0.85 | 784 1.46 |
| 652 0.88 | 788 1.39 |
| 656 0.92 | 792 1.35 |
| 660 0.95 | 796 1.32 |
| 664 0.99 | 800 1.29 |
| 668 1.05 | 804 1.26 |
| 672 1.14 | 808 1.23 |
| 676 1.23 | 812 1.20 |
| 680 1.34 | 816 1.17 |
| 684 1.44 | 820 1.14 |
| 688 1.55 | 824 1.11 |
| 692 1.67 | 828 1.08 |
| 696 2.00 | 832 1.05 |
| 700 2.67 | 836 1.02 |
| 704 3.57 | 840 0.99 |
| 708 4.57 | 844 0.96 |
| 712 5.62 | 848 0.94 |
| 716 6.87 | 852 0.92 |
| 720 10.06 | 856 0.91 |
| 724 14.77 | 860 0.89 |
| 728 14.97 | 864 0.88 |
| 732 11.34 | 868 0.86 |
| 736 8.16 | 872 0.85 |
| 740 6.65 | 876 0.83 |
| 744 5.59 | 880 0.82 |
| 748 4.52 | 884 0.81 |
| 752 3.45 | 888 0.79 |
| 756 2.62 | |
| 760 2.20 | |
| 764 2.03 | ...End |
| 768 1.91 | |
| 772 1.80 | |

Hydrograph Report

Hyd. No. 7

Post Subarea 3b

Hydrograph type = SCS Runoff
Storm frequency = 50 yrs
Drainage area = 0.35 ac
Basin Slope = 0.0 %
Tc method = USER
Total precip. = 6.50 in
Storm duration = 24 hrs

Peak discharge = 0.91 cfs
Time interval = 2 min
Curve number = 61
Hydraulic length = 0 ft
Time of conc. (Tc) = 6 min
Distribution = Type III
Shape factor = 484

Hydrograph Volume = 2,796 cuft

Hydrograph Discharge Table

| Time -- Outflow (min cfs) | Time -- Outflow (min cfs) |
|------------------------------|------------------------------|
| 694 0.05 | 830 0.07 |
| 698 0.08 | 834 0.07 |
| 702 0.11 | 838 0.07 |
| 706 0.16 | 842 0.07 |
| 710 0.21 | 846 0.06 |
| 714 0.27 | 850 0.06 |
| 718 0.43 | 854 0.06 |
| 722 0.81 | 858 0.06 |
| 726 0.85 | 862 0.06 |
| 730 0.56 | 866 0.06 |
| 734 0.44 | 870 0.06 |
| 738 0.39 | 874 0.06 |
| 742 0.34 | 878 0.06 |
| 746 0.27 | 882 0.06 |
| 750 0.21 | 886 0.06 |
| 754 0.15 | 890 0.05 |
| 758 0.14 | 894 0.05 |
| 762 0.13 | 898 0.05 |
| 766 0.12 | 902 0.05 |
| 770 0.12 | 906 0.05 |
| 774 0.11 | 910 0.05 |
| 778 0.10 | 914 0.05 |
| 782 0.10 | 918 0.05 |
| 786 0.09 | 922 0.05 |
| 790 0.09 | 926 0.05 |
| 794 0.09 | |
| 798 0.09 | |
| 802 0.08 | ...End |
| 806 0.08 | |
| 810 0.08 | |
| 814 0.08 | |
| 818 0.08 | |
| 822 0.08 | |
| 826 0.07 | |

Hydrograph Report

Hyd. No. 8

Basin 1 In

Hydrograph type = Combine
Storm frequency = 50 yrs
Inflow hyds. = 2, 3

Peak discharge = 9.25 cfs
Time interval = 2 min

Hydrograph Volume = 36,206 cuft

Hydrograph Discharge Table

| Time (min) | Hyd. 2 + (cfs) | Hyd. 3 + (cfs) | Outflow (cfs) |
|------------|----------------|----------------|---------------|
| 636 | 0.46 | 0.00 | 0.47 |
| 640 | 0.48 | 0.01 | 0.49 |
| 644 | 0.50 | 0.01 | 0.51 |
| 648 | 0.52 | 0.01 | 0.53 |
| 652 | 0.54 | 0.01 | 0.55 |
| 656 | 0.56 | 0.01 | 0.57 |
| 660 | 0.58 | 0.01 | 0.59 |
| 664 | 0.60 | 0.01 | 0.61 |
| 668 | 0.63 | 0.02 | 0.64 |
| 672 | 0.67 | 0.02 | 0.69 |
| 676 | 0.73 | 0.02 | 0.75 |
| 680 | 0.79 | 0.02 | 0.81 |
| 684 | 0.85 | 0.03 | 0.88 |
| 688 | 0.92 | 0.03 | 0.95 |
| 692 | 0.99 | 0.04 | 1.03 |
| 696 | 1.13 | 0.05 | 1.18 |
| 700 | 1.43 | 0.08 | 1.50 |
| 704 | 1.88 | 0.11 | 1.98 |
| 708 | 2.44 | 0.14 | 2.58 |
| 712 | 3.07 | 0.19 | 3.26 |
| 716 | 3.78 | 0.26 | 4.04 |
| 720 | 5.17 | 0.49 | 5.65 |
| 724 | 7.42 | 0.72 << | 8.15 |
| 728 | 8.70 << | 0.56 | 9.25 << |
| 732 | 8.00 | 0.39 | 8.39 |
| 736 | 6.53 | 0.34 | 6.86 |
| 740 | 5.00 | 0.29 | 5.29 |
| 744 | 3.94 | 0.24 | 4.19 |
| 748 | 3.25 | 0.19 | 3.45 |
| 752 | 2.59 | 0.14 | 2.73 |
| 756 | 2.00 | 0.11 | 2.12 |
| 760 | 1.60 | 0.11 | 1.70 |
| 764 | 1.36 | 0.10 | 1.47 |
| 768 | 1.24 | 0.10 | 1.34 |
| 772 | 1.17 | 0.09 | 1.26 |
| 776 | 1.10 | 0.09 | 1.18 |
| 780 | 1.02 | 0.08 | 1.10 |
| 784 | 0.96 | 0.07 | 1.03 |

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Hydrograph Discharge Table

| Time (min) | Hyd. 2 + (cfs) | Hyd. 3 + (cfs) | Outflow (cfs) |
|-----------------------|---------------------------|---------------------------|--------------------------|
| 788 | 0.90 | 0.07 | 0.97 |
| 792 | 0.86 | 0.07 | 0.93 |
| 796 | 0.83 | 0.07 | 0.90 |
| 800 | 0.81 | 0.07 | 0.88 |
| 804 | 0.79 | 0.07 | 0.86 |
| 808 | 0.78 | 0.07 | 0.84 |
| 812 | 0.76 | 0.06 | 0.82 |
| 816 | 0.74 | 0.06 | 0.80 |
| 820 | 0.72 | 0.06 | 0.78 |
| 824 | 0.70 | 0.06 | 0.76 |
| 828 | 0.68 | 0.06 | 0.74 |
| 832 | 0.67 | 0.06 | 0.72 |
| 836 | 0.65 | 0.06 | 0.70 |
| 840 | 0.63 | 0.05 | 0.68 |
| 844 | 0.61 | 0.05 | 0.66 |
| 848 | 0.59 | 0.05 | 0.65 |
| 852 | 0.58 | 0.05 | 0.63 |
| 856 | 0.57 | 0.05 | 0.62 |
| 860 | 0.56 | 0.05 | 0.61 |
| 864 | 0.55 | 0.05 | 0.60 |
| 868 | 0.54 | 0.05 | 0.59 |
| 872 | 0.53 | 0.05 | 0.58 |
| 876 | 0.53 | 0.05 | 0.57 |
| 880 | 0.52 | 0.05 | 0.56 |
| 884 | 0.51 | 0.05 | 0.55 |
| 888 | 0.50 | 0.04 | 0.54 |
| 892 | 0.49 | 0.04 | 0.53 |
| 896 | 0.48 | 0.04 | 0.52 |
| 900 | 0.47 | 0.04 | 0.51 |
| 904 | 0.46 | 0.04 | 0.50 |
| 908 | 0.45 | 0.04 | 0.49 |
| 912 | 0.44 | 0.04 | 0.48 |
| 916 | 0.43 | 0.04 | 0.47 |
| 920 | 0.43 | 0.04 | 0.46 |

...End

Hydrograph Report

Hyd. No. 9

Basin 2 In

Hydrograph type = Combine
Storm frequency = 50 yrs
Inflow hyds. = 4, 5

Peak discharge = 10.39 cfs
Time interval = 2 min

Hydrograph Volume = 44,104 cuft

Hydrograph Discharge Table

| Time (min) | Hyd. 4 + (cfs) | Hyd. 5 + (cfs) | Outflow (cfs) |
|------------|----------------|----------------|---------------|
| 620 | 0.52 | 0.00 | 0.52 |
| 624 | 0.54 | 0.00 | 0.54 |
| 628 | 0.56 | 0.00 | 0.57 |
| 632 | 0.59 | 0.00 | 0.59 |
| 636 | 0.61 | 0.00 | 0.61 |
| 640 | 0.63 | 0.01 | 0.63 |
| 644 | 0.65 | 0.01 | 0.66 |
| 648 | 0.67 | 0.01 | 0.68 |
| 652 | 0.70 | 0.01 | 0.71 |
| 656 | 0.72 | 0.01 | 0.73 |
| 660 | 0.74 | 0.01 | 0.76 |
| 664 | 0.77 | 0.01 | 0.78 |
| 668 | 0.80 | 0.01 | 0.82 |
| 672 | 0.85 | 0.02 | 0.87 |
| 676 | 0.91 | 0.02 | 0.93 |
| 680 | 0.98 | 0.02 | 1.01 |
| 684 | 1.06 | 0.03 | 1.09 |
| 688 | 1.14 | 0.03 | 1.17 |
| 692 | 1.23 | 0.03 | 1.26 |
| 696 | 1.37 | 0.05 | 1.42 |
| 700 | 1.65 | 0.07 | 1.73 |
| 704 | 2.12 | 0.10 | 2.22 |
| 708 | 2.74 | 0.14 | 2.88 |
| 712 | 3.46 | 0.18 | 3.64 |
| 716 | 4.28 | 0.25 | 4.53 |
| 720 | 5.67 | 0.47 | 6.14 |
| 724 | 7.84 | 0.70 << | 8.53 |
| 728 | 9.66 | 0.54 | 10.20 |
| 732 | 9.78 | 0.37 | 10.15 |
| 736 | 8.61 | 0.32 | 8.93 |
| 740 | 7.06 | 0.28 | 7.34 |
| 744 | 5.47 | 0.24 | 5.70 |
| 748 | 4.31 | 0.19 | 4.50 |
| 752 | 3.49 | 0.14 | 3.63 |
| 756 | 2.75 | 0.11 | 2.87 |
| 760 | 2.17 | 0.10 | 2.28 |
| 764 | 1.79 | 0.10 | 1.89 |
| 768 | 1.56 | 0.09 | 1.66 |

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Hydrograph Discharge Table

| Time (min) | Hyd. 4 + (cfs) | Hyd. 5 + (cfs) | Outflow (cfs) |
|-----------------------|---------------------------|---------------------------|--------------------------|
| 772 | 1.43 | 0.09 | 1.52 |
| 776 | 1.35 | 0.08 | 1.43 |
| 780 | 1.26 | 0.08 | 1.34 |
| 784 | 1.18 | 0.07 | 1.25 |
| 788 | 1.10 | 0.07 | 1.17 |
| 792 | 1.05 | 0.07 | 1.12 |
| 796 | 1.01 | 0.07 | 1.08 |
| 800 | 0.98 | 0.07 | 1.04 |
| 804 | 0.95 | 0.06 | 1.02 |
| 808 | 0.93 | 0.06 | 1.00 |
| 812 | 0.91 | 0.06 | 0.97 |
| 816 | 0.89 | 0.06 | 0.95 |
| 820 | 0.87 | 0.06 | 0.93 |
| 824 | 0.84 | 0.06 | 0.90 |
| 828 | 0.82 | 0.06 | 0.88 |
| 832 | 0.80 | 0.05 | 0.85 |
| 836 | 0.78 | 0.05 | 0.83 |
| 840 | 0.75 | 0.05 | 0.81 |
| 844 | 0.73 | 0.05 | 0.78 |
| 848 | 0.71 | 0.05 | 0.76 |
| 852 | 0.70 | 0.05 | 0.74 |
| 856 | 0.68 | 0.05 | 0.73 |
| 860 | 0.67 | 0.05 | 0.72 |
| 864 | 0.66 | 0.05 | 0.71 |
| 868 | 0.65 | 0.05 | 0.69 |
| 872 | 0.64 | 0.05 | 0.68 |
| 876 | 0.63 | 0.04 | 0.67 |
| 880 | 0.62 | 0.04 | 0.66 |
| 884 | 0.61 | 0.04 | 0.65 |
| 888 | 0.59 | 0.04 | 0.64 |
| 892 | 0.58 | 0.04 | 0.63 |
| 896 | 0.57 | 0.04 | 0.61 |
| 900 | 0.56 | 0.04 | 0.60 |
| 904 | 0.55 | 0.04 | 0.59 |
| 908 | 0.54 | 0.04 | 0.58 |
| 912 | 0.53 | 0.04 | 0.57 |
| 916 | 0.52 | 0.04 | 0.56 |
| 920 | 0.51 | 0.04 | 0.55 |
| 924 | 0.50 | 0.04 | 0.53 |
| 928 | 0.49 | 0.04 | 0.52 |

...End

Hydrograph Report

Hyd. No. 10

Basin 3 In

Hydrograph type = Combine
Storm frequency = 50 yrs
Inflow hyds. = 6, 7

Peak discharge = 16.49 cfs
Time interval = 2 min

Hydrograph Volume = 57,407 cuft

Hydrograph Discharge Table

| Time (min) | Hyd. 6 + (cfs) | Hyd. 7 + (cfs) | Outflow (cfs) |
|------------|----------------|----------------|---------------|
| 644 | 0.82 | 0.01 | 0.83 |
| 648 | 0.85 | 0.01 | 0.86 |
| 652 | 0.88 | 0.01 | 0.90 |
| 656 | 0.92 | 0.01 | 0.93 |
| 660 | 0.95 | 0.01 | 0.96 |
| 664 | 0.99 | 0.02 | 1.00 |
| 668 | 1.05 | 0.02 | 1.07 |
| 672 | 1.14 | 0.02 | 1.16 |
| 676 | 1.23 | 0.03 | 1.26 |
| 680 | 1.34 | 0.03 | 1.37 |
| 684 | 1.44 | 0.03 | 1.47 |
| 688 | 1.55 | 0.04 | 1.58 |
| 692 | 1.67 | 0.04 | 1.72 |
| 696 | 2.00 | 0.06 | 2.06 |
| 700 | 2.67 | 0.09 | 2.76 |
| 704 | 3.57 | 0.13 | 3.71 |
| 708 | 4.57 | 0.18 | 4.75 |
| 712 | 5.62 | 0.24 | 5.86 |
| 716 | 6.87 | 0.32 | 7.19 |
| 720 | 10.06 | 0.61 | 10.67 |
| 724 | 14.77 | 0.91 << | 15.68 |
| 728 | 14.97 | 0.70 | 15.67 |
| 732 | 11.34 | 0.48 | 11.82 |
| 736 | 8.16 | 0.42 | 8.58 |
| 740 | 6.65 | 0.37 | 7.01 |
| 744 | 5.59 | 0.31 | 5.90 |
| 748 | 4.52 | 0.24 | 4.76 |
| 752 | 3.45 | 0.18 | 3.63 |
| 756 | 2.62 | 0.14 | 2.76 |
| 760 | 2.20 | 0.13 | 2.34 |
| 764 | 2.03 | 0.13 | 2.15 |
| 768 | 1.91 | 0.12 | 2.03 |
| 772 | 1.80 | 0.11 | 1.91 |
| 776 | 1.69 | 0.11 | 1.79 |
| 780 | 1.57 | 0.10 | 1.67 |
| 784 | 1.46 | 0.09 | 1.56 |
| 788 | 1.39 | 0.09 | 1.48 |
| 792 | 1.35 | 0.09 | 1.44 |

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Hydrograph Discharge Table

| Time (min) | Hyd. 6 + (cfs) | Hyd. 7 + (cfs) | Outflow (cfs) |
|-----------------------|---------------------------|---------------------------|--------------------------|
| 796 | 1.32 | 0.09 | 1.40 |
| 800 | 1.29 | 0.09 | 1.37 |
| 804 | 1.26 | 0.08 | 1.34 |
| 808 | 1.23 | 0.08 | 1.31 |
| 812 | 1.20 | 0.08 | 1.28 |
| 816 | 1.17 | 0.08 | 1.25 |
| 820 | 1.14 | 0.08 | 1.22 |
| 824 | 1.11 | 0.07 | 1.18 |
| 828 | 1.08 | 0.07 | 1.15 |
| 832 | 1.05 | 0.07 | 1.12 |
| 836 | 1.02 | 0.07 | 1.09 |
| 840 | 0.99 | 0.07 | 1.06 |
| 844 | 0.96 | 0.07 | 1.03 |
| 848 | 0.94 | 0.06 | 1.00 |
| 852 | 0.92 | 0.06 | 0.98 |
| 856 | 0.91 | 0.06 | 0.97 |
| 860 | 0.89 | 0.06 | 0.95 |
| 864 | 0.88 | 0.06 | 0.94 |
| 868 | 0.86 | 0.06 | 0.92 |
| 872 | 0.85 | 0.06 | 0.91 |
| 876 | 0.83 | 0.06 | 0.89 |
| 880 | 0.82 | 0.06 | 0.88 |
| 884 | 0.81 | 0.06 | 0.86 |
| 888 | 0.79 | 0.06 | 0.85 |
| 892 | 0.78 | 0.05 | 0.83 |

...End

Hydrograph Report

Hyd. No. 11

Basin 1 Out

Hydrograph type = Reservoir
Storm frequency = 50 yrs
Inflow hyd. No. = 8
Max. Elevation = 243.22 ft

Peak discharge = 0.76 cfs
Time interval = 2 min
Reservoir name = Retention Basin N
Max. Storage = 32,617 cuft

Storage Indication method used.

Outflow hydrograph volume = 35,669 cuft

Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 540 | 0.19 | 240.12 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 544 | 0.20 | 240.13 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 548 | 0.21 | 240.13 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 552 | 0.22 | 240.14 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 556 | 0.23 | 240.14 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 560 | 0.23 | 240.15 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 564 | 0.24 | 240.16 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 568 | 0.25 | 240.16 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 572 | 0.26 | 240.17 | 23.09 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |
| 576 | 0.27 | 240.18 | 23.09 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |
| 580 | 0.28 | 240.19 | 23.09 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |
| 584 | 0.29 | 240.19 | 23.09 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |
| 588 | 0.30 | 240.20 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 592 | 0.31 | 240.21 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 596 | 0.32 | 240.22 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 600 | 0.33 | 240.23 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 604 | 0.34 | 240.24 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 608 | 0.35 | 240.25 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 612 | 0.36 | 240.26 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 616 | 0.38 | 240.27 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 620 | 0.39 | 240.28 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 624 | 0.41 | 240.29 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 628 | 0.43 | 240.30 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 632 | 0.45 | 240.31 | 23.09 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 636 | 0.47 | 240.33 | 23.09 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 640 | 0.49 | 240.34 | 23.09 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.11 |
| 644 | 0.51 | 240.35 | 23.09 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.11 |
| 648 | 0.53 | 240.37 | 23.09 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.11 |
| 652 | 0.55 | 240.38 | 23.09 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.12 |
| 656 | 0.57 | 240.40 | 23.09 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.12 |
| 660 | 0.59 | 240.42 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 664 | 0.61 | 240.43 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 668 | 0.64 | 240.45 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 672 | 0.69 | 240.47 | 23.09 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 676 | 0.75 | 240.49 | 23.09 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 680 | 0.81 | 240.51 | 23.09 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 684 | 0.88 | 240.54 | 23.09 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 688 | 0.95 | 240.57 | 23.09 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |

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Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 692 | 1.03 | 240.59 | 23.09 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |
| 696 | 1.18 | 240.63 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 700 | 1.50 | 240.67 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 704 | 1.98 | 240.73 | 23.09 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 708 | 2.58 | 240.80 | 23.09 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 712 | 3.26 | 240.90 | 23.09 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 716 | 4.04 | 241.02 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 720 | 5.65 | 241.18 | 23.09 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 724 | 8.15 | 241.42 | 23.09 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 728 | 9.25 << | 241.73 | 23.09 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 732 | 8.39 | 242.04 | 23.09 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 736 | 6.86 | 242.30 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 740 | 5.29 | 242.51 | 23.09 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 744 | 4.19 | 242.66 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 748 | 3.45 | 242.79 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 752 | 2.73 | 242.88 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 756 | 2.12 | 242.95 | 23.09 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 760 | 1.70 | 243.01 | 23.09 | 0.40 | ---- | ---- | 0.01 | ---- | ---- | ---- | ---- | 0.41 |
| 764 | 1.47 | 243.05 | 23.09 | 0.40 | ---- | ---- | 0.07 | ---- | ---- | ---- | ---- | 0.48 |
| 768 | 1.34 | 243.08 | 23.09 | 0.41 | ---- | ---- | 0.12 | ---- | ---- | ---- | ---- | 0.53 |
| 772 | 1.26 | 243.11 | 23.09 | 0.41 | ---- | ---- | 0.16 | ---- | ---- | ---- | ---- | 0.57 |
| 776 | 1.18 | 243.13 | 23.09 | 0.41 | ---- | ---- | 0.19 | ---- | ---- | ---- | ---- | 0.60 |
| 780 | 1.10 | 243.15 | 23.09 | 0.41 | ---- | ---- | 0.22 | ---- | ---- | ---- | ---- | 0.63 |
| 784 | 1.03 | 243.16 | 23.09 | 0.41 | ---- | ---- | 0.25 | ---- | ---- | ---- | ---- | 0.66 |
| 788 | 0.97 | 243.18 | 23.09 | 0.41 | ---- | ---- | 0.26 | ---- | ---- | ---- | ---- | 0.68 |
| 792 | 0.93 | 243.19 | 23.09 | 0.41 | ---- | ---- | 0.28 | ---- | ---- | ---- | ---- | 0.69 |
| 796 | 0.90 | 243.19 | 23.09 | 0.41 | ---- | ---- | 0.29 | ---- | ---- | ---- | ---- | 0.70 |
| 800 | 0.88 | 243.20 | 23.09 | 0.41 | ---- | ---- | 0.30 | ---- | ---- | ---- | ---- | 0.71 |
| 804 | 0.86 | 243.21 | 23.09 | 0.41 | ---- | ---- | 0.31 | ---- | ---- | ---- | ---- | 0.73 |
| 808 | 0.84 | 243.21 | 23.09 | 0.42 | ---- | ---- | 0.33 | ---- | ---- | ---- | ---- | 0.74 |
| 812 | 0.82 | 243.21 | 23.09 | 0.42 | ---- | ---- | 0.33 | ---- | ---- | ---- | ---- | 0.75 |
| 816 | 0.80 | 243.22 | 23.09 | 0.42 | ---- | ---- | 0.34 | ---- | ---- | ---- | ---- | 0.76 |
| 820 | 0.78 | 243.22 | 23.09 | 0.42 | ---- | ---- | 0.34 | ---- | ---- | ---- | ---- | 0.76 |
| 824 | 0.76 | 243.22 << | 23.09 | 0.42 | ---- | ---- | 0.35 | ---- | ---- | ---- | ---- | 0.76 << |
| 828 | 0.74 | 243.22 | 23.09 | 0.42 | ---- | ---- | 0.34 | ---- | ---- | ---- | ---- | 0.76 |
| 832 | 0.72 | 243.22 | 23.09 | 0.42 | ---- | ---- | 0.34 | ---- | ---- | ---- | ---- | 0.76 |
| 836 | 0.70 | 243.21 | 23.09 | 0.42 | ---- | ---- | 0.34 | ---- | ---- | ---- | ---- | 0.75 |
| 840 | 0.68 | 243.21 | 23.09 | 0.42 | ---- | ---- | 0.33 | ---- | ---- | ---- | ---- | 0.75 |
| 844 | 0.66 | 243.21 | 23.09 | 0.42 | ---- | ---- | 0.32 | ---- | ---- | ---- | ---- | 0.74 |
| 848 | 0.65 | 243.21 | 23.09 | 0.41 | ---- | ---- | 0.32 | ---- | ---- | ---- | ---- | 0.73 |
| 852 | 0.63 | 243.20 | 23.09 | 0.41 | ---- | ---- | 0.31 | ---- | ---- | ---- | ---- | 0.72 |
| 856 | 0.62 | 243.20 | 23.09 | 0.41 | ---- | ---- | 0.30 | ---- | ---- | ---- | ---- | 0.71 |
| 860 | 0.61 | 243.20 | 23.09 | 0.41 | ---- | ---- | 0.29 | ---- | ---- | ---- | ---- | 0.71 |
| 864 | 0.60 | 243.19 | 23.09 | 0.41 | ---- | ---- | 0.29 | ---- | ---- | ---- | ---- | 0.70 |
| 868 | 0.59 | 243.19 | 23.09 | 0.41 | ---- | ---- | 0.28 | ---- | ---- | ---- | ---- | 0.70 |
| 872 | 0.58 | 243.19 | 23.09 | 0.41 | ---- | ---- | 0.28 | ---- | ---- | ---- | ---- | 0.69 |
| 876 | 0.57 | 243.18 | 23.09 | 0.41 | ---- | ---- | 0.27 | ---- | ---- | ---- | ---- | 0.68 |
| 880 | 0.56 | 243.18 | 23.09 | 0.41 | ---- | ---- | 0.26 | ---- | ---- | ---- | ---- | 0.68 |
| 884 | 0.55 | 243.17 | 23.09 | 0.41 | ---- | ---- | 0.26 | ---- | ---- | ---- | ---- | 0.67 |
| 888 | 0.54 | 243.17 | 23.09 | 0.41 | ---- | ---- | 0.25 | ---- | ---- | ---- | ---- | 0.66 |
| 892 | 0.53 | 243.16 | 23.09 | 0.41 | ---- | ---- | 0.25 | ---- | ---- | ---- | ---- | 0.66 |

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Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 896 | 0.52 | 243.16 | 23.09 | 0.41 | ---- | ---- | 0.24 | ---- | ---- | ---- | ---- | 0.65 |
| 900 | 0.51 | 243.16 | 23.09 | 0.41 | ---- | ---- | 0.23 | ---- | ---- | ---- | ---- | 0.64 |
| 904 | 0.50 | 243.15 | 23.09 | 0.41 | ---- | ---- | 0.22 | ---- | ---- | ---- | ---- | 0.64 |
| 908 | 0.49 | 243.15 | 23.09 | 0.41 | ---- | ---- | 0.22 | ---- | ---- | ---- | ---- | 0.63 |
| 912 | 0.48 | 243.14 | 23.09 | 0.41 | ---- | ---- | 0.21 | ---- | ---- | ---- | ---- | 0.62 |
| 916 | 0.47 | 243.14 | 23.09 | 0.41 | ---- | ---- | 0.20 | ---- | ---- | ---- | ---- | 0.61 |
| 920 | 0.46 | 243.13 | 23.09 | 0.41 | ---- | ---- | 0.20 | ---- | ---- | ---- | ---- | 0.61 |
| 924 | 0.45 | 243.13 | 23.09 | 0.41 | ---- | ---- | 0.19 | ---- | ---- | ---- | ---- | 0.60 |
| 928 | 0.44 | 243.12 | 23.09 | 0.41 | ---- | ---- | 0.18 | ---- | ---- | ---- | ---- | 0.59 |
| 932 | 0.43 | 243.12 | 23.09 | 0.41 | ---- | ---- | 0.17 | ---- | ---- | ---- | ---- | 0.58 |
| 936 | 0.42 | 243.11 | 23.09 | 0.41 | ---- | ---- | 0.16 | ---- | ---- | ---- | ---- | 0.57 |
| 940 | 0.41 | 243.11 | 23.09 | 0.41 | ---- | ---- | 0.16 | ---- | ---- | ---- | ---- | 0.56 |
| 944 | 0.40 | 243.10 | 23.09 | 0.41 | ---- | ---- | 0.15 | ---- | ---- | ---- | ---- | 0.56 |
| 948 | 0.39 | 243.09 | 23.09 | 0.41 | ---- | ---- | 0.14 | ---- | ---- | ---- | ---- | 0.55 |
| 952 | 0.38 | 243.09 | 23.09 | 0.41 | ---- | ---- | 0.13 | ---- | ---- | ---- | ---- | 0.54 |
| 956 | 0.37 | 243.08 | 23.09 | 0.41 | ---- | ---- | 0.12 | ---- | ---- | ---- | ---- | 0.53 |
| 960 | 0.36 | 243.08 | 23.09 | 0.41 | ---- | ---- | 0.12 | ---- | ---- | ---- | ---- | 0.52 |
| 964 | 0.35 | 243.07 | 23.09 | 0.41 | ---- | ---- | 0.11 | ---- | ---- | ---- | ---- | 0.51 |
| 968 | 0.35 | 243.07 | 23.09 | 0.41 | ---- | ---- | 0.10 | ---- | ---- | ---- | ---- | 0.50 |
| 972 | 0.34 | 243.06 | 23.09 | 0.40 | ---- | ---- | 0.09 | ---- | ---- | ---- | ---- | 0.49 |
| 976 | 0.34 | 243.06 | 23.09 | 0.40 | ---- | ---- | 0.08 | ---- | ---- | ---- | ---- | 0.49 |
| 980 | 0.33 | 243.05 | 23.09 | 0.40 | ---- | ---- | 0.07 | ---- | ---- | ---- | ---- | 0.48 |
| 984 | 0.33 | 243.04 | 23.09 | 0.40 | ---- | ---- | 0.07 | ---- | ---- | ---- | ---- | 0.47 |
| 988 | 0.32 | 243.04 | 23.09 | 0.40 | ---- | ---- | 0.06 | ---- | ---- | ---- | ---- | 0.46 |
| 992 | 0.32 | 243.03 | 23.09 | 0.40 | ---- | ---- | 0.05 | ---- | ---- | ---- | ---- | 0.45 |
| 996 | 0.31 | 243.03 | 23.09 | 0.40 | ---- | ---- | 0.04 | ---- | ---- | ---- | ---- | 0.45 |
| 1000 | 0.31 | 243.02 | 23.09 | 0.40 | ---- | ---- | 0.04 | ---- | ---- | ---- | ---- | 0.44 |
| 1004 | 0.30 | 243.02 | 23.09 | 0.40 | ---- | ---- | 0.03 | ---- | ---- | ---- | ---- | 0.43 |
| 1008 | 0.30 | 243.02 | 23.09 | 0.40 | ---- | ---- | 0.02 | ---- | ---- | ---- | ---- | 0.43 |
| 1012 | 0.30 | 243.01 | 23.09 | 0.40 | ---- | ---- | 0.02 | ---- | ---- | ---- | ---- | 0.42 |
| 1016 | 0.29 | 243.01 | 23.09 | 0.40 | ---- | ---- | 0.01 | ---- | ---- | ---- | ---- | 0.41 |
| 1020 | 0.29 | 243.00 | 23.09 | 0.40 | ---- | ---- | 0.00 | ---- | ---- | ---- | ---- | 0.40 |
| 1024 | 0.28 | 243.00 | 23.09 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 1028 | 0.28 | 242.99 | 23.09 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 1032 | 0.27 | 242.99 | 23.09 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 1036 | 0.27 | 242.99 | 23.09 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 1040 | 0.27 | 242.98 | 23.09 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 1044 | 0.26 | 242.98 | 23.09 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 1048 | 0.26 | 242.97 | 23.09 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 1052 | 0.25 | 242.97 | 23.09 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 1056 | 0.25 | 242.96 | 23.09 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 1060 | 0.24 | 242.95 | 23.09 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 1064 | 0.24 | 242.95 | 23.09 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 1068 | 0.23 | 242.94 | 23.09 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 1072 | 0.23 | 242.94 | 23.09 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 1076 | 0.23 | 242.93 | 23.09 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 1080 | 0.22 | 242.93 | 23.09 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 1084 | 0.22 | 242.92 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1088 | 0.21 | 242.91 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1092 | 0.21 | 242.91 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1096 | 0.21 | 242.90 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |

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Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 1100 | 0.21 | 242.89 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1104 | 0.21 | 242.89 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1108 | 0.21 | 242.88 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1112 | 0.20 | 242.87 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1116 | 0.20 | 242.87 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1120 | 0.20 | 242.86 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1124 | 0.20 | 242.85 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1128 | 0.20 | 242.85 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1132 | 0.20 | 242.84 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1136 | 0.20 | 242.83 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1140 | 0.20 | 242.82 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1144 | 0.19 | 242.82 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1148 | 0.19 | 242.81 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1152 | 0.19 | 242.80 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1156 | 0.19 | 242.80 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1160 | 0.19 | 242.79 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1164 | 0.19 | 242.78 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1168 | 0.19 | 242.78 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1172 | 0.19 | 242.77 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1176 | 0.18 | 242.76 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1180 | 0.18 | 242.75 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1184 | 0.18 | 242.75 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1188 | 0.18 | 242.74 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1192 | 0.18 | 242.73 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1196 | 0.18 | 242.73 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1200 | 0.18 | 242.72 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1204 | 0.17 | 242.71 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1208 | 0.17 | 242.70 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1212 | 0.17 | 242.70 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1216 | 0.17 | 242.69 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1220 | 0.17 | 242.68 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1224 | 0.17 | 242.67 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1228 | 0.17 | 242.67 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1232 | 0.17 | 242.66 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1236 | 0.16 | 242.65 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1240 | 0.16 | 242.64 | 23.09 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1244 | 0.16 | 242.64 | 23.09 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1248 | 0.16 | 242.63 | 23.09 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1252 | 0.16 | 242.62 | 23.09 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1256 | 0.16 | 242.61 | 23.09 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1260 | 0.16 | 242.60 | 23.09 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1264 | 0.16 | 242.60 | 23.09 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1268 | 0.15 | 242.59 | 23.09 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1272 | 0.15 | 242.58 | 23.09 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1276 | 0.15 | 242.57 | 23.09 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1280 | 0.15 | 242.57 | 23.09 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1284 | 0.15 | 242.56 | 23.09 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1288 | 0.15 | 242.55 | 23.09 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1292 | 0.15 | 242.54 | 23.09 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1296 | 0.14 | 242.53 | 23.09 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1300 | 0.14 | 242.53 | 23.09 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |

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Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 1304 | 0.14 | 242.52 | 23.09 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1308 | 0.14 | 242.51 | 23.09 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1312 | 0.14 | 242.50 | 23.09 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1316 | 0.14 | 242.49 | 23.09 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1320 | 0.14 | 242.49 | 23.09 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1324 | 0.17 | 242.48 | 23.09 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1328 | 0.19 | 242.47 | 23.09 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1332 | 0.18 | 242.47 | 23.09 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1336 | 0.16 | 242.46 | 23.09 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1340 | 0.15 | 242.45 | 23.09 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1344 | 0.14 | 242.44 | 23.09 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1348 | 0.14 | 242.44 | 23.09 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1352 | 0.14 | 242.43 | 23.09 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1356 | 0.14 | 242.42 | 23.09 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1360 | 0.14 | 242.41 | 23.09 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1364 | 0.13 | 242.40 | 23.09 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1368 | 0.13 | 242.40 | 23.09 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1372 | 0.13 | 242.39 | 23.09 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1376 | 0.13 | 242.38 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1380 | 0.13 | 242.37 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1384 | 0.13 | 242.36 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1388 | 0.13 | 242.36 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1392 | 0.13 | 242.35 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1396 | 0.13 | 242.34 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1400 | 0.13 | 242.33 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1404 | 0.13 | 242.32 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1408 | 0.12 | 242.31 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1412 | 0.12 | 242.31 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1416 | 0.12 | 242.30 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1420 | 0.12 | 242.29 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1424 | 0.12 | 242.28 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1428 | 0.12 | 242.27 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1432 | 0.12 | 242.27 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1436 | 0.12 | 242.26 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1440 | 0.12 | 242.25 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1444 | 0.09 | 242.24 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1448 | 0.06 | 242.23 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1452 | 0.03 | 242.22 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1456 | 0.01 | 242.21 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1460 | 0.00 | 242.20 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1464 | 0.00 | 242.18 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1468 | 0.00 | 242.17 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1472 | 0.00 | 242.16 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1476 | 0.00 | 242.15 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1480 | 0.00 | 242.14 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1484 | 0.00 | 242.12 | 23.09 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1488 | 0.00 | 242.11 | 23.09 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1492 | 0.00 | 242.10 | 23.09 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1496 | 0.00 | 242.09 | 23.09 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1500 | 0.00 | 242.08 | 23.09 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1504 | 0.00 | 242.06 | 23.09 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |

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Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Civ A cfs | Civ B cfs | Civ C cfs | Civ D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 1508 | 0.00 | 242.05 | 23.09 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1512 | 0.00 | 242.04 | 23.09 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1516 | 0.00 | 242.03 | 23.09 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1520 | 0.00 | 242.02 | 23.09 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1524 | 0.00 | 242.01 | 23.09 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1528 | 0.00 | 241.99 | 23.09 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1532 | 0.00 | 241.98 | 23.09 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1536 | 0.00 | 241.97 | 23.09 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1540 | 0.00 | 241.96 | 23.09 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1544 | 0.00 | 241.95 | 23.09 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1548 | 0.00 | 241.94 | 23.09 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1552 | 0.00 | 241.93 | 23.09 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1556 | 0.00 | 241.91 | 23.09 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1560 | 0.00 | 241.90 | 23.09 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1564 | 0.00 | 241.89 | 23.09 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1568 | 0.00 | 241.88 | 23.09 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1572 | 0.00 | 241.87 | 23.09 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1576 | 0.00 | 241.86 | 23.09 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1580 | 0.00 | 241.85 | 23.09 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1584 | 0.00 | 241.84 | 23.09 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1588 | 0.00 | 241.82 | 23.09 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1592 | 0.00 | 241.81 | 23.09 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1596 | 0.00 | 241.80 | 23.09 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1600 | 0.00 | 241.79 | 23.09 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1604 | 0.00 | 241.78 | 23.09 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1608 | 0.00 | 241.77 | 23.09 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1612 | 0.00 | 241.76 | 23.09 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1616 | 0.00 | 241.75 | 23.09 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1620 | 0.00 | 241.74 | 23.09 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1624 | 0.00 | 241.73 | 23.09 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1628 | 0.00 | 241.72 | 23.09 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1632 | 0.00 | 241.70 | 23.09 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1636 | 0.00 | 241.69 | 23.09 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1640 | 0.00 | 241.68 | 23.09 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1644 | 0.00 | 241.67 | 23.09 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1648 | 0.00 | 241.66 | 23.09 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1652 | 0.00 | 241.65 | 23.09 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1656 | 0.00 | 241.64 | 23.09 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1660 | 0.00 | 241.63 | 23.09 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1664 | 0.00 | 241.62 | 23.09 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1668 | 0.00 | 241.61 | 23.09 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1672 | 0.00 | 241.60 | 23.09 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1676 | 0.00 | 241.59 | 23.09 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1680 | 0.00 | 241.58 | 23.09 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 1684 | 0.00 | 241.57 | 23.09 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 1688 | 0.00 | 241.56 | 23.09 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 1692 | 0.00 | 241.55 | 23.09 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 1696 | 0.00 | 241.54 | 23.09 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 1700 | 0.00 | 241.53 | 23.09 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 1704 | 0.00 | 241.52 | 23.09 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 1708 | 0.00 | 241.51 | 23.09 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |

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Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Civ A cfs | Civ B cfs | Civ C cfs | Civ D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 1712 | 0.00 | 241.50 | 23.09 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 1716 | 0.00 | 241.49 | 23.09 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 1720 | 0.00 | 241.48 | 23.09 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 1724 | 0.00 | 241.47 | 23.09 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 1728 | 0.00 | 241.46 | 23.09 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 1732 | 0.00 | 241.45 | 23.09 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 1736 | 0.00 | 241.44 | 23.09 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 1740 | 0.00 | 241.43 | 23.09 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 1744 | 0.00 | 241.42 | 23.09 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 1748 | 0.00 | 241.41 | 23.09 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 1752 | 0.00 | 241.40 | 23.09 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 1756 | 0.00 | 241.39 | 23.09 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 1760 | 0.00 | 241.38 | 23.09 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 1764 | 0.00 | 241.37 | 23.09 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 1768 | 0.00 | 241.36 | 23.09 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 1772 | 0.00 | 241.35 | 23.09 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 1776 | 0.00 | 241.34 | 23.09 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 1780 | 0.00 | 241.33 | 23.09 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 1784 | 0.00 | 241.33 | 23.09 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 1788 | 0.00 | 241.32 | 23.09 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 1792 | 0.00 | 241.31 | 23.09 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 1796 | 0.00 | 241.30 | 23.09 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 1800 | 0.00 | 241.29 | 23.09 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 1804 | 0.00 | 241.28 | 23.09 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 1808 | 0.00 | 241.27 | 23.09 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 1812 | 0.00 | 241.26 | 23.09 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 1816 | 0.00 | 241.25 | 23.09 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 1820 | 0.00 | 241.24 | 23.09 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 1824 | 0.00 | 241.23 | 23.09 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 1828 | 0.00 | 241.23 | 23.09 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 1832 | 0.00 | 241.22 | 23.09 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 1836 | 0.00 | 241.21 | 23.09 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 1840 | 0.00 | 241.20 | 23.09 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 1844 | 0.00 | 241.19 | 23.09 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 1848 | 0.00 | 241.18 | 23.09 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 1852 | 0.00 | 241.17 | 23.09 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 1856 | 0.00 | 241.16 | 23.09 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 1860 | 0.00 | 241.16 | 23.09 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 1864 | 0.00 | 241.15 | 23.09 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 1868 | 0.00 | 241.14 | 23.09 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 1872 | 0.00 | 241.13 | 23.09 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 1876 | 0.00 | 241.12 | 23.09 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 1880 | 0.00 | 241.11 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 1884 | 0.00 | 241.10 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 1888 | 0.00 | 241.10 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 1892 | 0.00 | 241.09 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 1896 | 0.00 | 241.08 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 1900 | 0.00 | 241.07 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 1904 | 0.00 | 241.06 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 1908 | 0.00 | 241.05 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 1912 | 0.00 | 241.05 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |

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Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 1916 | 0.00 | 241.04 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 1920 | 0.00 | 241.03 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 1924 | 0.00 | 241.02 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 1928 | 0.00 | 241.01 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 1932 | 0.00 | 241.01 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 1936 | 0.00 | 241.00 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 1940 | 0.00 | 240.99 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 1944 | 0.00 | 240.98 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 1948 | 0.00 | 240.97 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 1952 | 0.00 | 240.97 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 1956 | 0.00 | 240.96 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 1960 | 0.00 | 240.95 | 23.09 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 1964 | 0.00 | 240.94 | 23.09 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 1968 | 0.00 | 240.94 | 23.09 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 1972 | 0.00 | 240.93 | 23.09 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 1976 | 0.00 | 240.92 | 23.09 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 1980 | 0.00 | 240.91 | 23.09 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 1984 | 0.00 | 240.91 | 23.09 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 1988 | 0.00 | 240.90 | 23.09 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 1992 | 0.00 | 240.89 | 23.09 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 1996 | 0.00 | 240.88 | 23.09 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 2000 | 0.00 | 240.88 | 23.09 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 2004 | 0.00 | 240.87 | 23.09 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 2008 | 0.00 | 240.86 | 23.09 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 2012 | 0.00 | 240.85 | 23.09 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 2016 | 0.00 | 240.85 | 23.09 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 2020 | 0.00 | 240.84 | 23.09 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 2024 | 0.00 | 240.83 | 23.09 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 2028 | 0.00 | 240.83 | 23.09 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 2032 | 0.00 | 240.82 | 23.09 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 2036 | 0.00 | 240.81 | 23.09 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 2040 | 0.00 | 240.80 | 23.09 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 2044 | 0.00 | 240.80 | 23.09 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 2048 | 0.00 | 240.79 | 23.09 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 2052 | 0.00 | 240.78 | 23.09 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 2056 | 0.00 | 240.78 | 23.09 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 2060 | 0.00 | 240.77 | 23.09 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 2064 | 0.00 | 240.76 | 23.09 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 2068 | 0.00 | 240.76 | 23.09 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 2072 | 0.00 | 240.75 | 23.09 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 2076 | 0.00 | 240.74 | 23.09 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 2080 | 0.00 | 240.74 | 23.09 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 2084 | 0.00 | 240.73 | 23.09 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 2088 | 0.00 | 240.72 | 23.09 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 2092 | 0.00 | 240.72 | 23.09 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 2096 | 0.00 | 240.71 | 23.09 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 2100 | 0.00 | 240.70 | 23.09 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 2104 | 0.00 | 240.70 | 23.09 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 2108 | 0.00 | 240.69 | 23.09 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 2112 | 0.00 | 240.68 | 23.09 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 2116 | 0.00 | 240.68 | 23.09 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |

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Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 2120 | 0.00 | 240.67 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 2124 | 0.00 | 240.67 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 2128 | 0.00 | 240.66 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 2132 | 0.00 | 240.65 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 2136 | 0.00 | 240.65 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 2140 | 0.00 | 240.64 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 2144 | 0.00 | 240.63 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 2148 | 0.00 | 240.63 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 2152 | 0.00 | 240.62 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 2156 | 0.00 | 240.62 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 2160 | 0.00 | 240.61 | 23.09 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |
| 2164 | 0.00 | 240.61 | 23.09 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |
| 2168 | 0.00 | 240.60 | 23.09 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |
| 2172 | 0.00 | 240.59 | 23.09 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |
| 2176 | 0.00 | 240.59 | 23.09 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |
| 2180 | 0.00 | 240.58 | 23.09 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |
| 2184 | 0.00 | 240.58 | 23.09 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |
| 2188 | 0.00 | 240.57 | 23.09 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |
| 2192 | 0.00 | 240.56 | 23.09 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |
| 2196 | 0.00 | 240.56 | 23.09 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 2200 | 0.00 | 240.55 | 23.09 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 2204 | 0.00 | 240.55 | 23.09 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 2208 | 0.00 | 240.54 | 23.09 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 2212 | 0.00 | 240.54 | 23.09 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 2216 | 0.00 | 240.53 | 23.09 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 2220 | 0.00 | 240.53 | 23.09 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 2224 | 0.00 | 240.52 | 23.09 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 2228 | 0.00 | 240.52 | 23.09 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 2232 | 0.00 | 240.51 | 23.09 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 2236 | 0.00 | 240.51 | 23.09 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 2240 | 0.00 | 240.50 | 23.09 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 2244 | 0.00 | 240.50 | 23.09 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 2248 | 0.00 | 240.49 | 23.09 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 2252 | 0.00 | 240.49 | 23.09 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 2256 | 0.00 | 240.48 | 23.09 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 2260 | 0.00 | 240.48 | 23.09 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 2264 | 0.00 | 240.47 | 23.09 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 2268 | 0.00 | 240.47 | 23.09 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 2272 | 0.00 | 240.46 | 23.09 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 2276 | 0.00 | 240.46 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 2280 | 0.00 | 240.45 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 2284 | 0.00 | 240.45 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 2288 | 0.00 | 240.44 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 2292 | 0.00 | 240.44 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 2296 | 0.00 | 240.43 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 2300 | 0.00 | 240.43 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 2304 | 0.00 | 240.42 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 2308 | 0.00 | 240.42 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 2312 | 0.00 | 240.41 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 2316 | 0.00 | 240.41 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 2320 | 0.00 | 240.40 | 23.09 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.12 |

Continues on next page...

Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 2324 | 0.00 | 240.40 | 23.09 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.12 |
| 2328 | 0.00 | 240.40 | 23.09 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.12 |
| 2332 | 0.00 | 240.39 | 23.09 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.12 |
| 2336 | 0.00 | 240.39 | 23.09 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.12 |
| 2340 | 0.00 | 240.38 | 23.09 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.12 |
| 2344 | 0.00 | 240.38 | 23.09 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.12 |
| 2348 | 0.00 | 240.37 | 23.09 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.12 |
| 2352 | 0.00 | 240.37 | 23.09 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.11 |
| 2356 | 0.00 | 240.37 | 23.09 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.11 |
| 2360 | 0.00 | 240.36 | 23.09 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.11 |
| 2364 | 0.00 | 240.36 | 23.09 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.11 |
| 2368 | 0.00 | 240.35 | 23.09 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.11 |
| 2372 | 0.00 | 240.35 | 23.09 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.11 |
| 2376 | 0.00 | 240.35 | 23.09 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.11 |
| 2380 | 0.00 | 240.34 | 23.09 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.11 |
| 2384 | 0.00 | 240.34 | 23.09 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.11 |
| 2388 | 0.00 | 240.33 | 23.09 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 2392 | 0.00 | 240.33 | 23.09 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 2396 | 0.00 | 240.33 | 23.09 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 2400 | 0.00 | 240.32 | 23.09 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 2404 | 0.00 | 240.32 | 23.09 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 2408 | 0.00 | 240.32 | 23.09 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 2412 | 0.00 | 240.31 | 23.09 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 2416 | 0.00 | 240.31 | 23.09 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 2420 | 0.00 | 240.31 | 23.09 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 2424 | 0.00 | 240.30 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 2428 | 0.00 | 240.30 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 2432 | 0.00 | 240.30 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 2436 | 0.00 | 240.29 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 2440 | 0.00 | 240.29 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 2444 | 0.00 | 240.29 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 2448 | 0.00 | 240.28 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 2452 | 0.00 | 240.28 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 2456 | 0.00 | 240.28 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 2460 | 0.00 | 240.27 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 2464 | 0.00 | 240.27 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 2468 | 0.00 | 240.27 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 2472 | 0.00 | 240.26 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 2476 | 0.00 | 240.26 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 2480 | 0.00 | 240.26 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 2484 | 0.00 | 240.25 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 2488 | 0.00 | 240.25 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 2492 | 0.00 | 240.25 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 2496 | 0.00 | 240.25 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 2500 | 0.00 | 240.24 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 2504 | 0.00 | 240.24 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 2508 | 0.00 | 240.24 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 2512 | 0.00 | 240.24 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 2516 | 0.00 | 240.23 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 2520 | 0.00 | 240.23 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 2524 | 0.00 | 240.23 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |

Continues on next page...

Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 2528 | 0.00 | 240.22 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 2532 | 0.00 | 240.22 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 2536 | 0.00 | 240.22 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 2540 | 0.00 | 240.22 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 2544 | 0.00 | 240.21 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 2548 | 0.00 | 240.21 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 2552 | 0.00 | 240.21 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 2556 | 0.00 | 240.21 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 2560 | 0.00 | 240.20 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 2564 | 0.00 | 240.20 | 23.09 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 2568 | 0.00 | 240.20 | 23.09 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |
| 2572 | 0.00 | 240.20 | 23.09 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |
| 2576 | 0.00 | 240.20 | 23.09 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |
| 2580 | 0.00 | 240.19 | 23.09 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |
| 2584 | 0.00 | 240.19 | 23.09 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |
| 2588 | 0.00 | 240.19 | 23.09 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |
| 2592 | 0.00 | 240.19 | 23.09 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |
| 2596 | 0.00 | 240.18 | 23.09 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |
| 2600 | 0.00 | 240.18 | 23.09 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |
| 2604 | 0.00 | 240.18 | 23.09 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |
| 2608 | 0.00 | 240.18 | 23.09 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |
| 2612 | 0.00 | 240.18 | 23.09 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |
| 2616 | 0.00 | 240.17 | 23.09 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |
| 2620 | 0.00 | 240.17 | 23.09 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |
| 2624 | 0.00 | 240.17 | 23.09 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |
| 2628 | 0.00 | 240.17 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 2632 | 0.00 | 240.17 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 2636 | 0.00 | 240.16 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 2640 | 0.00 | 240.16 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 2644 | 0.00 | 240.16 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 2648 | 0.00 | 240.16 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 2652 | 0.00 | 240.16 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 2656 | 0.00 | 240.15 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 2660 | 0.00 | 240.15 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 2664 | 0.00 | 240.15 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 2668 | 0.00 | 240.15 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 2672 | 0.00 | 240.15 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 2676 | 0.00 | 240.15 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 2680 | 0.00 | 240.14 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 2684 | 0.00 | 240.14 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 2688 | 0.00 | 240.14 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 2692 | 0.00 | 240.14 | 23.09 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 2696 | 0.00 | 240.14 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 2700 | 0.00 | 240.14 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 2704 | 0.00 | 240.13 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 2708 | 0.00 | 240.13 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 2712 | 0.00 | 240.13 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 2716 | 0.00 | 240.13 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 2720 | 0.00 | 240.13 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 2724 | 0.00 | 240.13 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 2728 | 0.00 | 240.13 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |

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Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|-----------------------|-----------------------|-------------------------|----------------------|----------------------|----------------------|----------------------|---------------------|---------------------|---------------------|---------------------|----------------------|------------------------|
| 2732 | 0.00 | 240.12 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 2736 | 0.00 | 240.12 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 2740 | 0.00 | 240.12 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 2744 | 0.00 | 240.12 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 2748 | 0.00 | 240.12 | 23.09 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |

...End

Reservoir Report

Reservoir No. 1 - Retention Basin No. 1

Hydraflow Hydrographs by Intelisolve

Pond Data

Pond storage is based on known contour areas. Average end area method used.

Stage / Storage Table

| Stage (ft) | Elevation (ft) | Contour area (sqft) | Incr. Storage (cuft) | Total storage (cuft) |
|------------|----------------|---------------------|----------------------|----------------------|
| 0.00 | 238.00 | 4,449 | 0 | 0 |
| 2.00 | 240.00 | 6,679 | 11,128 | 11,128 |
| 4.00 | 242.00 | 6,679 | 13,358 | 24,486 |
| 6.00 | 244.00 | 6,679 | 13,358 | 37,844 |
| 8.00 | 246.00 | 6,679 | 13,358 | 51,202 |
| 8.50 | 246.50 | 6,679 | 3,340 | 54,542 |

Culvert / Orifice Structures

| | [A] | [B] | [C] | [D] |
|---------------|----------|--------|------|------|
| Rise in | = 6.0 | 3.0 | 0.0 | 0.0 |
| Span in | = 6.0 | 3.0 | 0.0 | 0.0 |
| No. Barrels | = 10 | 1 | 0 | 0 |
| Invert El. ft | = 227.00 | 240.00 | 0.00 | 0.00 |
| Length ft | = 68.0 | 1.0 | 0.0 | 0.0 |
| Slope % | = 6.03 | 0.00 | 0.00 | 0.00 |
| N-Value | = .013 | .013 | .000 | .000 |
| Orif. Coeff. | = 0.60 | 0.60 | 0.00 | 0.00 |
| Multi-Stage | = n/a | Yes | No | No |

Weir Structures

| | [A] | [B] | [C] | [D] |
|--------------|----------|--------|--------|------|
| Crest Len ft | = 1.00 | 40.00 | 16.00 | 0.00 |
| Crest El. ft | = 243.00 | 244.50 | 244.00 | 0.00 |
| Weir Coeff. | = 3.33 | 2.60 | 3.33 | 0.00 |
| Weir Type | = Rect | Broad | Rect | --- |
| Multi-Stage | = Yes | Yes | Yes | No |

Exfiltration Rate = 0.00 in/hr/sqft Tailwater Elev. = 0.00 ft

Stage / Storage / Discharge Table

Note: All outflows have been analyzed under inlet and outlet control.

| Stage ft | Storage cuft | Elevation ft | Civ A cfs | Civ B cfs | Civ C cfs | Civ D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Total cfs |
|----------|--------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-----------|
| 0.00 | 0 | 238.00 | 0.00 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.00 |
| 0.20 | 1,113 | 238.20 | 23.09 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.00 |
| 0.40 | 2,226 | 238.40 | 23.09 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.00 |
| 0.60 | 3,338 | 238.60 | 23.09 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.00 |
| 0.80 | 4,451 | 238.80 | 23.09 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.00 |
| 1.00 | 5,564 | 239.00 | 23.09 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.00 |
| 1.20 | 6,677 | 239.20 | 23.09 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.00 |
| 1.40 | 7,790 | 239.40 | 23.09 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.00 |
| 1.60 | 8,902 | 239.60 | 23.09 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.00 |
| 1.80 | 10,015 | 239.80 | 23.09 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.00 |
| 2.00 | 11,128 | 240.00 | 23.09 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.00 |
| 2.20 | 12,464 | 240.20 | 23.09 | 0.06 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.06 |
| 2.40 | 13,800 | 240.40 | 23.09 | 0.12 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.12 |
| 2.60 | 15,135 | 240.60 | 23.09 | 0.16 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.16 |
| 2.80 | 16,471 | 240.80 | 23.09 | 0.19 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.19 |
| 3.00 | 17,807 | 241.00 | 23.09 | 0.22 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.22 |
| 3.20 | 19,143 | 241.20 | 23.09 | 0.25 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.25 |
| 3.40 | 20,479 | 241.40 | 23.09 | 0.27 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.27 |
| 3.60 | 21,814 | 241.60 | 23.09 | 0.29 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.29 |
| 3.80 | 23,150 | 241.80 | 23.09 | 0.31 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.31 |
| 4.00 | 24,486 | 242.00 | 23.09 | 0.32 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.32 |
| 4.20 | 25,822 | 242.20 | 23.09 | 0.34 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.34 |
| 4.40 | 27,158 | 242.40 | 23.09 | 0.36 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.36 |
| 4.60 | 28,493 | 242.60 | 23.09 | 0.37 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.37 |
| 4.80 | 29,829 | 242.80 | 23.09 | 0.39 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.39 |
| 5.00 | 31,165 | 243.00 | 23.09 | 0.40 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.40 |
| 5.20 | 32,501 | 243.20 | 23.09 | 0.41 | --- | --- | 0.30 | 0.00 | 0.00 | --- | --- | 0.71 |
| 5.40 | 33,837 | 243.40 | 23.09 | 0.43 | --- | --- | 0.84 | 0.00 | 0.00 | --- | --- | 1.27 |
| 5.60 | 35,172 | 243.60 | 23.09 | 0.44 | --- | --- | 1.55 | 0.00 | 0.00 | --- | --- | 1.99 |
| 5.80 | 36,508 | 243.80 | 23.09 | 0.45 | --- | --- | 2.38 | 0.00 | 0.00 | --- | --- | 2.84 |
| 6.00 | 37,844 | 244.00 | 23.09 | 0.47 | --- | --- | 3.33 | 0.00 | 0.00 | --- | --- | 3.80 |
| 6.20 | 39,180 | 244.20 | 23.09 | 0.48 | --- | --- | 4.38 | 0.00 | 4.77 | --- | --- | 9.62 |

Continues on next page...

Stage / Storage / Discharge Table

| Stage ft | Storage cuft | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Total cfs |
|-------------|-----------------|-----------------|--------------|--------------|--------------|--------------|-------------|-------------|-------------|-------------|--------------|--------------|
| 6.40 | 40,516 | 244.40 | 23.09 | 0.49 | --- | --- | 5.52 | 0.00 | 13.48 | --- | --- | 19.48 |
| 6.60 | 41,851 | 244.60 | 27.65 | 0.12 | --- | --- | 3.92 | 3.29 | 20.31 | --- | --- | 27.64 |
| 6.80 | 43,187 | 244.80 | 27.92 | 0.05 | --- | --- | 2.40 | 10.00 | 15.47 | --- | --- | 27.92 |
| 7.00 | 44,523 | 245.00 | 28.07 | 0.03 | --- | --- | 1.86 | 12.37 | 13.75 | --- | --- | 28.02 |
| 7.20 | 45,859 | 245.20 | 28.21 | 0.02 | --- | --- | 1.58 | 13.73 | 12.83 | --- | --- | 28.16 |
| 7.40 | 47,195 | 245.40 | 28.34 | 0.02 | --- | --- | 1.40 | 14.64 | 12.28 | --- | --- | 28.34 |
| 7.60 | 48,530 | 245.60 | 28.47 | 0.01 | --- | --- | 1.28 | 15.27 | 11.88 | --- | --- | 28.43 |
| 7.80 | 49,866 | 245.80 | 28.60 | 0.01 | --- | --- | 1.18 | 15.60 | 11.49 | --- | --- | 28.28 |
| 8.00 | 51,202 | 246.00 | 28.73 | 0.01 | --- | --- | 1.11 | 15.96 | 11.27 | --- | --- | 28.34 |
| 8.05 | 51,536 | 246.05 | 28.76 | 0.01 | --- | --- | 1.10 | 16.14 | 11.30 | --- | --- | 28.55 |
| 8.10 | 51,870 | 246.10 | 28.79 | 0.01 | --- | --- | 1.09 | 16.28 | 11.29 | --- | --- | 28.67 |
| 8.15 | 52,204 | 246.15 | 28.82 | 0.01 | --- | --- | 1.08 | 16.37 | 11.27 | --- | --- | 28.72 |
| 8.20 | 52,538 | 246.20 | 28.86 | 0.01 | --- | --- | 1.06 | 16.40 | 11.20 | --- | --- | 28.68 |
| 8.25 | 52,872 | 246.25 | 28.89 | 0.01 | --- | --- | 1.05 | 16.38 | 11.10 | --- | --- | 28.53 |
| 8.30 | 53,206 | 246.30 | 28.92 | 0.01 | --- | --- | 1.02 | 16.28 | 10.96 | --- | --- | 28.28 |
| 8.35 | 53,540 | 246.35 | 28.95 | 0.01 | --- | --- | 1.00 | 16.06 | 10.74 | --- | --- | 27.80 |
| 8.40 | 53,874 | 246.40 | 28.98 | 0.01 | --- | --- | 1.01 | 16.54 | 11.00 | --- | --- | 28.56 |
| 8.45 | 54,208 | 246.45 | 29.01 | 0.01 | --- | --- | 0.98 | 16.25 | 10.74 | --- | --- | 27.98 |
| 8.50 | 54,542 | 246.50 | 29.05 | 0.01 | --- | --- | 0.98 | 16.46 | 10.82 | --- | --- | 28.27 |

...End

Hydrograph Report

Hyd. No. 12

Basin 2 Out

Hydrograph type = Reservoir
 Storm frequency = 50 yrs
 Inflow hyd. No. = 9
 Max. Elevation = 233.62 ft

Peak discharge = 4.95 cfs
 Time interval = 2 min
 Reservoir name = Detention Basin 2
 Max. Storage = 18,845 cuft

Storage Indication method used.

Outflow hydrograph volume = 40,824 cuft

Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 720 | 6.14 | 232.30 | 6.68 | 0.26 | ---- | ---- | 0.37 | ---- | ---- | ---- | 0.043 | 0.67 |
| 724 | 8.53 | 232.55 | 6.68 | 0.28 | ---- | ---- | 0.90 | ---- | ---- | ---- | 0.044 | 1.22 |
| 728 | 10.20 | 232.85 | 6.68 | 0.31 | ---- | ---- | 1.74 | ---- | ---- | ---- | 0.045 | 2.10 |
| 732 | 10.15 | 233.16 | 6.68 | 0.34 | ---- | ---- | 2.74 | ---- | ---- | ---- | 0.046 | 3.12 |
| 736 | 8.93 | 233.39 | 6.68 | 0.36 | ---- | ---- | 3.61 | ---- | ---- | ---- | 0.046 | 4.01 |
| 740 | 7.34 | 233.54 | 6.68 | 0.37 | ---- | ---- | 4.21 | ---- | ---- | ---- | 0.047 | 4.63 |
| 744 | 5.70 | 233.61 | 6.68 | 0.37 | ---- | ---- | 4.49 | ---- | ---- | ---- | 0.047 | 4.91 |
| 748 | 4.50 | 233.61 | 6.68 | 0.37 | ---- | ---- | 4.51 | ---- | ---- | ---- | 0.047 | 4.93 |
| 752 | 3.63 | 233.58 | 6.68 | 0.37 | ---- | ---- | 4.38 | ---- | ---- | ---- | 0.047 | 4.80 |
| 756 | 2.87 | 233.53 | 6.68 | 0.37 | ---- | ---- | 4.15 | ---- | ---- | ---- | 0.047 | 4.56 |
| 760 | 2.28 | 233.45 | 6.68 | 0.36 | ---- | ---- | 3.85 | ---- | ---- | ---- | 0.047 | 4.26 |
| 764 | 1.89 | 233.37 | 6.68 | 0.35 | ---- | ---- | 3.54 | ---- | ---- | ---- | 0.046 | 3.94 |
| 768 | 1.66 | 233.29 | 6.68 | 0.35 | ---- | ---- | 3.24 | ---- | ---- | ---- | 0.046 | 3.63 |
| 772 | 1.52 | 233.22 | 6.68 | 0.34 | ---- | ---- | 2.96 | ---- | ---- | ---- | 0.046 | 3.35 |
| 776 | 1.43 | 233.15 | 6.68 | 0.34 | ---- | ---- | 2.72 | ---- | ---- | ---- | 0.046 | 3.10 |
| 780 | 1.34 | 233.09 | 6.68 | 0.33 | ---- | ---- | 2.50 | ---- | ---- | ---- | 0.045 | 2.88 |
| 784 | 1.25 | 233.03 | 6.68 | 0.33 | ---- | ---- | 2.30 | ---- | ---- | ---- | 0.045 | 2.67 |
| 788 | 1.17 | 232.98 | 6.68 | 0.32 | ---- | ---- | 2.12 | ---- | ---- | ---- | 0.045 | 2.49 |
| 792 | 1.12 | 232.93 | 6.68 | 0.32 | ---- | ---- | 1.97 | ---- | ---- | ---- | 0.045 | 2.33 |
| 796 | 1.08 | 232.88 | 6.68 | 0.31 | ---- | ---- | 1.82 | ---- | ---- | ---- | 0.045 | 2.18 |
| 800 | 1.04 | 232.84 | 6.68 | 0.31 | ---- | ---- | 1.69 | ---- | ---- | ---- | 0.045 | 2.05 |
| 804 | 1.02 | 232.80 | 6.68 | 0.31 | ---- | ---- | 1.58 | ---- | ---- | ---- | 0.045 | 1.93 |
| 808 | 1.00 | 232.77 | 6.68 | 0.30 | ---- | ---- | 1.48 | ---- | ---- | ---- | 0.045 | 1.83 |
| 812 | 0.97 | 232.74 | 6.68 | 0.30 | ---- | ---- | 1.40 | ---- | ---- | ---- | 0.044 | 1.74 |
| 816 | 0.95 | 232.71 | 6.68 | 0.30 | ---- | ---- | 1.32 | ---- | ---- | ---- | 0.044 | 1.66 |
| 820 | 0.93 | 232.68 | 6.68 | 0.29 | ---- | ---- | 1.24 | ---- | ---- | ---- | 0.044 | 1.58 |
| 824 | 0.90 | 232.66 | 6.68 | 0.29 | ---- | ---- | 1.17 | ---- | ---- | ---- | 0.044 | 1.51 |
| 828 | 0.88 | 232.63 | 6.68 | 0.29 | ---- | ---- | 1.11 | ---- | ---- | ---- | 0.044 | 1.44 |
| 832 | 0.85 | 232.61 | 6.68 | 0.29 | ---- | ---- | 1.05 | ---- | ---- | ---- | 0.044 | 1.38 |
| 836 | 0.83 | 232.59 | 6.68 | 0.29 | ---- | ---- | 1.00 | ---- | ---- | ---- | 0.044 | 1.33 |
| 840 | 0.81 | 232.57 | 6.68 | 0.28 | ---- | ---- | 0.95 | ---- | ---- | ---- | 0.044 | 1.28 |
| 844 | 0.78 | 232.55 | 6.68 | 0.28 | ---- | ---- | 0.91 | ---- | ---- | ---- | 0.044 | 1.24 |
| 848 | 0.76 | 232.54 | 6.68 | 0.28 | ---- | ---- | 0.87 | ---- | ---- | ---- | 0.044 | 1.20 |
| 852 | 0.74 | 232.52 | 6.68 | 0.28 | ---- | ---- | 0.83 | ---- | ---- | ---- | 0.044 | 1.16 |
| 856 | 0.73 | 232.50 | 6.68 | 0.28 | ---- | ---- | 0.80 | ---- | ---- | ---- | 0.044 | 1.12 |
| 860 | 0.72 | 232.49 | 6.68 | 0.28 | ---- | ---- | 0.76 | ---- | ---- | ---- | 0.044 | 1.08 |
| 864 | 0.71 | 232.47 | 6.68 | 0.27 | ---- | ---- | 0.73 | ---- | ---- | ---- | 0.044 | 1.05 |
| 868 | 0.69 | 232.46 | 6.68 | 0.27 | ---- | ---- | 0.70 | ---- | ---- | ---- | 0.044 | 1.02 |

Continues on next page...

Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 872 | 0.68 | 232.45 | 6.68 | 0.27 | ---- | ---- | 0.67 | ---- | ---- | ---- | 0.044 | 0.99 |
| 876 | 0.67 | 232.44 | 6.68 | 0.27 | ---- | ---- | 0.64 | ---- | ---- | ---- | 0.043 | 0.96 |
| 880 | 0.66 | 232.43 | 6.68 | 0.27 | ---- | ---- | 0.62 | ---- | ---- | ---- | 0.043 | 0.93 |
| 884 | 0.65 | 232.42 | 6.68 | 0.27 | ---- | ---- | 0.59 | ---- | ---- | ---- | 0.043 | 0.91 |
| 888 | 0.64 | 232.41 | 6.68 | 0.27 | ---- | ---- | 0.57 | ---- | ---- | ---- | 0.043 | 0.88 |
| 892 | 0.63 | 232.40 | 6.68 | 0.27 | ---- | ---- | 0.55 | ---- | ---- | ---- | 0.043 | 0.86 |
| 896 | 0.61 | 232.39 | 6.68 | 0.27 | ---- | ---- | 0.53 | ---- | ---- | ---- | 0.043 | 0.84 |
| 900 | 0.60 | 232.38 | 6.68 | 0.26 | ---- | ---- | 0.52 | ---- | ---- | ---- | 0.043 | 0.83 |
| 904 | 0.59 | 232.37 | 6.68 | 0.26 | ---- | ---- | 0.50 | ---- | ---- | ---- | 0.043 | 0.81 |
| 908 | 0.58 | 232.36 | 6.68 | 0.26 | ---- | ---- | 0.49 | ---- | ---- | ---- | 0.043 | 0.79 |
| 912 | 0.57 | 232.35 | 6.68 | 0.26 | ---- | ---- | 0.47 | ---- | ---- | ---- | 0.043 | 0.78 |
| 916 | 0.56 | 232.35 | 6.68 | 0.26 | ---- | ---- | 0.46 | ---- | ---- | ---- | 0.043 | 0.76 |
| 920 | 0.55 | 232.34 | 6.68 | 0.26 | ---- | ---- | 0.44 | ---- | ---- | ---- | 0.043 | 0.75 |
| 924 | 0.53 | 232.33 | 6.68 | 0.26 | ---- | ---- | 0.43 | ---- | ---- | ---- | 0.043 | 0.73 |
| 928 | 0.52 | 232.32 | 6.68 | 0.26 | ---- | ---- | 0.42 | ---- | ---- | ---- | 0.043 | 0.72 |
| 932 | 0.51 | 232.31 | 6.68 | 0.26 | ---- | ---- | 0.40 | ---- | ---- | ---- | 0.043 | 0.70 |
| 936 | 0.50 | 232.31 | 6.68 | 0.26 | ---- | ---- | 0.39 | ---- | ---- | ---- | 0.043 | 0.69 |
| 940 | 0.49 | 232.30 | 6.68 | 0.26 | ---- | ---- | 0.38 | ---- | ---- | ---- | 0.043 | 0.67 |
| 944 | 0.48 | 232.29 | 6.68 | 0.26 | ---- | ---- | 0.36 | ---- | ---- | ---- | 0.043 | 0.66 |
| 948 | 0.46 | 232.28 | 6.68 | 0.25 | ---- | ---- | 0.35 | ---- | ---- | ---- | 0.043 | 0.65 |
| 952 | 0.45 | 232.28 | 6.68 | 0.25 | ---- | ---- | 0.34 | ---- | ---- | ---- | 0.043 | 0.63 |
| 956 | 0.44 | 232.27 | 6.68 | 0.25 | ---- | ---- | 0.32 | ---- | ---- | ---- | 0.043 | 0.62 |
| 960 | 0.43 | 232.26 | 6.68 | 0.25 | ---- | ---- | 0.31 | ---- | ---- | ---- | 0.043 | 0.61 |
| 964 | 0.42 | 232.26 | 6.68 | 0.25 | ---- | ---- | 0.30 | ---- | ---- | ---- | 0.043 | 0.59 |
| 968 | 0.41 | 232.25 | 6.68 | 0.25 | ---- | ---- | 0.29 | ---- | ---- | ---- | 0.043 | 0.58 |
| 972 | 0.40 | 232.24 | 6.68 | 0.25 | ---- | ---- | 0.27 | ---- | ---- | ---- | 0.043 | 0.57 |
| 976 | 0.39 | 232.24 | 6.68 | 0.25 | ---- | ---- | 0.26 | ---- | ---- | ---- | 0.043 | 0.55 |
| 980 | 0.39 | 232.23 | 6.68 | 0.25 | ---- | ---- | 0.25 | ---- | ---- | ---- | 0.043 | 0.54 |
| 984 | 0.38 | 232.22 | 6.68 | 0.25 | ---- | ---- | 0.24 | ---- | ---- | ---- | 0.043 | 0.53 |
| 988 | 0.38 | 232.22 | 6.68 | 0.25 | ---- | ---- | 0.23 | ---- | ---- | ---- | 0.043 | 0.52 |
| 992 | 0.37 | 232.21 | 6.68 | 0.25 | ---- | ---- | 0.22 | ---- | ---- | ---- | 0.043 | 0.51 |
| 996 | 0.37 | 232.21 | 6.68 | 0.25 | ---- | ---- | 0.21 | ---- | ---- | ---- | 0.043 | 0.50 |

...End

Reservoir Report

Reservoir No. 2 - Detention Basin 2

Hydraflow Hydrographs by Intelisolve

Pond Data

Pond storage is based on known contour areas. Average end area method used.

Stage / Storage Table

| Stage (ft) | Elevation (ft) | Contour area (sqft) | Incr. Storage (cuft) | Total storage (cuft) |
|------------|----------------|---------------------|----------------------|----------------------|
| 0.00 | 229.33 | 00 | 0 | 0 |
| 0.67 | 230.00 | 2,454 | 822 | 822 |
| 2.67 | 232.00 | 5,689 | 8,143 | 8,965 |
| 4.67 | 234.00 | 6,522 | 12,211 | 21,176 |
| 6.67 | 236.00 | 7,413 | 13,935 | 35,111 |
| 8.67 | 238.00 | 9,192 | 16,605 | 51,716 |

Culvert / Orifice Structures

| | [A] | [B] | [C] | [D] |
|---------------|----------|--------|------|------|
| Rise in | = 6.0 | 3.0 | 0.0 | 0.0 |
| Span in | = 6.0 | 3.0 | 0.0 | 0.0 |
| No. Barrels | = 10 | 1 | 0 | 0 |
| Invert El. ft | = 228.40 | 231.00 | 0.00 | 0.00 |
| Length ft | = 40.0 | 1.0 | 0.0 | 0.0 |
| Slope % | = 1.00 | 0.00 | 0.00 | 0.00 |
| N-Value | = .013 | .013 | .000 | .000 |
| Orif. Coeff. | = 0.60 | 0.60 | 0.00 | 0.00 |
| Multi-Stage | = n/a | Yes | No | No |

Weir Structures

| | [A] | [B] | [C] | [D] |
|--------------|----------|--------|--------|------|
| Crest Len ft | = 0.66 | 20.00 | 16.00 | 0.00 |
| Crest El. ft | = 232.00 | 236.00 | 235.50 | 0.00 |
| Weir Coeff. | = 3.33 | 2.60 | 3.33 | 0.00 |
| Weir Type | = Rect | Broad | Rect | --- |
| Multi-Stage | = Yes | No | Yes | No |

Exfiltration Rate = 0.32 in/hr/sqft Tailwater Elev. = 0.00 ft

Note: All outflows have been analyzed under inlet and outlet control.

Stage / Storage / Discharge Table

| Stage ft | Storage cuft | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfli cfs | Total cfs |
|----------|--------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-----------|
| 0.00 | 0 | 229.33 | 0.00 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.000 | 0.00 |
| 0.07 | 82 | 229.40 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.002 | 0.00 |
| 0.13 | 164 | 229.46 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.004 | 0.00 |
| 0.20 | 247 | 229.53 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.005 | 0.01 |
| 0.27 | 329 | 229.60 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.007 | 0.01 |
| 0.34 | 411 | 229.67 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.009 | 0.01 |
| 0.40 | 493 | 229.73 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.011 | 0.01 |
| 0.47 | 575 | 229.80 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.013 | 0.01 |
| 0.54 | 658 | 229.87 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.015 | 0.01 |
| 0.60 | 740 | 229.93 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.016 | 0.02 |
| 0.67 | 822 | 230.00 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.018 | 0.02 |
| 0.87 | 1,636 | 230.20 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.021 | 0.02 |
| 1.07 | 2,451 | 230.40 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.023 | 0.02 |
| 1.27 | 3,265 | 230.60 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.025 | 0.03 |
| 1.47 | 4,079 | 230.80 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.028 | 0.03 |
| 1.67 | 4,894 | 231.00 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.030 | 0.03 |
| 1.87 | 5,708 | 231.20 | 6.68 | 0.06 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.033 | 0.10 |
| 2.07 | 6,522 | 231.40 | 6.68 | 0.12 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.035 | 0.16 |
| 2.27 | 7,336 | 231.60 | 6.68 | 0.16 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.037 | 0.20 |
| 2.47 | 8,151 | 231.80 | 6.68 | 0.19 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.040 | 0.23 |
| 2.67 | 8,965 | 232.00 | 6.68 | 0.22 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.042 | 0.26 |
| 2.87 | 10,186 | 232.20 | 6.68 | 0.25 | --- | --- | 0.20 | 0.00 | 0.00 | --- | 0.043 | 0.48 |
| 3.07 | 11,407 | 232.40 | 6.68 | 0.27 | --- | --- | 0.56 | 0.00 | 0.00 | --- | 0.043 | 0.87 |
| 3.27 | 12,628 | 232.60 | 6.68 | 0.29 | --- | --- | 1.02 | 0.00 | 0.00 | --- | 0.044 | 1.35 |
| 3.47 | 13,849 | 232.80 | 6.68 | 0.31 | --- | --- | 1.57 | 0.00 | 0.00 | --- | 0.045 | 1.92 |
| 3.67 | 15,071 | 233.00 | 6.68 | 0.32 | --- | --- | 2.20 | 0.00 | 0.00 | --- | 0.045 | 2.57 |
| 3.87 | 16,292 | 233.20 | 6.68 | 0.34 | --- | --- | 2.89 | 0.00 | 0.00 | --- | 0.046 | 3.28 |
| 4.07 | 17,513 | 233.40 | 6.68 | 0.36 | --- | --- | 3.64 | 0.00 | 0.00 | --- | 0.046 | 4.04 |
| 4.27 | 18,734 | 233.60 | 6.68 | 0.37 | --- | --- | 4.45 | 0.00 | 0.00 | --- | 0.047 | 4.87 |
| 4.47 | 19,955 | 233.80 | 6.68 | 0.39 | --- | --- | 5.31 | 0.00 | 0.00 | --- | 0.048 | 5.74 |
| 4.67 | 21,176 | 234.00 | 6.68 | 0.40 | --- | --- | 6.22 | 0.00 | 0.00 | --- | 0.048 | 6.67 |
| 4.87 | 22,570 | 234.20 | 7.59 | 0.41 | --- | --- | 7.17 | 0.00 | 0.00 | --- | 0.049 | 7.64 |

Continues on next page...

Stage / Storage / Discharge Table

| Stage ft | Storage cuft | Elevation ft | Civ A cfs | Civ B cfs | Civ C cfs | Civ D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Total cfs |
|-------------|-----------------|-----------------|--------------|--------------|--------------|--------------|-------------|-------------|-------------|-------------|--------------|--------------|
| 5.07 | 23,963 | 234.40 | 8.60 | 0.43 | --- | --- | 8.17 | 0.00 | 0.00 | --- | 0.050 | 8.65 |
| 5.27 | 25,357 | 234.60 | 9.65 | 0.44 | --- | --- | 9.21 | 0.00 | 0.00 | --- | 0.050 | 9.70 |
| 5.47 | 26,750 | 234.80 | 10.75 | 0.45 | --- | --- | 10.30 | 0.00 | 0.00 | --- | 0.051 | 10.80 |
| 5.67 | 28,144 | 235.00 | 11.89 | 0.47 | --- | --- | 11.42 | 0.00 | 0.00 | --- | 0.052 | 11.94 |
| 5.87 | 29,537 | 235.20 | 13.03 | 0.44 | --- | --- | 12.58 | 0.00 | 0.00 | --- | 0.052 | 13.08 |
| 6.07 | 30,931 | 235.40 | 14.12 | 0.42 | --- | --- | 13.70 | 0.00 | 0.00 | --- | 0.053 | 14.17 |
| 6.27 | 32,324 | 235.60 | 15.89 | 0.37 | --- | --- | 13.84 | 0.00 | 1.68 | --- | 0.054 | 15.94 |
| 6.47 | 33,718 | 235.80 | 18.81 | 0.20 | --- | --- | 9.85 | 0.00 | 8.75 | --- | 0.054 | 18.86 |
| 6.67 | 35,111 | 236.00 | 19.86 | 0.10 | --- | --- | 5.97 | 0.00 | 13.80 | --- | 0.055 | 19.92 |
| 6.87 | 36,772 | 236.20 | 20.25 | 0.07 | --- | --- | 4.74 | 4.65 | 15.44 | --- | 0.056 | 24.95 |
| 7.07 | 38,432 | 236.40 | 20.56 | 0.05 | --- | --- | 4.01 | 13.15 | 16.50 | --- | 0.058 | 33.77 |
| 7.27 | 40,093 | 236.60 | 20.84 | 0.04 | --- | --- | 3.52 | 24.17 | 17.27 | --- | 0.059 | 45.05 |
| 7.47 | 41,753 | 236.80 | 21.10 | 0.03 | --- | --- | 3.17 | 37.21 | 17.88 | --- | 0.060 | 58.35 |
| 7.67 | 43,414 | 237.00 | 21.36 | 0.03 | --- | --- | 2.91 | 52.00 | 18.41 | --- | 0.061 | 73.40 |
| 7.87 | 45,074 | 237.20 | 21.62 | 0.02 | --- | --- | 2.71 | 68.35 | 18.85 | --- | 0.063 | 90.00 |
| 8.07 | 46,735 | 237.40 | 21.87 | 0.02 | --- | --- | 2.54 | 86.14 | 19.22 | --- | 0.064 | 107.99 |
| 8.27 | 48,395 | 237.60 | 22.12 | 0.02 | --- | --- | 2.41 | 105.24 | 19.56 | --- | 0.065 | 127.29 |
| 8.47 | 50,056 | 237.80 | 22.36 | 0.02 | --- | --- | 2.31 | 125.57 | 19.95 | --- | 0.067 | 147.91 |
| 8.67 | 51,716 | 238.00 | 22.60 | 0.01 | --- | --- | 2.21 | 147.08 | 20.20 | --- | 0.068 | 169.58 |

...End

Hydrograph Report

Hyd. No. 13

Basin 3 Out

Hydrograph type = Reservoir
 Storm frequency = 50 yrs
 Inflow hyd. No. = 10
 Max. Elevation = 225.21 ft

Peak discharge = 3.80 cfs
 Time interval = 2 min
 Reservoir name = Basin 3 (Hotel)
 Max. Storage = 25,675 cuft

Storage Indication method used.

Outflow hydrograph volume = 57,407 cuft

Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 704 | 3.71 | 221.77 | 10.70 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 708 | 4.75 | 222.04 | 10.70 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.41 |
| 712 | 5.86 | 222.25 | 10.70 | 0.43 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.43 |
| 716 | 7.19 | 222.52 | 10.70 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.44 |
| 720 | 10.67 | 222.89 | 10.70 | 0.47 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.47 |
| 724 | 15.68 | 223.46 | 10.70 | 0.50 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.50 |
| 728 | 15.67 | 224.13 | 10.70 | 0.54 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | 0.65 |
| 732 | 11.82 | 224.59 | 10.70 | 0.56 | 1.29 | ---- | ---- | ---- | ---- | ---- | ---- | 1.85 |
| 736 | 8.58 | 224.86 | 10.70 | 0.57 | 2.27 | ---- | ---- | ---- | ---- | ---- | ---- | 2.84 |
| 740 | 7.01 | 225.03 | 10.70 | 0.58 | 2.75 | ---- | ---- | ---- | ---- | ---- | ---- | 3.33 |
| 744 | 5.90 | 225.14 | 10.70 | 0.59 | 3.02 | ---- | ---- | ---- | ---- | ---- | ---- | 3.60 |
| 748 | 4.76 | 225.20 | 10.70 | 0.59 | 3.16 | ---- | ---- | ---- | ---- | ---- | ---- | 3.75 |
| 752 | 3.63 | 225.21 << | 10.70 | 0.59 | 3.19 | ---- | 0.01 | ---- | ---- | ---- | ---- | 3.80 << |
| 756 | 2.76 | 225.19 | 10.70 | 0.59 | 3.14 | ---- | ---- | ---- | ---- | ---- | ---- | 3.73 |
| 760 | 2.34 | 225.15 | 10.70 | 0.59 | 3.04 | ---- | ---- | ---- | ---- | ---- | ---- | 3.63 |
| 764 | 2.15 | 225.10 | 10.70 | 0.58 | 2.92 | ---- | ---- | ---- | ---- | ---- | ---- | 3.51 |
| 768 | 2.03 | 225.05 | 10.70 | 0.58 | 2.80 | ---- | ---- | ---- | ---- | ---- | ---- | 3.39 |
| 772 | 1.91 | 225.00 | 10.70 | 0.58 | 2.68 | ---- | ---- | ---- | ---- | ---- | ---- | 3.26 |
| 776 | 1.79 | 224.96 | 10.70 | 0.58 | 2.54 | ---- | ---- | ---- | ---- | ---- | ---- | 3.12 |
| 780 | 1.67 | 224.91 | 10.70 | 0.57 | 2.40 | ---- | ---- | ---- | ---- | ---- | ---- | 2.97 |
| 784 | 1.56 | 224.86 | 10.70 | 0.57 | 2.26 | ---- | ---- | ---- | ---- | ---- | ---- | 2.83 |
| 788 | 1.48 | 224.82 | 10.70 | 0.57 | 2.12 | ---- | ---- | ---- | ---- | ---- | ---- | 2.69 |
| 792 | 1.44 | 224.77 | 10.70 | 0.57 | 1.98 | ---- | ---- | ---- | ---- | ---- | ---- | 2.55 |
| 796 | 1.40 | 224.74 | 10.70 | 0.57 | 1.84 | ---- | ---- | ---- | ---- | ---- | ---- | 2.41 |
| 800 | 1.37 | 224.70 | 10.70 | 0.56 | 1.71 | ---- | ---- | ---- | ---- | ---- | ---- | 2.28 |
| 804 | 1.34 | 224.67 | 10.70 | 0.56 | 1.60 | ---- | ---- | ---- | ---- | ---- | ---- | 2.16 |
| 808 | 1.31 | 224.64 | 10.70 | 0.56 | 1.49 | ---- | ---- | ---- | ---- | ---- | ---- | 2.06 |
| 812 | 1.28 | 224.62 | 10.70 | 0.56 | 1.40 | ---- | ---- | ---- | ---- | ---- | ---- | 1.96 |
| 816 | 1.25 | 224.59 | 10.70 | 0.56 | 1.31 | ---- | ---- | ---- | ---- | ---- | ---- | 1.87 |
| 820 | 1.22 | 224.57 | 10.70 | 0.56 | 1.24 | ---- | ---- | ---- | ---- | ---- | ---- | 1.80 |
| 824 | 1.18 | 224.55 | 10.70 | 0.56 | 1.17 | ---- | ---- | ---- | ---- | ---- | ---- | 1.72 |
| 828 | 1.15 | 224.53 | 10.70 | 0.56 | 1.10 | ---- | ---- | ---- | ---- | ---- | ---- | 1.66 |
| 832 | 1.12 | 224.51 | 10.70 | 0.55 | 1.04 | ---- | ---- | ---- | ---- | ---- | ---- | 1.59 |
| 836 | 1.09 | 224.50 | 10.70 | 0.55 | 0.98 | ---- | ---- | ---- | ---- | ---- | ---- | 1.53 |
| 840 | 1.06 | 224.48 | 10.70 | 0.55 | 0.92 | ---- | ---- | ---- | ---- | ---- | ---- | 1.48 |
| 844 | 1.03 | 224.47 | 10.70 | 0.55 | 0.87 | ---- | ---- | ---- | ---- | ---- | ---- | 1.42 |
| 848 | 1.00 | 224.45 | 10.70 | 0.55 | 0.82 | ---- | ---- | ---- | ---- | ---- | ---- | 1.37 |
| 852 | 0.98 | 224.44 | 10.70 | 0.55 | 0.78 | ---- | ---- | ---- | ---- | ---- | ---- | 1.33 |

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Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 856 | 0.97 | 224.43 | 10.70 | 0.55 | 0.74 | ---- | ---- | ---- | ---- | ---- | ---- | 1.29 |
| 860 | 0.95 | 224.42 | 10.70 | 0.55 | 0.70 | ---- | ---- | ---- | ---- | ---- | ---- | 1.25 |
| 864 | 0.94 | 224.41 | 10.70 | 0.55 | 0.66 | ---- | ---- | ---- | ---- | ---- | ---- | 1.21 |
| 868 | 0.92 | 224.40 | 10.70 | 0.55 | 0.63 | ---- | ---- | ---- | ---- | ---- | ---- | 1.18 |
| 872 | 0.91 | 224.39 | 10.70 | 0.55 | 0.61 | ---- | ---- | ---- | ---- | ---- | ---- | 1.16 |
| 876 | 0.89 | 224.38 | 10.70 | 0.55 | 0.59 | ---- | ---- | ---- | ---- | ---- | ---- | 1.14 |
| 880 | 0.88 | 224.37 | 10.70 | 0.55 | 0.57 | ---- | ---- | ---- | ---- | ---- | ---- | 1.12 |
| 884 | 0.86 | 224.36 | 10.70 | 0.55 | 0.55 | ---- | ---- | ---- | ---- | ---- | ---- | 1.10 |
| 888 | 0.85 | 224.35 | 10.70 | 0.55 | 0.53 | ---- | ---- | ---- | ---- | ---- | ---- | 1.08 |
| 892 | 0.83 | 224.35 | 10.70 | 0.55 | 0.51 | ---- | ---- | ---- | ---- | ---- | ---- | 1.06 |
| 896 | 0.82 | 224.34 | 10.70 | 0.55 | 0.49 | ---- | ---- | ---- | ---- | ---- | ---- | 1.04 |
| 900 | 0.80 | 224.33 | 10.70 | 0.55 | 0.47 | ---- | ---- | ---- | ---- | ---- | ---- | 1.02 |
| 904 | 0.78 | 224.32 | 10.70 | 0.55 | 0.46 | ---- | ---- | ---- | ---- | ---- | ---- | 1.00 |
| 908 | 0.77 | 224.31 | 10.70 | 0.54 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | 0.98 |
| 912 | 0.75 | 224.31 | 10.70 | 0.54 | 0.42 | ---- | ---- | ---- | ---- | ---- | ---- | 0.96 |
| 916 | 0.74 | 224.30 | 10.70 | 0.54 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | 0.95 |
| 920 | 0.72 | 224.29 | 10.70 | 0.54 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | 0.93 |
| 924 | 0.71 | 224.28 | 10.70 | 0.54 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | 0.91 |
| 928 | 0.69 | 224.28 | 10.70 | 0.54 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | 0.89 |
| 932 | 0.68 | 224.27 | 10.70 | 0.54 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | 0.88 |
| 936 | 0.66 | 224.26 | 10.70 | 0.54 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | 0.86 |
| 940 | 0.64 | 224.25 | 10.70 | 0.54 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | 0.84 |
| 944 | 0.63 | 224.25 | 10.70 | 0.54 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | 0.83 |
| 948 | 0.61 | 224.24 | 10.70 | 0.54 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | 0.81 |
| 952 | 0.60 | 224.23 | 10.70 | 0.54 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | 0.79 |
| 956 | 0.58 | 224.23 | 10.70 | 0.54 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | 0.78 |
| 960 | 0.57 | 224.22 | 10.70 | 0.54 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | 0.76 |
| 964 | 0.55 | 224.21 | 10.70 | 0.54 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | 0.74 |
| 968 | 0.54 | 224.20 | 10.70 | 0.54 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | 0.73 |
| 972 | 0.53 | 224.20 | 10.70 | 0.54 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | 0.71 |
| 976 | 0.52 | 224.19 | 10.70 | 0.54 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | 0.71 |
| 980 | 0.52 | 224.18 | 10.70 | 0.54 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | 0.70 |
| 984 | 0.51 | 224.18 | 10.70 | 0.54 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | 0.70 |
| 988 | 0.50 | 224.17 | 10.70 | 0.54 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | 0.69 |
| 992 | 0.50 | 224.16 | 10.70 | 0.54 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | 0.68 |
| 996 | 0.49 | 224.16 | 10.70 | 0.54 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | 0.68 |
| 1000 | 0.48 | 224.15 | 10.70 | 0.54 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | 0.67 |
| 1004 | 0.48 | 224.14 | 10.70 | 0.54 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | 0.66 |
| 1008 | 0.47 | 224.14 | 10.70 | 0.54 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | 0.66 |
| 1012 | 0.46 | 224.13 | 10.70 | 0.54 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | 0.65 |
| 1016 | 0.46 | 224.12 | 10.70 | 0.53 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | 0.64 |
| 1020 | 0.45 | 224.12 | 10.70 | 0.53 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | 0.64 |
| 1024 | 0.44 | 224.11 | 10.70 | 0.53 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | 0.63 |
| 1028 | 0.44 | 224.10 | 10.70 | 0.53 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | 0.63 |
| 1032 | 0.43 | 224.10 | 10.70 | 0.53 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | 0.62 |
| 1036 | 0.42 | 224.09 | 10.70 | 0.53 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | 0.61 |
| 1040 | 0.41 | 224.08 | 10.70 | 0.53 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | 0.61 |
| 1044 | 0.41 | 224.08 | 10.70 | 0.53 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | 0.60 |
| 1048 | 0.40 | 224.07 | 10.70 | 0.53 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | 0.59 |
| 1052 | 0.39 | 224.06 | 10.70 | 0.53 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | 0.59 |
| 1056 | 0.39 | 224.05 | 10.70 | 0.53 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | 0.58 |

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Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 1060 | 0.38 | 224.05 | 10.70 | 0.53 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | 0.57 |
| 1064 | 0.37 | 224.04 | 10.70 | 0.53 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | 0.57 |
| 1068 | 0.37 | 224.03 | 10.70 | 0.53 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | 0.56 |
| 1072 | 0.36 | 224.03 | 10.70 | 0.53 | 0.02 | ---- | ---- | ---- | ---- | ---- | ---- | 0.55 |
| 1076 | 0.35 | 224.02 | 10.70 | 0.53 | 0.02 | ---- | ---- | ---- | ---- | ---- | ---- | 0.55 |
| 1080 | 0.35 | 224.01 | 10.70 | 0.53 | 0.01 | ---- | ---- | ---- | ---- | ---- | ---- | 0.54 |
| 1084 | 0.34 | 224.01 | 10.70 | 0.53 | 0.00 | ---- | ---- | ---- | ---- | ---- | ---- | 0.53 |
| 1088 | 0.33 | 224.00 | 10.70 | 0.53 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.53 |
| 1092 | 0.33 | 223.99 | 10.70 | 0.53 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.53 |
| 1096 | 0.33 | 223.98 | 10.70 | 0.53 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.53 |
| 1100 | 0.33 | 223.97 | 10.70 | 0.53 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.53 |
| 1104 | 0.33 | 223.96 | 10.70 | 0.53 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.53 |
| 1108 | 0.32 | 223.95 | 10.70 | 0.53 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.53 |
| 1112 | 0.32 | 223.94 | 10.70 | 0.53 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.53 |
| 1116 | 0.32 | 223.94 | 10.70 | 0.52 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.52 |
| 1120 | 0.32 | 223.93 | 10.70 | 0.52 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.52 |
| 1124 | 0.32 | 223.92 | 10.70 | 0.52 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.52 |
| 1128 | 0.31 | 223.91 | 10.70 | 0.52 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.52 |
| 1132 | 0.31 | 223.90 | 10.70 | 0.52 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.52 |
| 1136 | 0.31 | 223.89 | 10.70 | 0.52 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.52 |
| 1140 | 0.31 | 223.88 | 10.70 | 0.52 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.52 |
| 1144 | 0.31 | 223.87 | 10.70 | 0.52 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.52 |
| 1148 | 0.30 | 223.86 | 10.70 | 0.52 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.52 |
| 1152 | 0.30 | 223.85 | 10.70 | 0.52 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.52 |
| 1156 | 0.30 | 223.84 | 10.70 | 0.52 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.52 |
| 1160 | 0.30 | 223.83 | 10.70 | 0.52 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.52 |
| 1164 | 0.29 | 223.82 | 10.70 | 0.52 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.52 |
| 1168 | 0.29 | 223.81 | 10.70 | 0.52 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.52 |
| 1172 | 0.29 | 223.80 | 10.70 | 0.52 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.52 |
| 1176 | 0.29 | 223.79 | 10.70 | 0.52 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.52 |
| 1180 | 0.29 | 223.78 | 10.70 | 0.52 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.52 |
| 1184 | 0.28 | 223.77 | 10.70 | 0.52 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.52 |
| 1188 | 0.28 | 223.76 | 10.70 | 0.52 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.52 |
| 1192 | 0.28 | 223.75 | 10.70 | 0.51 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.51 |
| 1196 | 0.28 | 223.74 | 10.70 | 0.51 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.51 |
| 1200 | 0.28 | 223.73 | 10.70 | 0.51 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.51 |
| 1204 | 0.27 | 223.72 | 10.70 | 0.51 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.51 |
| 1208 | 0.27 | 223.71 | 10.70 | 0.51 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.51 |
| 1212 | 0.27 | 223.70 | 10.70 | 0.51 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.51 |
| 1216 | 0.27 | 223.68 | 10.70 | 0.51 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.51 |
| 1220 | 0.27 | 223.67 | 10.70 | 0.51 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.51 |
| 1224 | 0.26 | 223.66 | 10.70 | 0.51 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.51 |
| 1228 | 0.26 | 223.65 | 10.70 | 0.51 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.51 |
| 1232 | 0.26 | 223.64 | 10.70 | 0.51 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.51 |
| 1236 | 0.26 | 223.63 | 10.70 | 0.51 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.51 |
| 1240 | 0.26 | 223.62 | 10.70 | 0.51 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.51 |
| 1244 | 0.25 | 223.61 | 10.70 | 0.51 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.51 |
| 1248 | 0.25 | 223.60 | 10.70 | 0.51 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.51 |
| 1252 | 0.25 | 223.58 | 10.70 | 0.51 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.51 |
| 1256 | 0.25 | 223.57 | 10.70 | 0.51 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.51 |
| 1260 | 0.25 | 223.56 | 10.70 | 0.50 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.50 |

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Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 1264 | 0.24 | 223.55 | 10.70 | 0.50 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.50 |
| 1268 | 0.24 | 223.54 | 10.70 | 0.50 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.50 |
| 1272 | 0.24 | 223.53 | 10.70 | 0.50 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.50 |
| 1276 | 0.24 | 223.51 | 10.70 | 0.50 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.50 |
| 1280 | 0.23 | 223.50 | 10.70 | 0.50 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.50 |
| 1284 | 0.23 | 223.49 | 10.70 | 0.50 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.50 |
| 1288 | 0.23 | 223.48 | 10.70 | 0.50 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.50 |
| 1292 | 0.23 | 223.47 | 10.70 | 0.50 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.50 |
| 1296 | 0.23 | 223.45 | 10.70 | 0.50 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.50 |
| 1300 | 0.22 | 223.44 | 10.70 | 0.50 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.50 |
| 1304 | 0.22 | 223.43 | 10.70 | 0.50 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.50 |
| 1308 | 0.22 | 223.42 | 10.70 | 0.50 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.50 |
| 1312 | 0.22 | 223.40 | 10.70 | 0.50 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.50 |
| 1316 | 0.22 | 223.39 | 10.70 | 0.50 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.50 |
| 1320 | 0.21 | 223.38 | 10.70 | 0.49 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.49 |
| 1324 | 0.30 | 223.37 | 10.70 | 0.49 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.49 |
| 1328 | 0.31 | 223.36 | 10.70 | 0.49 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.49 |
| 1332 | 0.27 | 223.35 | 10.70 | 0.49 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.49 |
| 1336 | 0.22 | 223.34 | 10.70 | 0.49 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.49 |
| 1340 | 0.22 | 223.33 | 10.70 | 0.49 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.49 |
| 1344 | 0.22 | 223.32 | 10.70 | 0.49 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.49 |
| 1348 | 0.22 | 223.31 | 10.70 | 0.49 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.49 |
| 1352 | 0.22 | 223.29 | 10.70 | 0.49 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.49 |
| 1356 | 0.21 | 223.28 | 10.70 | 0.49 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.49 |
| 1360 | 0.21 | 223.27 | 10.70 | 0.49 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.49 |
| 1364 | 0.21 | 223.26 | 10.70 | 0.49 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.49 |
| 1368 | 0.21 | 223.24 | 10.70 | 0.49 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.49 |
| 1372 | 0.21 | 223.23 | 10.70 | 0.49 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.49 |
| 1376 | 0.21 | 223.22 | 10.70 | 0.49 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.49 |
| 1380 | 0.21 | 223.21 | 10.70 | 0.48 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.48 |
| 1384 | 0.20 | 223.19 | 10.70 | 0.48 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.48 |
| 1388 | 0.20 | 223.18 | 10.70 | 0.48 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.48 |
| 1392 | 0.20 | 223.17 | 10.70 | 0.48 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.48 |
| 1396 | 0.20 | 223.16 | 10.70 | 0.48 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.48 |
| 1400 | 0.20 | 223.14 | 10.70 | 0.48 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.48 |
| 1404 | 0.20 | 223.13 | 10.70 | 0.48 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.48 |
| 1408 | 0.19 | 223.12 | 10.70 | 0.48 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.48 |
| 1412 | 0.19 | 223.11 | 10.70 | 0.48 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.48 |
| 1416 | 0.19 | 223.09 | 10.70 | 0.48 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.48 |
| 1420 | 0.19 | 223.08 | 10.70 | 0.48 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.48 |
| 1424 | 0.19 | 223.07 | 10.70 | 0.48 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.48 |
| 1428 | 0.19 | 223.05 | 10.70 | 0.48 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.48 |
| 1432 | 0.19 | 223.04 | 10.70 | 0.48 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.48 |
| 1436 | 0.18 | 223.03 | 10.70 | 0.47 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.47 |
| 1440 | 0.18 | 223.02 | 10.70 | 0.47 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.47 |
| 1444 | 0.13 | 223.00 | 10.70 | 0.47 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.47 |
| 1448 | 0.05 | 222.98 | 10.70 | 0.47 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.47 |
| 1452 | 0.01 | 222.96 | 10.70 | 0.47 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.47 |
| 1456 | 0.00 | 222.94 | 10.70 | 0.47 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.47 |
| 1460 | 0.00 | 222.92 | 10.70 | 0.47 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.47 |
| 1464 | 0.00 | 222.90 | 10.70 | 0.47 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.47 |

Continues on next page...

Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 1468 | 0.00 | 222.88 | 10.70 | 0.47 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.47 |
| 1472 | 0.00 | 222.86 | 10.70 | 0.46 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.46 |
| 1476 | 0.00 | 222.84 | 10.70 | 0.46 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.46 |
| 1480 | 0.00 | 222.82 | 10.70 | 0.46 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.46 |
| 1484 | 0.00 | 222.80 | 10.70 | 0.46 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.46 |
| 1488 | 0.00 | 222.78 | 10.70 | 0.46 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.46 |
| 1492 | 0.00 | 222.76 | 10.70 | 0.46 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.46 |
| 1496 | 0.00 | 222.74 | 10.70 | 0.46 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.46 |
| 1500 | 0.00 | 222.72 | 10.70 | 0.46 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.46 |
| 1504 | 0.00 | 222.70 | 10.70 | 0.45 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.45 |
| 1508 | 0.00 | 222.68 | 10.70 | 0.45 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.45 |
| 1512 | 0.00 | 222.66 | 10.70 | 0.45 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.45 |
| 1516 | 0.00 | 222.64 | 10.70 | 0.45 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.45 |
| 1520 | 0.00 | 222.62 | 10.70 | 0.45 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.45 |
| 1524 | 0.00 | 222.60 | 10.70 | 0.45 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.45 |
| 1528 | 0.00 | 222.58 | 10.70 | 0.45 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.45 |
| 1532 | 0.00 | 222.56 | 10.70 | 0.45 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.45 |
| 1536 | 0.00 | 222.54 | 10.70 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.44 |
| 1540 | 0.00 | 222.52 | 10.70 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.44 |
| 1544 | 0.00 | 222.50 | 10.70 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.44 |
| 1548 | 0.00 | 222.48 | 10.70 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.44 |
| 1552 | 0.00 | 222.46 | 10.70 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.44 |
| 1556 | 0.00 | 222.44 | 10.70 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.44 |
| 1560 | 0.00 | 222.42 | 10.70 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.44 |
| 1564 | 0.00 | 222.40 | 10.70 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.44 |
| 1568 | 0.00 | 222.38 | 10.70 | 0.43 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.43 |
| 1572 | 0.00 | 222.36 | 10.70 | 0.43 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.43 |
| 1576 | 0.00 | 222.34 | 10.70 | 0.43 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.43 |
| 1580 | 0.00 | 222.32 | 10.70 | 0.43 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.43 |
| 1584 | 0.00 | 222.30 | 10.70 | 0.43 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.43 |
| 1588 | 0.00 | 222.28 | 10.70 | 0.43 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.43 |
| 1592 | 0.00 | 222.26 | 10.70 | 0.43 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.43 |
| 1596 | 0.00 | 222.24 | 10.70 | 0.43 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.43 |
| 1600 | 0.00 | 222.23 | 10.70 | 0.42 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.42 |
| 1604 | 0.00 | 222.21 | 10.70 | 0.42 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.42 |
| 1608 | 0.00 | 222.19 | 10.70 | 0.42 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.42 |
| 1612 | 0.00 | 222.17 | 10.70 | 0.42 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.42 |
| 1616 | 0.00 | 222.15 | 10.70 | 0.42 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.42 |
| 1620 | 0.00 | 222.13 | 10.70 | 0.42 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.42 |
| 1624 | 0.00 | 222.11 | 10.70 | 0.42 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.42 |
| 1628 | 0.00 | 222.09 | 10.70 | 0.42 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.42 |
| 1632 | 0.00 | 222.08 | 10.70 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.41 |
| 1636 | 0.00 | 222.06 | 10.70 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.41 |
| 1640 | 0.00 | 222.04 | 10.70 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.41 |
| 1644 | 0.00 | 222.02 | 10.70 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.41 |
| 1648 | 0.00 | 222.00 | 10.70 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.41 |
| 1652 | 0.00 | 221.97 | 10.70 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.41 |
| 1656 | 0.00 | 221.94 | 10.70 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.41 |
| 1660 | 0.00 | 221.91 | 10.70 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 1664 | 0.00 | 221.88 | 10.70 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 1668 | 0.00 | 221.85 | 10.70 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |

Continues on next page...

Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 1672 | 0.00 | 221.82 | 10.70 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 1676 | 0.00 | 221.78 | 10.70 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1680 | 0.00 | 221.75 | 10.70 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1684 | 0.00 | 221.72 | 10.70 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1688 | 0.00 | 221.69 | 10.70 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1692 | 0.00 | 221.66 | 10.70 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1696 | 0.00 | 221.63 | 10.70 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1700 | 0.00 | 221.60 | 10.70 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |

...End

Reservoir Report

Reservoir No. 3 - Basin 3 (Hotel)

Hydraflow Hydrographs by Intelisolve

Pond Data

Pond storage is based on known contour areas. Average end area method used.

Stage / Storage Table

| Stage (ft) | Elevation (ft) | Contour area (sqft) | Incr. Storage (cuft) | Total storage (cuft) |
|------------|----------------|---------------------|----------------------|----------------------|
| 0.00 | 219.00 | 00 | 0 | 0 |
| 1.00 | 220.00 | 1,406 | 703 | 703 |
| 3.00 | 222.00 | 4,776 | 6,182 | 6,885 |
| 5.00 | 224.00 | 5,971 | 10,747 | 17,632 |
| 7.00 | 226.00 | 7,278 | 13,249 | 30,881 |
| 9.00 | 228.00 | 8,709 | 15,987 | 46,868 |
| 9.50 | 228.50 | 9,086 | 4,449 | 51,317 |

Culvert / Orifice Structures

| | [A] | [B] | [C] | [D] |
|---------------|----------|--------|--------|------|
| Rise in | = 24.0 | 3.0 | 12.0 | 0.0 |
| Span in | = 24.0 | 3.0 | 12.0 | 0.0 |
| No. Barrels | = 1 | 1 | 1 | 0 |
| Invert El. ft | = 217.50 | 217.90 | 224.00 | 0.00 |
| Length ft | = 48.0 | 1.0 | 1.0 | 0.0 |
| Slope % | = 10.00 | 0.00 | 0.00 | 0.00 |
| N-Value | = .013 | .013 | .013 | .000 |
| Orif. Coeff. | = 0.60 | 0.60 | 0.60 | 0.00 |
| Multi-Stage | = n/a | Yes | Yes | No |

Weir Structures

| | [A] | [B] | [C] | [D] |
|--------------|----------|--------|--------|--------|
| Crest Len ft | = 1.00 | 2.00 | 16.00 | 90.00 |
| Crest El. ft | = 225.25 | 226.00 | 227.00 | 227.00 |
| Weir Coeff. | = 3.33 | 3.33 | 3.33 | 2.60 |
| Weir Type | = Rect | Rect | Rect | Broad |
| Multi-Stage | = Yes | Yes | Yes | Yes |

Exfiltration Rate = 0.00 in/hr/sqft Tailwater Elev. = 0.00 ft

Note: All outflows have been analyzed under inlet and outlet control.

Stage / Storage / Discharge Table

| Stage ft | Storage cuft | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Total cfs |
|----------|--------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-----------|
| 0.00 | 0 | 219.00 | 0.00 | 0.00 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.00 |
| 0.10 | 70 | 219.10 | 10.70 | 0.07 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.07 |
| 0.20 | 141 | 219.20 | 10.70 | 0.11 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.11 |
| 0.30 | 211 | 219.30 | 10.70 | 0.13 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.13 |
| 0.40 | 281 | 219.40 | 10.70 | 0.15 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.15 |
| 0.50 | 352 | 219.50 | 10.70 | 0.17 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.17 |
| 0.60 | 422 | 219.60 | 10.70 | 0.18 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.18 |
| 0.70 | 492 | 219.70 | 10.70 | 0.20 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.20 |
| 0.80 | 562 | 219.80 | 10.70 | 0.21 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.21 |
| 0.90 | 633 | 219.90 | 10.70 | 0.22 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.22 |
| 1.00 | 703 | 220.00 | 10.70 | 0.24 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.24 |
| 1.20 | 1,321 | 220.20 | 10.70 | 0.26 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.26 |
| 1.40 | 1,939 | 220.40 | 10.70 | 0.28 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.28 |
| 1.60 | 2,558 | 220.60 | 10.70 | 0.30 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.30 |
| 1.80 | 3,176 | 220.80 | 10.70 | 0.32 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.32 |
| 2.00 | 3,794 | 221.00 | 10.70 | 0.33 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.33 |
| 2.20 | 4,412 | 221.20 | 10.70 | 0.35 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.35 |
| 2.40 | 5,030 | 221.40 | 10.70 | 0.37 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.37 |
| 2.60 | 5,649 | 221.60 | 10.70 | 0.38 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.38 |
| 2.80 | 6,267 | 221.80 | 10.70 | 0.40 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.40 |
| 3.00 | 6,885 | 222.00 | 10.70 | 0.41 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.41 |
| 3.20 | 7,960 | 222.20 | 10.70 | 0.42 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.42 |
| 3.40 | 9,034 | 222.40 | 10.70 | 0.44 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.44 |
| 3.60 | 10,109 | 222.60 | 10.70 | 0.45 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.45 |
| 3.80 | 11,184 | 222.80 | 10.70 | 0.46 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.46 |
| 4.00 | 12,259 | 223.00 | 10.70 | 0.47 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.47 |
| 4.20 | 13,333 | 223.20 | 10.70 | 0.48 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.48 |
| 4.40 | 14,408 | 223.40 | 10.70 | 0.50 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.50 |
| 4.60 | 15,483 | 223.60 | 10.70 | 0.51 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.51 |
| 4.80 | 16,557 | 223.80 | 10.70 | 0.52 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.52 |
| 5.00 | 17,632 | 224.00 | 10.70 | 0.53 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.53 |

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Stage / Storage / Discharge Table

| Stage ft | Storage cuft | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Total cfs |
|-------------|-----------------|-----------------|--------------|--------------|--------------|--------------|-------------|-------------|-------------|-------------|--------------|--------------|
| 5.20 | 18,957 | 224.20 | 10.70 | 0.54 | 0.18 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.72 |
| 5.40 | 20,282 | 224.40 | 10.70 | 0.55 | 0.64 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 1.19 |
| 5.60 | 21,607 | 224.60 | 10.70 | 0.56 | 1.34 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 1.90 |
| 5.80 | 22,932 | 224.80 | 10.70 | 0.57 | 2.07 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 2.64 |
| 6.00 | 24,257 | 225.00 | 10.70 | 0.58 | 2.67 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 3.25 |
| 6.20 | 25,581 | 225.20 | 10.70 | 0.59 | 3.16 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 3.75 |
| 6.40 | 26,906 | 225.40 | 10.70 | 0.60 | 3.59 | --- | 0.19 | 0.00 | 0.00 | 0.00 | --- | 4.38 |
| 6.60 | 28,231 | 225.60 | 10.70 | 0.61 | 3.97 | --- | 0.69 | 0.00 | 0.00 | 0.00 | --- | 5.26 |
| 6.80 | 29,556 | 225.80 | 10.70 | 0.62 | 4.31 | --- | 1.36 | 0.00 | 0.00 | 0.00 | --- | 6.29 |
| 7.00 | 30,881 | 226.00 | 10.70 | 0.63 | 4.63 | --- | 2.16 | 0.00 | 0.00 | 0.00 | --- | 7.42 |
| 7.20 | 32,480 | 226.20 | 10.70 | 0.63 | 4.93 | --- | 3.08 | 0.60 | 0.00 | 0.00 | --- | 9.24 |
| 7.40 | 34,078 | 226.40 | 11.69 | 0.64 | 5.21 | --- | 4.11 | 1.68 | 0.00 | 0.00 | --- | 11.64 |
| 7.60 | 35,677 | 226.60 | 14.47 | 0.63 | 5.48 | --- | 5.22 | 3.10 | 0.00 | 0.00 | --- | 14.43 |
| 7.80 | 37,276 | 226.80 | 17.55 | 0.62 | 5.73 | --- | 6.43 | 4.77 | 0.00 | 0.00 | --- | 17.55 |
| 8.00 | 38,875 | 227.00 | 20.95 | 0.61 | 5.98 | --- | 7.71 | 6.66 | 0.00 | 0.00 | --- | 20.95 |
| 8.20 | 40,473 | 227.20 | 42.98 | 0.19 | 2.99 | --- | 6.61 | 7.50 | 4.76 | 20.93 | --- | 42.98 |
| 8.40 | 42,072 | 227.40 | 45.00 | 0.05 | 0.84 | --- | 2.87 | 3.56 | 6.98 | 30.65 | --- | 44.96 |
| 8.60 | 43,671 | 227.60 | 45.58 | 0.03 | 0.50 | --- | 2.13 | 2.78 | 7.43 | 32.62 | --- | 45.49 |
| 8.80 | 45,269 | 227.80 | 46.10 | 0.02 | 0.35 | --- | 1.75 | 2.38 | 7.69 | 33.77 | --- | 45.95 |
| 9.00 | 46,868 | 228.00 | 46.61 | 0.02 | 0.26 | --- | 1.53 | 2.14 | 7.90 | 34.69 | --- | 46.53 |
| 9.05 | 47,313 | 228.05 | 46.73 | 0.02 | 0.24 | --- | 1.48 | 2.09 | 7.91 | 34.75 | --- | 46.48 |
| 9.10 | 47,758 | 228.10 | 46.85 | 0.01 | 0.23 | --- | 1.43 | 2.04 | 7.92 | 34.79 | --- | 46.41 |
| 9.15 | 48,203 | 228.15 | 46.98 | 0.01 | 0.21 | --- | 1.39 | 2.00 | 7.95 | 34.93 | --- | 46.50 |
| 9.20 | 48,648 | 228.20 | 47.10 | 0.01 | 0.20 | --- | 1.37 | 1.97 | 8.02 | 35.22 | --- | 46.79 |
| 9.25 | 49,092 | 228.25 | 47.22 | 0.01 | 0.19 | --- | 1.33 | 1.94 | 8.04 | 35.33 | --- | 46.85 |
| 9.30 | 49,537 | 228.30 | 47.34 | 0.01 | 0.18 | --- | 1.30 | 1.89 | 8.01 | 35.19 | --- | 46.59 |
| 9.35 | 49,982 | 228.35 | 47.46 | 0.01 | 0.17 | --- | 1.27 | 1.87 | 8.07 | 35.43 | --- | 46.82 |
| 9.40 | 50,427 | 228.40 | 47.58 | 0.01 | 0.16 | --- | 1.25 | 1.84 | 8.07 | 35.43 | --- | 46.76 |
| 9.45 | 50,872 | 228.45 | 47.70 | 0.01 | 0.16 | --- | 1.24 | 1.84 | 8.21 | 36.07 | --- | 47.54 |
| 9.50 | 51,317 | 228.50 | 47.83 | 0.01 | 0.15 | --- | 1.20 | 1.79 | 8.08 | 35.50 | --- | 46.73 |

...End

Hydrograph Report

Hyd. No. 14

Hydrograph type = Combine
Storm frequency = 50 yrs
Inflow hyds. = 11, 12, 13

Peak discharge = 9.95 cfs
Time interval = 2 min

Hydrograph Volume = 133,908 cuft

Hydrograph Discharge Table

| Time (min) | Hyd. 11 + (cfs) | Hyd. 12 + (cfs) | Hyd. 13 = (cfs) | Outflow (cfs) |
|------------|-----------------|-----------------|-----------------|---------------|
| 716 | 0.22 | 0.38 | 0.44 | 1.10 |
| 720 | 0.24 | 0.67 | 0.47 | 1.55 |
| 724 | 0.27 | 1.22 | 0.50 | 2.40 |
| 728 | 0.30 | 2.10 | 0.65 | 3.76 |
| 732 | 0.33 | 3.12 | 1.85 | 6.32 |
| 736 | 0.35 | 4.01 | 2.84 | 8.39 |
| 740 | 0.36 | 4.63 | 3.33 | 9.49 |
| 744 | 0.38 | 4.91 | 3.60 | 9.92 |
| 748 | 0.39 | 4.93 | 3.75 | 9.89 |
| 752 | 0.39 | 4.80 | 3.80 << | 9.60 |
| 756 | 0.40 | 4.56 | 3.73 | 9.09 |
| 760 | 0.41 | 4.26 | 3.63 | 8.54 |
| 764 | 0.48 | 3.94 | 3.51 | 8.02 |
| 768 | 0.53 | 3.63 | 3.39 | 7.53 |
| 772 | 0.57 | 3.35 | 3.26 | 7.10 |
| 776 | 0.60 | 3.10 | 3.12 | 6.68 |
| 780 | 0.63 | 2.88 | 2.97 | 6.29 |
| 784 | 0.66 | 2.67 | 2.83 | 5.96 |
| 788 | 0.68 | 2.49 | 2.69 | 5.65 |
| 792 | 0.69 | 2.33 | 2.55 | 5.34 |
| 796 | 0.70 | 2.18 | 2.41 | 5.05 |
| 800 | 0.71 | 2.05 | 2.28 | 4.81 |
| 804 | 0.73 | 1.93 | 2.16 | 4.60 |
| 808 | 0.74 | 1.83 | 2.06 | 4.42 |
| 812 | 0.75 | 1.74 | 1.96 | 4.25 |
| 816 | 0.76 | 1.66 | 1.87 | 4.09 |
| 820 | 0.76 | 1.58 | 1.80 | 3.94 |
| 824 | 0.76 << | 1.51 | 1.72 | 3.81 |
| 828 | 0.76 | 1.44 | 1.66 | 3.68 |
| 832 | 0.76 | 1.38 | 1.59 | 3.56 |
| 836 | 0.75 | 1.33 | 1.53 | 3.45 |
| 840 | 0.75 | 1.28 | 1.48 | 3.35 |
| 844 | 0.74 | 1.24 | 1.42 | 3.26 |
| 848 | 0.73 | 1.20 | 1.37 | 3.16 |
| 852 | 0.72 | 1.16 | 1.33 | 3.08 |
| 856 | 0.71 | 1.12 | 1.29 | 2.99 |
| 860 | 0.71 | 1.08 | 1.25 | 2.92 |
| 864 | 0.70 | 1.05 | 1.21 | 2.85 |

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Hydrograph Discharge Table

| Time (min) | Hyd. 11 + (cfs) | Hyd. 12 + (cfs) | Hyd. 13 = (cfs) | Outflow (cfs) |
|---------------|--------------------|--------------------|--------------------|------------------|
| 868 | 0.70 | 1.02 | 1.18 | 2.79 |
| 872 | 0.69 | 0.99 | 1.16 | 2.74 |
| 876 | 0.68 | 0.96 | 1.14 | 2.69 |
| 880 | 0.68 | 0.93 | 1.12 | 2.64 |
| 884 | 0.67 | 0.91 | 1.10 | 2.59 |
| 888 | 0.66 | 0.88 | 1.08 | 2.55 |
| 892 | 0.66 | 0.86 | 1.06 | 2.50 |
| 896 | 0.65 | 0.84 | 1.04 | 2.46 |
| 900 | 0.64 | 0.83 | 1.02 | 2.42 |
| 904 | 0.64 | 0.81 | 1.00 | 2.37 |
| 908 | 0.63 | 0.79 | 0.98 | 2.33 |
| 912 | 0.62 | 0.78 | 0.96 | 2.29 |
| 916 | 0.61 | 0.76 | 0.95 | 2.25 |
| 920 | 0.61 | 0.75 | 0.93 | 2.21 |
| 924 | 0.60 | 0.73 | 0.91 | 2.17 |
| 928 | 0.59 | 0.72 | 0.89 | 2.13 |
| 932 | 0.58 | 0.70 | 0.88 | 2.09 |
| 936 | 0.57 | 0.69 | 0.86 | 2.05 |
| 940 | 0.56 | 0.67 | 0.84 | 2.01 |
| 944 | 0.56 | 0.66 | 0.83 | 1.97 |
| 948 | 0.55 | 0.65 | 0.81 | 1.94 |
| 952 | 0.54 | 0.63 | 0.79 | 1.91 |
| 956 | 0.53 | 0.62 | 0.78 | 1.87 |
| 960 | 0.52 | 0.61 | 0.76 | 1.84 |
| 964 | 0.51 | 0.59 | 0.74 | 1.81 |
| 968 | 0.50 | 0.58 | 0.73 | 1.77 |
| 972 | 0.49 | 0.57 | 0.71 | 1.74 |
| 976 | 0.49 | 0.55 | 0.71 | 1.72 |
| 980 | 0.48 | 0.54 | 0.70 | 1.70 |
| 984 | 0.47 | 0.53 | 0.70 | 1.67 |
| 988 | 0.46 | 0.52 | 0.69 | 1.65 |
| 992 | 0.45 | 0.51 | 0.68 | 1.63 |
| 996 | 0.45 | 0.50 | 0.68 | 1.61 |
| 1000 | 0.44 | 0.49 | 0.67 | 1.59 |
| 1004 | 0.43 | 0.48 | 0.66 | 1.57 |
| 1008 | 0.43 | 0.48 | 0.66 | 1.55 |
| 1012 | 0.42 | 0.47 | 0.65 | 1.53 |
| 1016 | 0.41 | 0.47 | 0.64 | 1.51 |
| 1020 | 0.40 | 0.46 | 0.64 | 1.49 |
| 1024 | 0.40 | 0.45 | 0.63 | 1.47 |
| 1028 | 0.40 | 0.45 | 0.63 | 1.45 |
| 1032 | 0.40 | 0.44 | 0.62 | 1.44 |
| 1036 | 0.40 | 0.44 | 0.61 | 1.43 |
| 1040 | 0.40 | 0.43 | 0.61 | 1.41 |
| 1044 | 0.40 | 0.43 | 0.60 | 1.40 |
| 1048 | 0.40 | 0.42 | 0.59 | 1.39 |
| 1052 | 0.40 | 0.42 | 0.59 | 1.38 |
| 1056 | 0.40 | 0.41 | 0.58 | 1.36 |
| 1060 | 0.40 | 0.41 | 0.57 | 1.35 |
| 1064 | 0.40 | 0.40 | 0.57 | 1.34 |
| 1068 | 0.40 | 0.40 | 0.56 | 1.32 |

Continues on next page...

Hydrograph Discharge Table

| Time (min) | Hyd. 11 + (cfs) | Hyd. 12 + (cfs) | Hyd. 13 = (cfs) | Outflow (cfs) |
|---------------|--------------------|--------------------|--------------------|------------------|
| 1072 | 0.40 | 0.39 | 0.55 | 1.31 |
| 1076 | 0.40 | 0.39 | 0.55 | 1.30 |
| 1080 | 0.40 | 0.38 | 0.54 | 1.29 |
| 1084 | 0.39 | 0.38 | 0.53 | 1.27 |
| 1088 | 0.39 | 0.37 | 0.53 | 1.26 |
| 1092 | 0.39 | 0.36 | 0.53 | 1.26 |
| 1096 | 0.39 | 0.36 | 0.53 | 1.25 |
| 1100 | 0.39 | 0.35 | 0.53 | 1.24 |
| 1104 | 0.39 | 0.35 | 0.53 | 1.24 |
| 1108 | 0.39 | 0.35 | 0.53 | 1.23 |
| 1112 | 0.39 | 0.34 | 0.53 | 1.23 |
| 1116 | 0.39 | 0.34 | 0.52 | 1.22 |
| 1120 | 0.39 | 0.33 | 0.52 | 1.22 |
| 1124 | 0.39 | 0.33 | 0.52 | 1.21 |
| 1128 | 0.39 | 0.32 | 0.52 | 1.21 |
| 1132 | 0.39 | 0.32 | 0.52 | 1.20 |
| 1136 | 0.39 | 0.32 | 0.52 | 1.20 |
| 1140 | 0.39 | 0.31 | 0.52 | 1.19 |
| 1144 | 0.39 | 0.31 | 0.52 | 1.19 |
| 1148 | 0.39 | 0.31 | 0.52 | 1.18 |
| 1152 | 0.39 | 0.30 | 0.52 | 1.18 |
| 1156 | 0.39 | 0.30 | 0.52 | 1.17 |
| 1160 | 0.39 | 0.30 | 0.52 | 1.17 |
| 1164 | 0.39 | 0.29 | 0.52 | 1.17 |
| 1168 | 0.38 | 0.29 | 0.52 | 1.17 |
| 1172 | 0.38 | 0.29 | 0.52 | 1.16 |
| 1176 | 0.38 | 0.28 | 0.52 | 1.16 |
| 1180 | 0.38 | 0.28 | 0.52 | 1.16 |
| 1184 | 0.38 | 0.28 | 0.52 | 1.16 |
| 1188 | 0.38 | 0.27 | 0.52 | 1.16 |
| 1192 | 0.38 | 0.27 | 0.51 | 1.16 |
| 1196 | 0.38 | 0.27 | 0.51 | 1.16 |
| 1200 | 0.38 | 0.27 | 0.51 | 1.15 |
| 1204 | 0.38 | 0.26 | 0.51 | 1.15 |
| 1208 | 0.38 | 0.26 | 0.51 | 1.15 |
| 1212 | 0.38 | 0.26 | 0.51 | 1.15 |
| 1216 | 0.38 | 0.26 | 0.51 | 1.15 |
| 1220 | 0.38 | 0.26 | 0.51 | 1.15 |
| 1224 | 0.38 | 0.26 | 0.51 | 1.14 |
| 1228 | 0.38 | 0.26 | 0.51 | 1.14 |
| 1232 | 0.38 | 0.26 | 0.51 | 1.14 |
| 1236 | 0.38 | 0.26 | 0.51 | 1.14 |
| 1240 | 0.37 | 0.26 | 0.51 | 1.14 |
| 1244 | 0.37 | 0.26 | 0.51 | 1.14 |
| 1248 | 0.37 | 0.26 | 0.51 | 1.13 |
| 1252 | 0.37 | 0.26 | 0.51 | 1.13 |
| 1256 | 0.37 | 0.26 | 0.51 | 1.13 |
| 1260 | 0.37 | 0.26 | 0.50 | 1.13 |
| 1264 | 0.37 | 0.25 | 0.50 | 1.13 |
| 1268 | 0.37 | 0.25 | 0.50 | 1.12 |
| 1272 | 0.37 | 0.25 | 0.50 | 1.12 |

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Hydrograph Discharge Table

| Time (min) | Hyd. 11 + (cfs) | Hyd. 12 + (cfs) | Hyd. 13 = (cfs) | Outflow (cfs) |
|---------------|--------------------|--------------------|--------------------|------------------|
| 1276 | 0.37 | 0.25 | 0.50 | 1.12 |
| 1280 | 0.37 | 0.25 | 0.50 | 1.12 |
| 1284 | 0.37 | 0.25 | 0.50 | 1.12 |
| 1288 | 0.37 | 0.25 | 0.50 | 1.11 |
| 1292 | 0.37 | 0.25 | 0.50 | 1.11 |
| 1296 | 0.37 | 0.25 | 0.50 | 1.11 |
| 1300 | 0.37 | 0.25 | 0.50 | 1.11 |
| 1304 | 0.37 | 0.25 | 0.50 | 1.11 |
| 1308 | 0.36 | 0.25 | 0.50 | 1.11 |
| 1312 | 0.36 | 0.25 | 0.50 | 1.10 |
| 1316 | 0.36 | 0.25 | 0.50 | 1.10 |
| 1320 | 0.36 | 0.24 | 0.49 | 1.10 |
| 1324 | 0.36 | 0.24 | 0.49 | 1.10 |
| 1328 | 0.36 | 0.24 | 0.49 | 1.10 |
| 1332 | 0.36 | 0.24 | 0.49 | 1.09 |
| 1336 | 0.36 | 0.24 | 0.49 | 1.09 |
| 1340 | 0.36 | 0.24 | 0.49 | 1.09 |
| 1344 | 0.36 | 0.24 | 0.49 | 1.09 |
| 1348 | 0.36 | 0.24 | 0.49 | 1.09 |
| 1352 | 0.36 | 0.24 | 0.49 | 1.09 |
| 1356 | 0.36 | 0.24 | 0.49 | 1.08 |
| 1360 | 0.36 | 0.24 | 0.49 | 1.08 |
| 1364 | 0.36 | 0.24 | 0.49 | 1.08 |
| 1368 | 0.36 | 0.24 | 0.49 | 1.08 |
| 1372 | 0.36 | 0.24 | 0.49 | 1.08 |
| 1376 | 0.35 | 0.24 | 0.49 | 1.07 |
| 1380 | 0.35 | 0.24 | 0.48 | 1.07 |
| 1384 | 0.35 | 0.23 | 0.48 | 1.07 |
| 1388 | 0.35 | 0.23 | 0.48 | 1.07 |
| 1392 | 0.35 | 0.23 | 0.48 | 1.06 |
| 1396 | 0.35 | 0.23 | 0.48 | 1.06 |
| 1400 | 0.35 | 0.23 | 0.48 | 1.06 |
| 1404 | 0.35 | 0.23 | 0.48 | 1.06 |
| 1408 | 0.35 | 0.23 | 0.48 | 1.06 |
| 1412 | 0.35 | 0.23 | 0.48 | 1.05 |
| 1416 | 0.35 | 0.23 | 0.48 | 1.05 |
| 1420 | 0.35 | 0.23 | 0.48 | 1.05 |
| 1424 | 0.35 | 0.23 | 0.48 | 1.05 |
| 1428 | 0.35 | 0.23 | 0.48 | 1.04 |
| 1432 | 0.35 | 0.22 | 0.48 | 1.04 |
| 1436 | 0.35 | 0.22 | 0.47 | 1.04 |
| 1440 | 0.34 | 0.22 | 0.47 | 1.04 |
| 1444 | 0.34 | 0.22 | 0.47 | 1.04 |
| 1448 | 0.34 | 0.22 | 0.47 | 1.03 |
| 1452 | 0.34 | 0.22 | 0.47 | 1.03 |
| 1456 | 0.34 | 0.22 | 0.47 | 1.03 |
| 1460 | 0.34 | 0.22 | 0.47 | 1.02 |
| 1464 | 0.34 | 0.21 | 0.47 | 1.02 |
| 1468 | 0.34 | 0.21 | 0.47 | 1.01 |
| 1472 | 0.34 | 0.21 | 0.46 | 1.01 |
| 1476 | 0.34 | 0.21 | 0.46 | 1.00 |

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Hydrograph Discharge Table

| Time (min) | Hyd. 11 + (cfs) | Hyd. 12 + (cfs) | Hyd. 13 = (cfs) | Outflow (cfs) |
|-----------------------|----------------------------|----------------------------|----------------------------|--------------------------|
| 1480 | 0.34 | 0.21 | 0.46 | 1.00 |
| 1484 | 0.33 | 0.20 | 0.46 | 1.00 |

...End

Hydrograph Summary Report

| Hyd. No. | Hydrograph type (origin) | Peak flow (cfs) | Time interval (min) | Time to peak (min) | Volume (cuft) | Inflow hyd(s) | Maximum elevation (ft) | Maximum storage (cuft) | Hydrograph description |
|----------|--------------------------|-----------------|---------------------|--------------------|---------------|---------------|------------------------|------------------------|------------------------|
| 1 | SCS Runoff | 20.55 | 2 | 732 | 85,479 | --- | --- | --- | Predevelopment |
| 2 | SCS Runoff | 10.02 | 2 | 728 | 39,402 | --- | --- | --- | Post Subarea 1a |
| 3 | SCS Runoff | 0.91 | 2 | 724 | 2,783 | --- | --- | --- | Post Subarea 1b |
| 4 | SCS Runoff | 11.39 | 2 | 730 | 48,324 | --- | --- | --- | Post Subarea 2a |
| 5 | SCS Runoff | 0.88 | 2 | 724 | 2,683 | --- | --- | --- | Post Subarea 2b |
| 6 | SCS Runoff | 18.02 | 2 | 726 | 63,345 | --- | --- | --- | Post Subarea 3a |
| 7 | SCS Runoff | 1.14 | 2 | 724 | 3,478 | --- | --- | --- | Post Subarea 3b |
| 8 | Combine | 10.71 | 2 | 728 | 42,185 | 2, 3, | --- | --- | Basin 1 In |
| 9 | Combine | 11.93 | 2 | 730 | 51,007 | 4, 5, | --- | --- | Basin 2 In |
| 10 | Combine | 19.08 | 2 | 726 | 66,824 | 6, 7, | --- | --- | Basin 3 In |
| 11 | Reservoir | 1.50 | 2 | 770 | 41,596 | 8 | 243.46 | 34,262 | Basin 1 Out |
| 12 | Reservoir | 6.27 | 2 | 744 | 47,691 | 9 | 233.92 | 20,659 | Basin 2 Out |
| 13 | Reservoir | 5.59 | 2 | 748 | 66,824 | 10 | 225.66 | 28,658 | Basin 3 Out |
| 14 | Combine | 13.56 | 2 | 746 | 156,118 | 11, 12, 13 | --- | --- | |

Proj. file: ansuya.basin.9-30-04.gpw Return Period: 100 yr

Run date: 10-08-2004

Hydrograph Report

Hyd. No. 1

Predevelopment

| | | | | | |
|-----------------|---|------------|--------------------|---|-----------|
| Hydrograph type | = | SCS Runoff | Peak discharge | = | 20.55 cfs |
| Storm frequency | = | 100 yrs | Time interval | = | 2 min |
| Drainage area | = | 8.27 ac | Curve number | = | 61 |
| Basin Slope | = | 0.0 % | Hydraulic length | = | 0 ft |
| Tc method | = | USER | Time of conc. (Tc) | = | 14.4 min |
| Total precip. | = | 7.30 in | Distribution | = | Type III |
| Storm duration | = | 24 hrs | Shape factor | = | 484 |

Hydrograph Volume = 85,479 cuft

Hydrograph Discharge Table

| Time -- Outflow (min cfs) | Time -- Outflow (min cfs) | Time -- Outflow (min cfs) |
|-----------------------------------|-----------------------------------|-----------------------------------|
| 686 1.08 | 822 2.35 | 958 1.17 |
| 690 1.21 | 826 2.29 | 962 1.14 |
| 694 1.39 | 830 2.23 | 966 1.11 |
| 698 1.70 | 834 2.18 | 970 1.09 |
| 702 2.26 | 838 2.12 | 974 1.07 |
| 706 3.12 | 842 2.06 | 978 1.05 |
| 710 4.27 | 846 2.01 | 982 1.04 |
| 714 5.70 | 850 1.96 | |
| 718 7.81 | 854 1.92 | |
| 722 11.88 | 858 1.89 | ...End |
| 726 17.13 | 862 1.86 | |
| 730 20.41 | 866 1.83 | |
| 734 19.95 | 870 1.81 | |
| 738 17.68 | 874 1.78 | |
| 742 14.66 | 878 1.75 | |
| 746 11.76 | 882 1.72 | |
| 750 9.68 | 886 1.70 | |
| 754 7.87 | 890 1.67 | |
| 758 6.25 | 894 1.64 | |
| 762 5.07 | 898 1.61 | |
| 766 4.33 | 902 1.58 | |
| 770 3.91 | 906 1.56 | |
| 774 3.66 | 910 1.53 | |
| 778 3.45 | 914 1.50 | |
| 782 3.24 | 918 1.47 | |
| 786 3.04 | 922 1.44 | |
| 790 2.88 | 926 1.41 | |
| 794 2.76 | 930 1.38 | |
| 798 2.68 | 934 1.35 | |
| 802 2.61 | 938 1.32 | |
| 806 2.56 | 942 1.29 | |
| 810 2.51 | 946 1.26 | |
| 814 2.45 | 950 1.23 | |
| 818 2.40 | 954 1.20 | |

Hydrograph Report

Hyd. No. 2

Post Subarea 1a

| | | | |
|-----------------|--------------|--------------------|-------------|
| Hydrograph type | = SCS Runoff | Peak discharge | = 10.02 cfs |
| Storm frequency | = 100 yrs | Time interval | = 2 min |
| Drainage area | = 1.90 ac | Curve number | = 85 |
| Basin Slope | = 0.0 % | Hydraulic length | = 0 ft |
| Tc method | = USER | Time of conc. (Tc) | = 10.6 min |
| Total precip. | = 7.30 in | Distribution | = Type III |
| Storm duration | = 24 hrs | Shape factor | = 484 |

Hydrograph Volume = 39,402 cuft

Hydrograph Discharge Table

| Time (min) | Outflow (cfs) | Time (min) | Outflow (cfs) | Time (min) | Outflow (cfs) |
|------------|---------------|------------|---------------|------------|---------------|
| 626 | 0.51 | 762 | 1.67 | 898 | 0.54 |
| 630 | 0.53 | 766 | 1.47 | 902 | 0.53 |
| 634 | 0.55 | 770 | 1.37 | 906 | 0.52 |
| 638 | 0.57 | 774 | 1.29 | 910 | 0.51 |
| 642 | 0.59 | 778 | 1.21 | | |
| 646 | 0.61 | 782 | 1.13 | | |
| 650 | 0.63 | 786 | 1.05 | ...End | |
| 654 | 0.66 | 790 | 1.00 | | |
| 658 | 0.68 | 794 | 0.96 | | |
| 662 | 0.70 | 798 | 0.94 | | |
| 666 | 0.73 | 802 | 0.92 | | |
| 670 | 0.77 | 806 | 0.89 | | |
| 674 | 0.83 | 810 | 0.87 | | |
| 678 | 0.90 | 814 | 0.85 | | |
| 682 | 0.97 | 818 | 0.83 | | |
| 686 | 1.05 | 822 | 0.81 | | |
| 690 | 1.12 | 826 | 0.79 | | |
| 694 | 1.24 | 830 | 0.77 | | |
| 698 | 1.48 | 834 | 0.75 | | |
| 702 | 1.92 | 838 | 0.72 | | |
| 706 | 2.52 | 842 | 0.70 | | |
| 710 | 3.22 | 846 | 0.68 | | |
| 714 | 3.96 | 850 | 0.67 | | |
| 718 | 5.04 | 854 | 0.65 | | |
| 722 | 7.26 | 858 | 0.64 | | |
| 726 | 9.60 | 862 | 0.63 | | |
| 730 | 9.82 | 866 | 0.62 | | |
| 734 | 8.38 | 870 | 0.61 | | |
| 738 | 6.57 | 874 | 0.60 | | |
| 742 | 5.03 | 878 | 0.59 | | |
| 746 | 4.10 | 882 | 0.58 | | |
| 750 | 3.33 | 886 | 0.57 | | |
| 754 | 2.60 | 890 | 0.56 | | |
| 758 | 2.02 | 894 | 0.55 | | |

Hydrograph Report

Hyd. No. 3

Post Subarea 1b

Hydrograph type = SCS Runoff
Storm frequency = 100 yrs
Drainage area = 0.28 ac
Basin Slope = 0.0 %
Tc method = USER
Total precip. = 7.30 in
Storm duration = 24 hrs

Peak discharge = 0.91 cfs
Time interval = 2 min
Curve number = 61
Hydraulic length = 0 ft
Time of conc. (Tc) = 6 min
Distribution = Type III
Shape factor = 484

Hydrograph Volume = 2,783 cuft

Hydrograph Discharge Table

| Time -- Outflow (min cfs) | Time -- Outflow (min cfs) |
|------------------------------|------------------------------|
| 690 0.05 | 826 0.07 |
| 694 0.06 | 830 0.07 |
| 698 0.09 | 834 0.07 |
| 702 0.13 | 838 0.07 |
| 706 0.17 | 842 0.06 |
| 710 0.22 | 846 0.06 |
| 714 0.29 | 850 0.06 |
| 718 0.45 | 854 0.06 |
| 722 0.82 | 858 0.06 |
| 726 0.85 | 862 0.06 |
| 730 0.55 | 866 0.06 |
| 734 0.44 | 870 0.06 |
| 738 0.39 | 874 0.06 |
| 742 0.33 | 878 0.06 |
| 746 0.27 | 882 0.05 |
| 750 0.20 | 886 0.05 |
| 754 0.15 | 890 0.05 |
| 758 0.13 | 894 0.05 |
| 762 0.13 | 898 0.05 |
| 766 0.12 | 902 0.05 |
| 770 0.11 | 906 0.05 |
| 774 0.11 | 910 0.05 |
| 778 0.10 | 914 0.05 |
| 782 0.09 | 918 0.05 |
| 786 0.09 | |
| 790 0.09 | |
| 794 0.09 | ...End |
| 798 0.08 | |
| 802 0.08 | |
| 806 0.08 | |
| 810 0.08 | |
| 814 0.08 | |
| 818 0.07 | |
| 822 0.07 | |

Hydrograph Report

Hyd. No. 4

Post Subarea 2a

| | | | |
|-----------------|--------------|--------------------|-------------|
| Hydrograph type | = SCS Runoff | Peak discharge | = 11.39 cfs |
| Storm frequency | = 100 yrs | Time interval | = 2 min |
| Drainage area | = 2.32 ac | Curve number | = 88 |
| Basin Slope | = 0.0 % | Hydraulic length | = 0 ft |
| Tc method | = USER | Time of conc. (Tc) | = 14.5 min |
| Total precip. | = 7.30 in | Distribution | = Type III |
| Storm duration | = 24 hrs | Shape factor | = 484 |

Hydrograph Volume = 48,324 cuft

Hydrograph Discharge Table

| Time -- Outflow (min cfs) | Time -- Outflow (min cfs) | Time -- Outflow (min cfs) |
|-----------------------------------|-----------------------------------|-----------------------------------|
| 612 0.58 | 748 4.90 | 884 0.69 |
| 616 0.60 | 752 3.96 | 888 0.67 |
| 620 0.62 | 756 3.13 | 892 0.66 |
| 624 0.65 | 760 2.47 | 896 0.65 |
| 628 0.67 | 764 2.03 | 900 0.64 |
| 632 0.69 | 768 1.77 | 904 0.62 |
| 636 0.72 | 772 1.63 | 908 0.61 |
| 640 0.74 | 776 1.53 | 912 0.60 |
| 644 0.77 | 780 1.43 | 916 0.59 |
| 648 0.80 | 784 1.34 | 920 0.58 |
| 652 0.82 | 788 1.25 | |
| 656 0.85 | 792 1.19 | |
| 660 0.88 | 796 1.14 | ...End |
| 664 0.90 | 800 1.11 | |
| 668 0.94 | 804 1.08 | |
| 672 1.00 | 808 1.06 | |
| 676 1.07 | 812 1.03 | |
| 680 1.15 | 816 1.01 | |
| 684 1.24 | 820 0.98 | |
| 688 1.33 | 824 0.96 | |
| 692 1.43 | 828 0.93 | |
| 696 1.60 | 832 0.91 | |
| 700 1.92 | 836 0.88 | |
| 704 2.46 | 840 0.85 | |
| 708 3.17 | 844 0.83 | |
| 712 4.00 | 848 0.81 | |
| 716 4.94 | 852 0.79 | |
| 720 6.52 | 856 0.77 | |
| 724 8.99 | 860 0.76 | |
| 728 11.06 | 864 0.75 | |
| 732 11.18 | 868 0.73 | |
| 736 9.82 | 872 0.72 | |
| 740 8.04 | 876 0.71 | |
| 744 6.22 | 880 0.70 | |

Hydrograph Report

Hyd. No. 5

Post Subarea 2b

Hydrograph type = SCS Runoff
Storm frequency = 100 yrs
Drainage area = 0.27 ac
Basin Slope = 0.0 %
Tc method = USER
Total precip. = 7.30 in
Storm duration = 24 hrs

Peak discharge = 0.88 cfs
Time interval = 2 min
Curve number = 61
Hydraulic length = 0 ft
Time of conc. (Tc) = 6 min
Distribution = Type III
Shape factor = 484

Hydrograph Volume = 2,683 cuft

Hydrograph Discharge Table

| Time -- Outflow (min cfs) | Time -- Outflow (min cfs) |
|------------------------------|------------------------------|
| 690 0.05 | 826 0.07 |
| 694 0.06 | 830 0.07 |
| 698 0.08 | 834 0.07 |
| 702 0.12 | 838 0.06 |
| 706 0.16 | 842 0.06 |
| 710 0.22 | 846 0.06 |
| 714 0.28 | 850 0.06 |
| 718 0.43 | 854 0.06 |
| 722 0.79 | 858 0.06 |
| 726 0.82 | 862 0.06 |
| 730 0.53 | 866 0.06 |
| 734 0.42 | 870 0.06 |
| 738 0.37 | 874 0.05 |
| 742 0.32 | 878 0.05 |
| 746 0.26 | 882 0.05 |
| 750 0.19 | 886 0.05 |
| 754 0.14 | 890 0.05 |
| 758 0.13 | 894 0.05 |
| 762 0.12 | 898 0.05 |
| 766 0.12 | 902 0.05 |
| 770 0.11 | 906 0.05 |
| 774 0.10 | 910 0.05 |
| 778 0.10 | 914 0.05 |
| 782 0.09 | 918 0.04 |
| 786 0.09 | |
| 790 0.08 | |
| 794 0.08 | ...End |
| 798 0.08 | |
| 802 0.08 | |
| 806 0.08 | |
| 810 0.08 | |
| 814 0.07 | |
| 818 0.07 | |
| 822 0.07 | |

Hydrograph Report

Hyd. No. 6

Post Subarea 3a

| | | | |
|-----------------|--------------|--------------------|-------------|
| Hydrograph type | = SCS Runoff | Peak discharge | = 18.02 cfs |
| Storm frequency | = 100 yrs | Time interval | = 2 min |
| Drainage area | = 3.15 ac | Curve number | = 85 |
| Basin Slope | = 0.0 % | Hydraulic length | = 0 ft |
| Tc method | = USER | Time of conc. (Tc) | = 7.5 min |
| Total precip. | = 7.30 in | Distribution | = Type III |
| Storm duration | = 24 hrs | Shape factor | = 484 |

Hydrograph Volume = 63,345 cuft

Hydrograph Discharge Table

| Time (min) | Outflow (cfs) | Time (min) | Outflow (cfs) |
|------------|---------------|------------|---------------|
| 634 | 0.90 | 770 | 2.12 |
| 638 | 0.94 | 774 | 1.99 |
| 642 | 0.97 | 778 | 1.86 |
| 646 | 1.01 | 782 | 1.73 |
| 650 | 1.04 | 786 | 1.62 |
| 654 | 1.08 | 790 | 1.56 |
| 658 | 1.11 | 794 | 1.52 |
| 662 | 1.15 | 798 | 1.48 |
| 666 | 1.21 | 802 | 1.45 |
| 670 | 1.30 | 806 | 1.42 |
| 674 | 1.41 | 810 | 1.38 |
| 678 | 1.52 | 814 | 1.35 |
| 682 | 1.64 | 818 | 1.31 |
| 686 | 1.77 | 822 | 1.28 |
| 690 | 1.89 | 826 | 1.25 |
| 694 | 2.11 | 830 | 1.21 |
| 698 | 2.70 | 834 | 1.18 |
| 702 | 3.65 | 838 | 1.14 |
| 706 | 4.77 | 842 | 1.11 |
| 710 | 5.95 | 846 | 1.08 |
| 714 | 7.18 | 850 | 1.06 |
| 718 | 9.35 | 854 | 1.04 |
| 722 | 14.57 | 858 | 1.02 |
| 726 | 18.02 << | 862 | 1.01 |
| 730 | 15.30 | 866 | 0.99 |
| 734 | 10.93 | 870 | 0.97 |
| 738 | 8.31 | 874 | 0.96 |
| 742 | 7.00 | 878 | 0.94 |
| 746 | 5.77 | 882 | 0.92 |
| 750 | 4.54 | 886 | 0.91 |
| 754 | 3.41 | | |
| 758 | 2.70 | | |
| 762 | 2.39 | ...End | |
| 766 | 2.25 | | |

Hydrograph Report

Hyd. No. 7

Post Subarea 3b

Hydrograph type = SCS Runoff
Storm frequency = 100 yrs
Drainage area = 0.35 ac
Basin Slope = 0.0 %
Tc method = USER
Total precip. = 7.30 in
Storm duration = 24 hrs

Peak discharge = 1.14 cfs
Time interval = 2 min
Curve number = 61
Hydraulic length = 0 ft
Time of conc. (Tc) = 6 min
Distribution = Type III
Shape factor = 484

Hydrograph Volume = 3,478 cuft

Hydrograph Discharge Table

| Time -- Outflow (min cfs) | Time -- Outflow (min cfs) |
|------------------------------|------------------------------|
| 690 0.06 | 826 0.09 |
| 694 0.07 | 830 0.09 |
| 698 0.11 | 834 0.08 |
| 702 0.16 | 838 0.08 |
| 706 0.21 | 842 0.08 |
| 710 0.28 | 846 0.08 |
| 714 0.36 | 850 0.08 |
| 718 0.56 | 854 0.08 |
| 722 1.03 | 858 0.07 |
| 726 1.06 | 862 0.07 |
| 730 0.69 | 866 0.07 |
| 734 0.55 | 870 0.07 |
| 738 0.48 | 874 0.07 |
| 742 0.41 | 878 0.07 |
| 746 0.33 | 882 0.07 |
| 750 0.25 | 886 0.07 |
| 754 0.19 | 890 0.07 |
| 758 0.17 | 894 0.06 |
| 762 0.16 | 898 0.06 |
| 766 0.15 | 902 0.06 |
| 770 0.14 | 906 0.06 |
| 774 0.13 | 910 0.06 |
| 778 0.12 | 914 0.06 |
| 782 0.12 | 918 0.06 |
| 786 0.11 | |
| 790 0.11 | |
| 794 0.11 | ...End |
| 798 0.10 | |
| 802 0.10 | |
| 806 0.10 | |
| 810 0.10 | |
| 814 0.10 | |
| 818 0.09 | |
| 822 0.09 | |

Hydrograph Report

Hydraflow Hydrographs by Intelisolve

Hyd. No. 8

Basin 1 In

Hydrograph type = Combine
Storm frequency = 100 yrs
Inflow hyds. = 2, 3

Peak discharge = 10.71 cfs
Time interval = 2 min

Hydrograph Volume = 42,185 cuft

Hydrograph Discharge Table

| Time (min) | Hyd. 2 + (cfs) | Hyd. 3 + (cfs) | Outflow (cfs) |
|------------|----------------|----------------|---------------|
| 632 | 0.54 | 0.01 | 0.55 |
| 636 | 0.56 | 0.01 | 0.57 |
| 640 | 0.58 | 0.01 | 0.59 |
| 644 | 0.60 | 0.01 | 0.61 |
| 648 | 0.62 | 0.02 | 0.64 |
| 652 | 0.64 | 0.02 | 0.66 |
| 656 | 0.67 | 0.02 | 0.68 |
| 660 | 0.69 | 0.02 | 0.71 |
| 664 | 0.71 | 0.02 | 0.74 |
| 668 | 0.75 | 0.02 | 0.77 |
| 672 | 0.80 | 0.03 | 0.83 |
| 676 | 0.87 | 0.03 | 0.90 |
| 680 | 0.94 | 0.04 | 0.97 |
| 684 | 1.01 | 0.04 | 1.05 |
| 688 | 1.09 | 0.05 | 1.13 |
| 692 | 1.17 | 0.05 | 1.22 |
| 696 | 1.33 | 0.07 | 1.41 |
| 700 | 1.68 | 0.11 | 1.79 |
| 704 | 2.20 | 0.15 | 2.35 |
| 708 | 2.86 | 0.20 | 3.05 |
| 712 | 3.58 | 0.25 | 3.84 |
| 716 | 4.40 | 0.34 | 4.74 |
| 720 | 5.99 | 0.63 | 6.62 |
| 724 | 8.58 | 0.91 << | 9.50 |
| 728 | 10.02 << | 0.69 | 10.71 << |
| 732 | 9.20 | 0.48 | 9.67 |
| 736 | 7.49 | 0.41 | 7.90 |
| 740 | 5.72 | 0.36 | 6.08 |
| 744 | 4.51 | 0.30 | 4.81 |
| 748 | 3.72 | 0.23 | 3.95 |
| 752 | 2.96 | 0.17 | 3.13 |
| 756 | 2.29 | 0.14 | 2.42 |
| 760 | 1.82 | 0.13 | 1.95 |
| 764 | 1.55 | 0.12 | 1.68 |
| 768 | 1.42 | 0.12 | 1.53 |
| 772 | 1.33 | 0.11 | 1.44 |
| 776 | 1.25 | 0.10 | 1.35 |
| 780 | 1.17 | 0.10 | 1.26 |

Continues on next page...

Hydrograph Discharge Table

| Time (min) | Hyd. 2 + (cfs) | Hyd. 3 + (cfs) | Outflow (cfs) |
|-----------------------|---------------------------|---------------------------|--------------------------|
| 784 | 1.09 | 0.09 | 1.18 |
| 788 | 1.02 | 0.09 | 1.11 |
| 792 | 0.98 | 0.09 | 1.07 |
| 796 | 0.95 | 0.08 | 1.03 |
| 800 | 0.93 | 0.08 | 1.01 |
| 804 | 0.91 | 0.08 | 0.99 |
| 808 | 0.88 | 0.08 | 0.96 |
| 812 | 0.86 | 0.08 | 0.94 |
| 816 | 0.84 | 0.08 | 0.92 |
| 820 | 0.82 | 0.07 | 0.89 |
| 824 | 0.80 | 0.07 | 0.87 |
| 828 | 0.78 | 0.07 | 0.85 |
| 832 | 0.76 | 0.07 | 0.83 |
| 836 | 0.74 | 0.07 | 0.80 |
| 840 | 0.71 | 0.06 | 0.78 |
| 844 | 0.69 | 0.06 | 0.76 |
| 848 | 0.67 | 0.06 | 0.74 |
| 852 | 0.66 | 0.06 | 0.72 |
| 856 | 0.65 | 0.06 | 0.71 |
| 860 | 0.64 | 0.06 | 0.70 |
| 864 | 0.63 | 0.06 | 0.69 |
| 868 | 0.62 | 0.06 | 0.67 |
| 872 | 0.61 | 0.06 | 0.66 |
| 876 | 0.60 | 0.06 | 0.65 |
| 880 | 0.59 | 0.05 | 0.64 |
| 884 | 0.58 | 0.05 | 0.63 |
| 888 | 0.57 | 0.05 | 0.62 |
| 892 | 0.56 | 0.05 | 0.61 |
| 896 | 0.55 | 0.05 | 0.60 |
| 900 | 0.54 | 0.05 | 0.59 |
| 904 | 0.52 | 0.05 | 0.57 |
| 908 | 0.51 | 0.05 | 0.56 |
| 912 | 0.50 | 0.05 | 0.55 |
| 916 | 0.49 | 0.05 | 0.54 |

...End

Hydrograph Report

Hyd. No. 9

Basin 2 In

Hydrograph type = Combine
Storm frequency = 100 yrs
Inflow hyds. = 4, 5

Peak discharge = 11.93 cfs
Time interval = 2 min

Hydrograph Volume = 51,007 cuft

Hydrograph Discharge Table

| Time (min) | Hyd. 4 + (cfs) | Hyd. 5 + (cfs) | Outflow (cfs) |
|------------|----------------|----------------|---------------|
| 616 | 0.60 | 0.01 | 0.60 |
| 620 | 0.62 | 0.01 | 0.63 |
| 624 | 0.65 | 0.01 | 0.65 |
| 628 | 0.67 | 0.01 | 0.68 |
| 632 | 0.69 | 0.01 | 0.70 |
| 636 | 0.72 | 0.01 | 0.73 |
| 640 | 0.74 | 0.01 | 0.76 |
| 644 | 0.77 | 0.01 | 0.78 |
| 648 | 0.80 | 0.01 | 0.81 |
| 652 | 0.82 | 0.02 | 0.84 |
| 656 | 0.85 | 0.02 | 0.87 |
| 660 | 0.88 | 0.02 | 0.89 |
| 664 | 0.90 | 0.02 | 0.93 |
| 668 | 0.94 | 0.02 | 0.97 |
| 672 | 1.00 | 0.03 | 1.03 |
| 676 | 1.07 | 0.03 | 1.10 |
| 680 | 1.15 | 0.03 | 1.18 |
| 684 | 1.24 | 0.04 | 1.28 |
| 688 | 1.33 | 0.04 | 1.37 |
| 692 | 1.43 | 0.05 | 1.48 |
| 696 | 1.60 | 0.07 | 1.67 |
| 700 | 1.92 | 0.10 | 2.03 |
| 704 | 2.46 | 0.14 | 2.60 |
| 708 | 3.17 | 0.19 | 3.36 |
| 712 | 4.00 | 0.25 | 4.24 |
| 716 | 4.94 | 0.33 | 5.27 |
| 720 | 6.52 | 0.61 | 7.13 |
| 724 | 8.99 | 0.88 << | 9.87 |
| 728 | 11.06 | 0.67 | 11.73 |
| 732 | 11.18 | 0.46 | 11.64 |
| 736 | 9.82 | 0.40 | 10.22 |
| 740 | 8.04 | 0.35 | 8.39 |
| 744 | 6.22 | 0.29 | 6.51 |
| 748 | 4.90 | 0.23 | 5.13 |
| 752 | 3.96 | 0.17 | 4.13 |
| 756 | 3.13 | 0.13 | 3.26 |
| 760 | 2.47 | 0.13 | 2.59 |
| 764 | 2.03 | 0.12 | 2.15 |

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Hydrograph Discharge Table

| Time (min) | Hyd. 4 + (cfs) | Hyd. 5 + (cfs) | Outflow (cfs) |
|-----------------------|---------------------------|---------------------------|--------------------------|
| 768 | 1.77 | 0.11 | 1.89 |
| 772 | 1.63 | 0.11 | 1.73 |
| 776 | 1.53 | 0.10 | 1.63 |
| 780 | 1.43 | 0.09 | 1.52 |
| 784 | 1.34 | 0.09 | 1.42 |
| 788 | 1.25 | 0.08 | 1.34 |
| 792 | 1.19 | 0.08 | 1.27 |
| 796 | 1.14 | 0.08 | 1.22 |
| 800 | 1.11 | 0.08 | 1.19 |
| 804 | 1.08 | 0.08 | 1.16 |
| 808 | 1.06 | 0.08 | 1.13 |
| 812 | 1.03 | 0.07 | 1.11 |
| 816 | 1.01 | 0.07 | 1.08 |
| 820 | 0.98 | 0.07 | 1.05 |
| 824 | 0.96 | 0.07 | 1.03 |
| 828 | 0.93 | 0.07 | 1.00 |
| 832 | 0.91 | 0.07 | 0.97 |
| 836 | 0.88 | 0.06 | 0.94 |
| 840 | 0.85 | 0.06 | 0.92 |
| 844 | 0.83 | 0.06 | 0.89 |
| 848 | 0.81 | 0.06 | 0.87 |
| 852 | 0.79 | 0.06 | 0.85 |
| 856 | 0.77 | 0.06 | 0.83 |
| 860 | 0.76 | 0.06 | 0.82 |
| 864 | 0.75 | 0.06 | 0.80 |
| 868 | 0.73 | 0.06 | 0.79 |
| 872 | 0.72 | 0.05 | 0.78 |
| 876 | 0.71 | 0.05 | 0.76 |
| 880 | 0.70 | 0.05 | 0.75 |
| 884 | 0.69 | 0.05 | 0.74 |
| 888 | 0.67 | 0.05 | 0.72 |
| 892 | 0.66 | 0.05 | 0.71 |
| 896 | 0.65 | 0.05 | 0.70 |
| 900 | 0.64 | 0.05 | 0.68 |
| 904 | 0.62 | 0.05 | 0.67 |
| 908 | 0.61 | 0.05 | 0.66 |
| 912 | 0.60 | 0.05 | 0.65 |
| 916 | 0.59 | 0.04 | 0.63 |
| 920 | 0.58 | 0.04 | 0.62 |
| 924 | 0.56 | 0.04 | 0.61 |

...End

Hydrograph Report

Hyd. No. 10

Basin 3 In

Hydrograph type = Combine
Storm frequency = 100 yrs
Inflow hyds. = 6, 7

Peak discharge = 19.08 cfs
Time interval = 2 min

Hydrograph Volume = 66,824 cuft

Hydrograph Discharge Table

| Time (min) | Hyd. 6 + (cfs) | Hyd. 7 + (cfs) | Outflow (cfs) |
|------------|----------------|----------------|---------------|
| 640 | 0.95 | 0.02 | 0.97 |
| 644 | 0.99 | 0.02 | 1.01 |
| 648 | 1.02 | 0.02 | 1.04 |
| 652 | 1.06 | 0.02 | 1.08 |
| 656 | 1.09 | 0.02 | 1.12 |
| 660 | 1.13 | 0.02 | 1.16 |
| 664 | 1.18 | 0.03 | 1.20 |
| 668 | 1.25 | 0.03 | 1.28 |
| 672 | 1.35 | 0.04 | 1.39 |
| 676 | 1.47 | 0.04 | 1.51 |
| 680 | 1.58 | 0.05 | 1.63 |
| 684 | 1.70 | 0.05 | 1.76 |
| 688 | 1.83 | 0.06 | 1.88 |
| 692 | 1.97 | 0.07 | 2.04 |
| 696 | 2.35 | 0.09 | 2.44 |
| 700 | 3.14 | 0.13 | 3.27 |
| 704 | 4.19 | 0.18 | 4.38 |
| 708 | 5.35 | 0.25 | 5.60 |
| 712 | 6.55 | 0.32 | 6.87 |
| 716 | 7.99 | 0.42 | 8.41 |
| 720 | 11.65 | 0.78 | 12.43 |
| 724 | 17.05 | 1.14 << | 18.19 |
| 728 | 17.22 | 0.87 | 18.09 |
| 732 | 13.01 | 0.59 | 13.60 |
| 736 | 9.35 | 0.52 | 9.86 |
| 740 | 7.60 | 0.45 | 8.05 |
| 744 | 6.39 | 0.37 | 6.76 |
| 748 | 5.16 | 0.29 | 5.45 |
| 752 | 3.94 | 0.21 | 4.15 |
| 756 | 2.99 | 0.17 | 3.16 |
| 760 | 2.51 | 0.16 | 2.67 |
| 764 | 2.31 | 0.15 | 2.47 |
| 768 | 2.18 | 0.15 | 2.33 |
| 772 | 2.05 | 0.14 | 2.19 |
| 776 | 1.92 | 0.13 | 2.05 |
| 780 | 1.79 | 0.12 | 1.91 |
| 784 | 1.67 | 0.11 | 1.78 |
| 788 | 1.58 | 0.11 | 1.69 |

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Hydrograph Discharge Table

| Time (min) | Hyd. 6 + (cfs) | Hyd. 7 + (cfs) | Outflow (cfs) |
|-----------------------|---------------------------|---------------------------|--------------------------|
| 792 | 1.54 | 0.11 | 1.64 |
| 796 | 1.50 | 0.11 | 1.61 |
| 800 | 1.47 | 0.10 | 1.57 |
| 804 | 1.43 | 0.10 | 1.53 |
| 808 | 1.40 | 0.10 | 1.50 |
| 812 | 1.36 | 0.10 | 1.46 |
| 816 | 1.33 | 0.09 | 1.43 |
| 820 | 1.30 | 0.09 | 1.39 |
| 824 | 1.26 | 0.09 | 1.35 |
| 828 | 1.23 | 0.09 | 1.32 |
| 832 | 1.19 | 0.09 | 1.28 |
| 836 | 1.16 | 0.08 | 1.24 |
| 840 | 1.12 | 0.08 | 1.21 |
| 844 | 1.09 | 0.08 | 1.17 |
| 848 | 1.07 | 0.08 | 1.14 |
| 852 | 1.05 | 0.08 | 1.12 |
| 856 | 1.03 | 0.08 | 1.11 |
| 860 | 1.01 | 0.07 | 1.09 |
| 864 | 1.00 | 0.07 | 1.07 |
| 868 | 0.98 | 0.07 | 1.05 |
| 872 | 0.97 | 0.07 | 1.04 |
| 876 | 0.95 | 0.07 | 1.02 |
| 880 | 0.93 | 0.07 | 1.00 |
| 884 | 0.92 | 0.07 | 0.98 |
| 888 | 0.90 | 0.07 | 0.97 |

...End

Hydrograph Report

Hyd. No. 11

Basin 1 Out

Hydrograph type = Reservoir
 Storm frequency = 100 yrs
 Inflow hyd. No. = 8
 Max. Elevation = 243.46 ft

Peak discharge = 1.50 cfs
 Time interval = 2 min
 Reservoir name = Retention Basin N
 Max. Storage = 34,262 cuft

Storage Indication method used.

Outflow hydrograph volume = 41,596 cuft

Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 580 | 0.34 | 240.24 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 584 | 0.35 | 240.25 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 588 | 0.37 | 240.26 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 592 | 0.38 | 240.27 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 596 | 0.39 | 240.28 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 600 | 0.40 | 240.30 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 604 | 0.41 | 240.31 | 23.09 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 608 | 0.43 | 240.32 | 23.09 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 612 | 0.44 | 240.33 | 23.09 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 616 | 0.46 | 240.34 | 23.09 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.11 |
| 620 | 0.48 | 240.36 | 23.09 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.11 |
| 624 | 0.50 | 240.37 | 23.09 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.11 |
| 628 | 0.53 | 240.38 | 23.09 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.12 |
| 632 | 0.55 | 240.40 | 23.09 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.12 |
| 636 | 0.57 | 240.41 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 640 | 0.59 | 240.43 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 644 | 0.61 | 240.45 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 648 | 0.64 | 240.46 | 23.09 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 652 | 0.66 | 240.48 | 23.09 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 656 | 0.68 | 240.50 | 23.09 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 660 | 0.71 | 240.52 | 23.09 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 664 | 0.74 | 240.54 | 23.09 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 668 | 0.77 | 240.56 | 23.09 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |
| 672 | 0.83 | 240.59 | 23.09 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |
| 676 | 0.90 | 240.61 | 23.09 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |
| 680 | 0.97 | 240.64 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 684 | 1.05 | 240.67 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 688 | 1.13 | 240.70 | 23.09 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 692 | 1.22 | 240.74 | 23.09 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 696 | 1.41 | 240.78 | 23.09 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 700 | 1.79 | 240.83 | 23.09 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 704 | 2.35 | 240.90 | 23.09 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 708 | 3.05 | 240.98 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 712 | 3.84 | 241.10 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 716 | 4.74 | 241.25 | 23.09 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 720 | 6.62 | 241.44 | 23.09 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 724 | 9.50 | 241.72 | 23.09 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 728 | 10.71 << | 242.07 | 23.09 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |

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Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 732 | 9.67 | 242.43 | 23.09 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 736 | 7.90 | 242.73 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 740 | 6.08 | 242.97 | 23.09 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 744 | 4.81 | 243.15 | 23.09 | 0.41 | ---- | ---- | 0.22 | ---- | ---- | ---- | ---- | 0.63 |
| 748 | 3.95 | 243.28 | 23.09 | 0.42 | ---- | ---- | 0.51 | ---- | ---- | ---- | ---- | 0.92 |
| 752 | 3.13 | 243.37 | 23.09 | 0.43 | ---- | ---- | 0.75 | ---- | ---- | ---- | ---- | 1.17 |
| 756 | 2.42 | 243.42 | 23.09 | 0.43 | ---- | ---- | 0.91 | ---- | ---- | ---- | ---- | 1.34 |
| 760 | 1.95 | 243.45 | 23.09 | 0.43 | ---- | ---- | 1.01 | ---- | ---- | ---- | ---- | 1.44 |
| 764 | 1.68 | 243.46 | 23.09 | 0.43 | ---- | ---- | 1.05 | ---- | ---- | ---- | ---- | 1.48 |
| 768 | 1.53 | 243.46 | 23.09 | 0.43 | ---- | ---- | 1.07 | ---- | ---- | ---- | ---- | 1.50 |
| 772 | 1.44 | 243.46 | 23.09 | 0.43 | ---- | ---- | 1.06 | ---- | ---- | ---- | ---- | 1.50 |
| 776 | 1.35 | 243.46 | 23.09 | 0.43 | ---- | ---- | 1.05 | ---- | ---- | ---- | ---- | 1.48 |
| 780 | 1.26 | 243.45 | 23.09 | 0.43 | ---- | ---- | 1.03 | ---- | ---- | ---- | ---- | 1.46 |
| 784 | 1.18 | 243.45 | 23.09 | 0.43 | ---- | ---- | 1.00 | ---- | ---- | ---- | ---- | 1.43 |
| 788 | 1.11 | 243.44 | 23.09 | 0.43 | ---- | ---- | 0.97 | ---- | ---- | ---- | ---- | 1.40 |
| 792 | 1.07 | 243.43 | 23.09 | 0.43 | ---- | ---- | 0.93 | ---- | ---- | ---- | ---- | 1.36 |
| 796 | 1.03 | 243.41 | 23.09 | 0.43 | ---- | ---- | 0.89 | ---- | ---- | ---- | ---- | 1.32 |
| 800 | 1.01 | 243.40 | 23.09 | 0.43 | ---- | ---- | 0.86 | ---- | ---- | ---- | ---- | 1.29 |
| 804 | 0.99 | 243.39 | 23.09 | 0.43 | ---- | ---- | 0.83 | ---- | ---- | ---- | ---- | 1.26 |
| 808 | 0.96 | 243.39 | 23.09 | 0.43 | ---- | ---- | 0.80 | ---- | ---- | ---- | ---- | 1.23 |
| 812 | 0.94 | 243.38 | 23.09 | 0.43 | ---- | ---- | 0.78 | ---- | ---- | ---- | ---- | 1.20 |
| 816 | 0.92 | 243.37 | 23.09 | 0.43 | ---- | ---- | 0.75 | ---- | ---- | ---- | ---- | 1.18 |
| 820 | 0.89 | 243.36 | 23.09 | 0.42 | ---- | ---- | 0.73 | ---- | ---- | ---- | ---- | 1.15 |
| 824 | 0.87 | 243.35 | 23.09 | 0.42 | ---- | ---- | 0.70 | ---- | ---- | ---- | ---- | 1.12 |
| 828 | 0.85 | 243.34 | 23.09 | 0.42 | ---- | ---- | 0.68 | ---- | ---- | ---- | ---- | 1.10 |
| 832 | 0.83 | 243.33 | 23.09 | 0.42 | ---- | ---- | 0.65 | ---- | ---- | ---- | ---- | 1.07 |
| 836 | 0.80 | 243.32 | 23.09 | 0.42 | ---- | ---- | 0.63 | ---- | ---- | ---- | ---- | 1.05 |
| 840 | 0.78 | 243.31 | 23.09 | 0.42 | ---- | ---- | 0.60 | ---- | ---- | ---- | ---- | 1.02 |
| 844 | 0.76 | 243.30 | 23.09 | 0.42 | ---- | ---- | 0.58 | ---- | ---- | ---- | ---- | 1.00 |
| 848 | 0.74 | 243.29 | 23.09 | 0.42 | ---- | ---- | 0.56 | ---- | ---- | ---- | ---- | 0.98 |
| 852 | 0.72 | 243.29 | 23.09 | 0.42 | ---- | ---- | 0.53 | ---- | ---- | ---- | ---- | 0.95 |
| 856 | 0.71 | 243.28 | 23.09 | 0.42 | ---- | ---- | 0.51 | ---- | ---- | ---- | ---- | 0.93 |
| 860 | 0.70 | 243.27 | 23.09 | 0.42 | ---- | ---- | 0.49 | ---- | ---- | ---- | ---- | 0.91 |
| 864 | 0.69 | 243.26 | 23.09 | 0.42 | ---- | ---- | 0.47 | ---- | ---- | ---- | ---- | 0.89 |
| 868 | 0.67 | 243.26 | 23.09 | 0.42 | ---- | ---- | 0.45 | ---- | ---- | ---- | ---- | 0.87 |
| 872 | 0.66 | 243.25 | 23.09 | 0.42 | ---- | ---- | 0.43 | ---- | ---- | ---- | ---- | 0.85 |
| 876 | 0.65 | 243.24 | 23.09 | 0.42 | ---- | ---- | 0.41 | ---- | ---- | ---- | ---- | 0.83 |
| 880 | 0.64 | 243.24 | 23.09 | 0.42 | ---- | ---- | 0.40 | ---- | ---- | ---- | ---- | 0.81 |
| 884 | 0.63 | 243.23 | 23.09 | 0.42 | ---- | ---- | 0.38 | ---- | ---- | ---- | ---- | 0.80 |
| 888 | 0.62 | 243.22 | 23.09 | 0.42 | ---- | ---- | 0.36 | ---- | ---- | ---- | ---- | 0.78 |
| 892 | 0.61 | 243.22 | 23.09 | 0.42 | ---- | ---- | 0.35 | ---- | ---- | ---- | ---- | 0.76 |
| 896 | 0.60 | 243.21 | 23.09 | 0.42 | ---- | ---- | 0.33 | ---- | ---- | ---- | ---- | 0.75 |
| 900 | 0.59 | 243.21 | 23.09 | 0.41 | ---- | ---- | 0.32 | ---- | ---- | ---- | ---- | 0.73 |
| 904 | 0.57 | 243.20 | 23.09 | 0.41 | ---- | ---- | 0.30 | ---- | ---- | ---- | ---- | 0.72 |
| 908 | 0.56 | 243.20 | 23.09 | 0.41 | ---- | ---- | 0.29 | ---- | ---- | ---- | ---- | 0.71 |
| 912 | 0.55 | 243.19 | 23.09 | 0.41 | ---- | ---- | 0.29 | ---- | ---- | ---- | ---- | 0.70 |
| 916 | 0.54 | 243.19 | 23.09 | 0.41 | ---- | ---- | 0.28 | ---- | ---- | ---- | ---- | 0.69 |
| 920 | 0.53 | 243.18 | 23.09 | 0.41 | ---- | ---- | 0.27 | ---- | ---- | ---- | ---- | 0.68 |
| 924 | 0.52 | 243.18 | 23.09 | 0.41 | ---- | ---- | 0.26 | ---- | ---- | ---- | ---- | 0.67 |
| 928 | 0.51 | 243.17 | 23.09 | 0.41 | ---- | ---- | 0.25 | ---- | ---- | ---- | ---- | 0.67 |
| 932 | 0.50 | 243.16 | 23.09 | 0.41 | ---- | ---- | 0.24 | ---- | ---- | ---- | ---- | 0.66 |

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Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 936 | 0.48 | 243.16 | 23.09 | 0.41 | ---- | ---- | 0.24 | ---- | ---- | ---- | ---- | 0.65 |
| 940 | 0.47 | 243.15 | 23.09 | 0.41 | ---- | ---- | 0.23 | ---- | ---- | ---- | ---- | 0.64 |
| 944 | 0.46 | 243.15 | 23.09 | 0.41 | ---- | ---- | 0.22 | ---- | ---- | ---- | ---- | 0.63 |
| 948 | 0.45 | 243.14 | 23.09 | 0.41 | ---- | ---- | 0.21 | ---- | ---- | ---- | ---- | 0.62 |
| 952 | 0.44 | 243.13 | 23.09 | 0.41 | ---- | ---- | 0.20 | ---- | ---- | ---- | ---- | 0.61 |
| 956 | 0.43 | 243.13 | 23.09 | 0.41 | ---- | ---- | 0.19 | ---- | ---- | ---- | ---- | 0.60 |
| 960 | 0.42 | 243.12 | 23.09 | 0.41 | ---- | ---- | 0.18 | ---- | ---- | ---- | ---- | 0.59 |
| 964 | 0.40 | 243.12 | 23.09 | 0.41 | ---- | ---- | 0.17 | ---- | ---- | ---- | ---- | 0.58 |
| 968 | 0.40 | 243.11 | 23.09 | 0.41 | ---- | ---- | 0.16 | ---- | ---- | ---- | ---- | 0.57 |
| 972 | 0.39 | 243.10 | 23.09 | 0.41 | ---- | ---- | 0.15 | ---- | ---- | ---- | ---- | 0.56 |
| 976 | 0.38 | 243.10 | 23.09 | 0.41 | ---- | ---- | 0.14 | ---- | ---- | ---- | ---- | 0.55 |
| 980 | 0.38 | 243.09 | 23.09 | 0.41 | ---- | ---- | 0.14 | ---- | ---- | ---- | ---- | 0.54 |
| 984 | 0.37 | 243.08 | 23.09 | 0.41 | ---- | ---- | 0.13 | ---- | ---- | ---- | ---- | 0.53 |
| 988 | 0.37 | 243.08 | 23.09 | 0.41 | ---- | ---- | 0.12 | ---- | ---- | ---- | ---- | 0.52 |
| 992 | 0.36 | 243.07 | 23.09 | 0.41 | ---- | ---- | 0.11 | ---- | ---- | ---- | ---- | 0.52 |
| 996 | 0.36 | 243.07 | 23.09 | 0.41 | ---- | ---- | 0.10 | ---- | ---- | ---- | ---- | 0.51 |
| 1000 | 0.35 | 243.06 | 23.09 | 0.41 | ---- | ---- | 0.09 | ---- | ---- | ---- | ---- | 0.50 |
| 1004 | 0.35 | 243.06 | 23.09 | 0.40 | ---- | ---- | 0.09 | ---- | ---- | ---- | ---- | 0.49 |
| 1008 | 0.34 | 243.05 | 23.09 | 0.40 | ---- | ---- | 0.08 | ---- | ---- | ---- | ---- | 0.48 |
| 1012 | 0.34 | 243.05 | 23.09 | 0.40 | ---- | ---- | 0.07 | ---- | ---- | ---- | ---- | 0.47 |
| 1016 | 0.33 | 243.04 | 23.09 | 0.40 | ---- | ---- | 0.06 | ---- | ---- | ---- | ---- | 0.47 |
| 1020 | 0.33 | 243.04 | 23.09 | 0.40 | ---- | ---- | 0.06 | ---- | ---- | ---- | ---- | 0.46 |
| 1024 | 0.32 | 243.03 | 23.09 | 0.40 | ---- | ---- | 0.05 | ---- | ---- | ---- | ---- | 0.45 |
| 1028 | 0.32 | 243.03 | 23.09 | 0.40 | ---- | ---- | 0.04 | ---- | ---- | ---- | ---- | 0.45 |
| 1032 | 0.31 | 243.02 | 23.09 | 0.40 | ---- | ---- | 0.04 | ---- | ---- | ---- | ---- | 0.44 |
| 1036 | 0.31 | 243.02 | 23.09 | 0.40 | ---- | ---- | 0.03 | ---- | ---- | ---- | ---- | 0.43 |
| 1040 | 0.30 | 243.02 | 23.09 | 0.40 | ---- | ---- | 0.02 | ---- | ---- | ---- | ---- | 0.42 |
| 1044 | 0.30 | 243.01 | 23.09 | 0.40 | ---- | ---- | 0.02 | ---- | ---- | ---- | ---- | 0.42 |
| 1048 | 0.29 | 243.01 | 23.09 | 0.40 | ---- | ---- | 0.01 | ---- | ---- | ---- | ---- | 0.41 |
| 1052 | 0.29 | 243.00 | 23.09 | 0.40 | ---- | ---- | 0.00 | ---- | ---- | ---- | ---- | 0.40 |
| 1056 | 0.28 | 243.00 | 23.09 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 1060 | 0.28 | 242.99 | 23.09 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 1064 | 0.27 | 242.99 | 23.09 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 1068 | 0.27 | 242.98 | 23.09 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 1072 | 0.26 | 242.98 | 23.09 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 1076 | 0.26 | 242.97 | 23.09 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 1080 | 0.25 | 242.97 | 23.09 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 1084 | 0.25 | 242.96 | 23.09 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 1088 | 0.24 | 242.96 | 23.09 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 1092 | 0.24 | 242.95 | 23.09 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 1096 | 0.24 | 242.95 | 23.09 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 1100 | 0.24 | 242.94 | 23.09 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 1104 | 0.24 | 242.94 | 23.09 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 1108 | 0.23 | 242.93 | 23.09 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 1112 | 0.23 | 242.92 | 23.09 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 1116 | 0.23 | 242.92 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1120 | 0.23 | 242.91 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1124 | 0.23 | 242.91 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1128 | 0.23 | 242.90 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1132 | 0.23 | 242.90 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1136 | 0.22 | 242.89 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |

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Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 1140 | 0.22 | 242.88 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1144 | 0.22 | 242.88 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1148 | 0.22 | 242.87 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1152 | 0.22 | 242.86 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1156 | 0.22 | 242.86 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1160 | 0.22 | 242.85 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1164 | 0.21 | 242.85 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1168 | 0.21 | 242.84 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1172 | 0.21 | 242.83 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1176 | 0.21 | 242.83 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1180 | 0.21 | 242.82 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1184 | 0.21 | 242.81 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1188 | 0.21 | 242.81 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1192 | 0.20 | 242.80 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1196 | 0.20 | 242.79 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1200 | 0.20 | 242.79 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1204 | 0.20 | 242.78 | 23.09 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 1208 | 0.20 | 242.77 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1212 | 0.20 | 242.77 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1216 | 0.19 | 242.76 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1220 | 0.19 | 242.75 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1224 | 0.19 | 242.75 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1228 | 0.19 | 242.74 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1232 | 0.19 | 242.73 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1236 | 0.19 | 242.73 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1240 | 0.19 | 242.72 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1244 | 0.18 | 242.71 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1248 | 0.18 | 242.71 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1252 | 0.18 | 242.70 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1256 | 0.18 | 242.69 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1260 | 0.18 | 242.68 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1264 | 0.18 | 242.68 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1268 | 0.17 | 242.67 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1272 | 0.17 | 242.66 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1276 | 0.17 | 242.65 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1280 | 0.17 | 242.65 | 23.09 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1284 | 0.17 | 242.64 | 23.09 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1288 | 0.17 | 242.63 | 23.09 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1292 | 0.17 | 242.63 | 23.09 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1296 | 0.16 | 242.62 | 23.09 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1300 | 0.16 | 242.61 | 23.09 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1304 | 0.16 | 242.60 | 23.09 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1308 | 0.16 | 242.59 | 23.09 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1312 | 0.16 | 242.59 | 23.09 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1316 | 0.16 | 242.58 | 23.09 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1320 | 0.16 | 242.57 | 23.09 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1324 | 0.20 | 242.57 | 23.09 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1328 | 0.22 | 242.56 | 23.09 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1332 | 0.20 | 242.55 | 23.09 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1336 | 0.18 | 242.55 | 23.09 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1340 | 0.17 | 242.54 | 23.09 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |

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Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 1344 | 0.16 | 242.53 | 23.09 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1348 | 0.16 | 242.53 | 23.09 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1352 | 0.16 | 242.52 | 23.09 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1356 | 0.16 | 242.51 | 23.09 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1360 | 0.15 | 242.50 | 23.09 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1364 | 0.15 | 242.50 | 23.09 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1368 | 0.15 | 242.49 | 23.09 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1372 | 0.15 | 242.48 | 23.09 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1376 | 0.15 | 242.47 | 23.09 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1380 | 0.15 | 242.47 | 23.09 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1384 | 0.15 | 242.46 | 23.09 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1388 | 0.15 | 242.45 | 23.09 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1392 | 0.15 | 242.44 | 23.09 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1396 | 0.14 | 242.43 | 23.09 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1400 | 0.14 | 242.43 | 23.09 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1404 | 0.14 | 242.42 | 23.09 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1408 | 0.14 | 242.41 | 23.09 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1412 | 0.14 | 242.40 | 23.09 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1416 | 0.14 | 242.40 | 23.09 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1420 | 0.14 | 242.39 | 23.09 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1424 | 0.14 | 242.38 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1428 | 0.14 | 242.37 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1432 | 0.13 | 242.36 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1436 | 0.13 | 242.36 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1440 | 0.13 | 242.35 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1444 | 0.11 | 242.34 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1448 | 0.06 | 242.33 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1452 | 0.03 | 242.32 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1456 | 0.01 | 242.31 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1460 | 0.00 | 242.30 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1464 | 0.00 | 242.28 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1468 | 0.00 | 242.27 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1472 | 0.00 | 242.26 | 23.09 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1476 | 0.00 | 242.25 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1480 | 0.00 | 242.23 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1484 | 0.00 | 242.22 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1488 | 0.00 | 242.21 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1492 | 0.00 | 242.20 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1496 | 0.00 | 242.18 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1500 | 0.00 | 242.17 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1504 | 0.00 | 242.16 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1508 | 0.00 | 242.15 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1512 | 0.00 | 242.14 | 23.09 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1516 | 0.00 | 242.12 | 23.09 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1520 | 0.00 | 242.11 | 23.09 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1524 | 0.00 | 242.10 | 23.09 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1528 | 0.00 | 242.09 | 23.09 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1532 | 0.00 | 242.08 | 23.09 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1536 | 0.00 | 242.06 | 23.09 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1540 | 0.00 | 242.05 | 23.09 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1544 | 0.00 | 242.04 | 23.09 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |

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Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 1548 | 0.00 | 242.03 | 23.09 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1552 | 0.00 | 242.02 | 23.09 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1556 | 0.00 | 242.01 | 23.09 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1560 | 0.00 | 241.99 | 23.09 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1564 | 0.00 | 241.98 | 23.09 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1568 | 0.00 | 241.97 | 23.09 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1572 | 0.00 | 241.96 | 23.09 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1576 | 0.00 | 241.95 | 23.09 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1580 | 0.00 | 241.94 | 23.09 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1584 | 0.00 | 241.93 | 23.09 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1588 | 0.00 | 241.91 | 23.09 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1592 | 0.00 | 241.90 | 23.09 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1596 | 0.00 | 241.89 | 23.09 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1600 | 0.00 | 241.88 | 23.09 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1604 | 0.00 | 241.87 | 23.09 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1608 | 0.00 | 241.86 | 23.09 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1612 | 0.00 | 241.85 | 23.09 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1616 | 0.00 | 241.84 | 23.09 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1620 | 0.00 | 241.82 | 23.09 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1624 | 0.00 | 241.81 | 23.09 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1628 | 0.00 | 241.80 | 23.09 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1632 | 0.00 | 241.79 | 23.09 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1636 | 0.00 | 241.78 | 23.09 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1640 | 0.00 | 241.77 | 23.09 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1644 | 0.00 | 241.76 | 23.09 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1648 | 0.00 | 241.75 | 23.09 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1652 | 0.00 | 241.74 | 23.09 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1656 | 0.00 | 241.73 | 23.09 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1660 | 0.00 | 241.72 | 23.09 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1664 | 0.00 | 241.70 | 23.09 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1668 | 0.00 | 241.69 | 23.09 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1672 | 0.00 | 241.68 | 23.09 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1676 | 0.00 | 241.67 | 23.09 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1680 | 0.00 | 241.66 | 23.09 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1684 | 0.00 | 241.65 | 23.09 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1688 | 0.00 | 241.64 | 23.09 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1692 | 0.00 | 241.63 | 23.09 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1696 | 0.00 | 241.62 | 23.09 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1700 | 0.00 | 241.61 | 23.09 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1704 | 0.00 | 241.60 | 23.09 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1708 | 0.00 | 241.59 | 23.09 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1712 | 0.00 | 241.58 | 23.09 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 1716 | 0.00 | 241.57 | 23.09 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 1720 | 0.00 | 241.56 | 23.09 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 1724 | 0.00 | 241.55 | 23.09 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 1728 | 0.00 | 241.54 | 23.09 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 1732 | 0.00 | 241.53 | 23.09 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 1736 | 0.00 | 241.52 | 23.09 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 1740 | 0.00 | 241.51 | 23.09 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 1744 | 0.00 | 241.50 | 23.09 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 1748 | 0.00 | 241.49 | 23.09 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |

Continues on next page...

Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 1752 | 0.00 | 241.48 | 23.09 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 1756 | 0.00 | 241.47 | 23.09 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 1760 | 0.00 | 241.46 | 23.09 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 1764 | 0.00 | 241.45 | 23.09 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 1768 | 0.00 | 241.44 | 23.09 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 1772 | 0.00 | 241.43 | 23.09 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 1776 | 0.00 | 241.42 | 23.09 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 1780 | 0.00 | 241.41 | 23.09 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 1784 | 0.00 | 241.40 | 23.09 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 1788 | 0.00 | 241.39 | 23.09 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 1792 | 0.00 | 241.38 | 23.09 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 1796 | 0.00 | 241.37 | 23.09 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 1800 | 0.00 | 241.36 | 23.09 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 1804 | 0.00 | 241.35 | 23.09 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 1808 | 0.00 | 241.34 | 23.09 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 1812 | 0.00 | 241.33 | 23.09 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 1816 | 0.00 | 241.33 | 23.09 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 1820 | 0.00 | 241.32 | 23.09 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 1824 | 0.00 | 241.31 | 23.09 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 1828 | 0.00 | 241.30 | 23.09 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 1832 | 0.00 | 241.29 | 23.09 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 1836 | 0.00 | 241.28 | 23.09 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 1840 | 0.00 | 241.27 | 23.09 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 1844 | 0.00 | 241.26 | 23.09 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 1848 | 0.00 | 241.25 | 23.09 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 1852 | 0.00 | 241.24 | 23.09 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 1856 | 0.00 | 241.23 | 23.09 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 1860 | 0.00 | 241.23 | 23.09 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 1864 | 0.00 | 241.22 | 23.09 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 1868 | 0.00 | 241.21 | 23.09 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 1872 | 0.00 | 241.20 | 23.09 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 1876 | 0.00 | 241.19 | 23.09 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 1880 | 0.00 | 241.18 | 23.09 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 1884 | 0.00 | 241.17 | 23.09 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 1888 | 0.00 | 241.16 | 23.09 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 1892 | 0.00 | 241.16 | 23.09 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 1896 | 0.00 | 241.15 | 23.09 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 1900 | 0.00 | 241.14 | 23.09 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 1904 | 0.00 | 241.13 | 23.09 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 1908 | 0.00 | 241.12 | 23.09 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 1912 | 0.00 | 241.11 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 1916 | 0.00 | 241.10 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 1920 | 0.00 | 241.10 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 1924 | 0.00 | 241.09 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 1928 | 0.00 | 241.08 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 1932 | 0.00 | 241.07 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 1936 | 0.00 | 241.06 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 1940 | 0.00 | 241.05 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 1944 | 0.00 | 241.05 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 1948 | 0.00 | 241.04 | 23.09 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 1952 | 0.00 | 241.03 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |

Continues on next page...

Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 1956 | 0.00 | 241.02 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 1960 | 0.00 | 241.01 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 1964 | 0.00 | 241.01 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 1968 | 0.00 | 241.00 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 1972 | 0.00 | 240.99 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 1976 | 0.00 | 240.98 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 1980 | 0.00 | 240.97 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 1984 | 0.00 | 240.97 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 1988 | 0.00 | 240.96 | 23.09 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 1992 | 0.00 | 240.95 | 23.09 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 1996 | 0.00 | 240.94 | 23.09 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 2000 | 0.00 | 240.94 | 23.09 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 2004 | 0.00 | 240.93 | 23.09 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 2008 | 0.00 | 240.92 | 23.09 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 2012 | 0.00 | 240.91 | 23.09 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 2016 | 0.00 | 240.91 | 23.09 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 2020 | 0.00 | 240.90 | 23.09 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 2024 | 0.00 | 240.89 | 23.09 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 2028 | 0.00 | 240.88 | 23.09 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 2032 | 0.00 | 240.88 | 23.09 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 2036 | 0.00 | 240.87 | 23.09 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 2040 | 0.00 | 240.86 | 23.09 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 2044 | 0.00 | 240.85 | 23.09 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 2048 | 0.00 | 240.85 | 23.09 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 2052 | 0.00 | 240.84 | 23.09 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 2056 | 0.00 | 240.83 | 23.09 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 2060 | 0.00 | 240.83 | 23.09 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 2064 | 0.00 | 240.82 | 23.09 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 2068 | 0.00 | 240.81 | 23.09 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 2072 | 0.00 | 240.80 | 23.09 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 2076 | 0.00 | 240.80 | 23.09 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 2080 | 0.00 | 240.79 | 23.09 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 2084 | 0.00 | 240.78 | 23.09 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 2088 | 0.00 | 240.78 | 23.09 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 2092 | 0.00 | 240.77 | 23.09 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 2096 | 0.00 | 240.76 | 23.09 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 2100 | 0.00 | 240.76 | 23.09 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 2104 | 0.00 | 240.75 | 23.09 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 2108 | 0.00 | 240.74 | 23.09 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 2112 | 0.00 | 240.74 | 23.09 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 2116 | 0.00 | 240.73 | 23.09 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 2120 | 0.00 | 240.72 | 23.09 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 2124 | 0.00 | 240.72 | 23.09 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 2128 | 0.00 | 240.71 | 23.09 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 2132 | 0.00 | 240.70 | 23.09 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 2136 | 0.00 | 240.70 | 23.09 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 2140 | 0.00 | 240.69 | 23.09 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 2144 | 0.00 | 240.68 | 23.09 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 2148 | 0.00 | 240.68 | 23.09 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 2152 | 0.00 | 240.67 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 2156 | 0.00 | 240.67 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |

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Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 2160 | 0.00 | 240.66 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 2164 | 0.00 | 240.65 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 2168 | 0.00 | 240.65 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 2172 | 0.00 | 240.64 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 2176 | 0.00 | 240.63 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 2180 | 0.00 | 240.63 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 2184 | 0.00 | 240.62 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 2188 | 0.00 | 240.62 | 23.09 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 2192 | 0.00 | 240.61 | 23.09 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |
| 2196 | 0.00 | 240.60 | 23.09 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |
| 2200 | 0.00 | 240.60 | 23.09 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |
| 2204 | 0.00 | 240.59 | 23.09 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |
| 2208 | 0.00 | 240.59 | 23.09 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |
| 2212 | 0.00 | 240.58 | 23.09 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |
| 2216 | 0.00 | 240.58 | 23.09 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |
| 2220 | 0.00 | 240.57 | 23.09 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |
| 2224 | 0.00 | 240.56 | 23.09 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |
| 2228 | 0.00 | 240.56 | 23.09 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 2232 | 0.00 | 240.55 | 23.09 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 2236 | 0.00 | 240.55 | 23.09 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 2240 | 0.00 | 240.54 | 23.09 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 2244 | 0.00 | 240.54 | 23.09 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 2248 | 0.00 | 240.53 | 23.09 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 2252 | 0.00 | 240.53 | 23.09 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 2256 | 0.00 | 240.52 | 23.09 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 2260 | 0.00 | 240.52 | 23.09 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 2264 | 0.00 | 240.51 | 23.09 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 2268 | 0.00 | 240.51 | 23.09 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 2272 | 0.00 | 240.50 | 23.09 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 2276 | 0.00 | 240.50 | 23.09 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 2280 | 0.00 | 240.49 | 23.09 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 2284 | 0.00 | 240.48 | 23.09 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 2288 | 0.00 | 240.48 | 23.09 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 2292 | 0.00 | 240.47 | 23.09 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 2296 | 0.00 | 240.47 | 23.09 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 2300 | 0.00 | 240.47 | 23.09 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 2304 | 0.00 | 240.46 | 23.09 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 2308 | 0.00 | 240.46 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 2312 | 0.00 | 240.45 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 2316 | 0.00 | 240.45 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 2320 | 0.00 | 240.44 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 2324 | 0.00 | 240.44 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 2328 | 0.00 | 240.43 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 2332 | 0.00 | 240.43 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 2336 | 0.00 | 240.42 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 2340 | 0.00 | 240.42 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 2344 | 0.00 | 240.41 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 2348 | 0.00 | 240.41 | 23.09 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 2352 | 0.00 | 240.40 | 23.09 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.12 |
| 2356 | 0.00 | 240.40 | 23.09 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.12 |
| 2360 | 0.00 | 240.40 | 23.09 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.12 |

Continues on next page...

Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 2364 | 0.00 | 240.39 | 23.09 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.12 |
| 2368 | 0.00 | 240.39 | 23.09 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.12 |
| 2372 | 0.00 | 240.38 | 23.09 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.12 |
| 2376 | 0.00 | 240.38 | 23.09 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.12 |
| 2380 | 0.00 | 240.37 | 23.09 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.12 |
| 2384 | 0.00 | 240.37 | 23.09 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.11 |
| 2388 | 0.00 | 240.37 | 23.09 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.11 |
| 2392 | 0.00 | 240.36 | 23.09 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.11 |
| 2396 | 0.00 | 240.36 | 23.09 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.11 |
| 2400 | 0.00 | 240.35 | 23.09 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.11 |
| 2404 | 0.00 | 240.35 | 23.09 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.11 |
| 2408 | 0.00 | 240.35 | 23.09 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.11 |
| 2412 | 0.00 | 240.34 | 23.09 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.11 |
| 2416 | 0.00 | 240.34 | 23.09 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.11 |
| 2420 | 0.00 | 240.33 | 23.09 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 2424 | 0.00 | 240.33 | 23.09 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 2428 | 0.00 | 240.33 | 23.09 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 2432 | 0.00 | 240.32 | 23.09 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 2436 | 0.00 | 240.32 | 23.09 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 2440 | 0.00 | 240.32 | 23.09 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 2444 | 0.00 | 240.31 | 23.09 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 2448 | 0.00 | 240.31 | 23.09 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 2452 | 0.00 | 240.31 | 23.09 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 2456 | 0.00 | 240.30 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 2460 | 0.00 | 240.30 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 2464 | 0.00 | 240.30 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 2468 | 0.00 | 240.29 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 2472 | 0.00 | 240.29 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 2476 | 0.00 | 240.29 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 2480 | 0.00 | 240.28 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 2484 | 0.00 | 240.28 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 2488 | 0.00 | 240.28 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 2492 | 0.00 | 240.27 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 2496 | 0.00 | 240.27 | 23.09 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 2500 | 0.00 | 240.27 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 2504 | 0.00 | 240.26 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 2508 | 0.00 | 240.26 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 2512 | 0.00 | 240.26 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 2516 | 0.00 | 240.25 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 2520 | 0.00 | 240.25 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 2524 | 0.00 | 240.25 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 2528 | 0.00 | 240.25 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 2532 | 0.00 | 240.24 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 2536 | 0.00 | 240.24 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 2540 | 0.00 | 240.24 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 2544 | 0.00 | 240.23 | 23.09 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |

...End

Reservoir Report

Reservoir No. 1 - Retention Basin No. 1

Hydraflow Hydrographs by Intelisolve

Pond Data

Pond storage is based on known contour areas. Average end area method used.

Stage / Storage Table

| Stage (ft) | Elevation (ft) | Contour area (sqft) | Incr. Storage (cuft) | Total storage (cuft) |
|------------|----------------|---------------------|----------------------|----------------------|
| 0.00 | 238.00 | 4,449 | 0 | 0 |
| 2.00 | 240.00 | 6,679 | 11,128 | 11,128 |
| 4.00 | 242.00 | 6,679 | 13,358 | 24,486 |
| 6.00 | 244.00 | 6,679 | 13,358 | 37,844 |
| 8.00 | 246.00 | 6,679 | 13,358 | 51,202 |
| 8.50 | 246.50 | 6,679 | 3,340 | 54,542 |

Culvert / Orifice Structures

| | [A] | [B] | [C] | [D] |
|---------------|----------|--------|------|------|
| Rise in | = 6.0 | 3.0 | 0.0 | 0.0 |
| Span in | = 6.0 | 3.0 | 0.0 | 0.0 |
| No. Barrels | = 10 | 1 | 0 | 0 |
| Invert El. ft | = 227.00 | 240.00 | 0.00 | 0.00 |
| Length ft | = 68.0 | 1.0 | 0.0 | 0.0 |
| Slope % | = 6.03 | 0.00 | 0.00 | 0.00 |
| N-Value | = .013 | .013 | .000 | .000 |
| Orif. Coeff. | = 0.60 | 0.60 | 0.00 | 0.00 |
| Multi-Stage | = n/a | Yes | No | No |

Weir Structures

| | [A] | [B] | [C] | [D] |
|--------------|----------|--------|--------|------|
| Crest Len ft | = 1.00 | 40.00 | 16.00 | 0.00 |
| Crest El. ft | = 243.00 | 244.50 | 244.00 | 0.00 |
| Weir Coeff. | = 3.33 | 2.60 | 3.33 | 0.00 |
| Weir Type | = Rect | Broad | Rect | --- |
| Multi-Stage | = Yes | Yes | Yes | No |

Exfiltration Rate = 0.00 in/hr/sqft Tailwater Elev. = 0.00 ft

Note: All outflows have been analyzed under inlet and outlet control.

Stage / Storage / Discharge Table

| Stage ft | Storage cuft | Elevation ft | Civ A cfs | Civ B cfs | Civ C cfs | Civ D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Total cfs |
|----------|--------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-----------|
| 0.00 | 0 | 238.00 | 0.00 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.00 |
| 0.20 | 1,113 | 238.20 | 23.09 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.00 |
| 0.40 | 2,226 | 238.40 | 23.09 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.00 |
| 0.60 | 3,338 | 238.60 | 23.09 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.00 |
| 0.80 | 4,451 | 238.80 | 23.09 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.00 |
| 1.00 | 5,564 | 239.00 | 23.09 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.00 |
| 1.20 | 6,677 | 239.20 | 23.09 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.00 |
| 1.40 | 7,790 | 239.40 | 23.09 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.00 |
| 1.60 | 8,902 | 239.60 | 23.09 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.00 |
| 1.80 | 10,015 | 239.80 | 23.09 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.00 |
| 2.00 | 11,128 | 240.00 | 23.09 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.00 |
| 2.20 | 12,464 | 240.20 | 23.09 | 0.06 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.06 |
| 2.40 | 13,800 | 240.40 | 23.09 | 0.12 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.12 |
| 2.60 | 15,135 | 240.60 | 23.09 | 0.16 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.16 |
| 2.80 | 16,471 | 240.80 | 23.09 | 0.19 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.19 |
| 3.00 | 17,807 | 241.00 | 23.09 | 0.22 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.22 |
| 3.20 | 19,143 | 241.20 | 23.09 | 0.25 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.25 |
| 3.40 | 20,479 | 241.40 | 23.09 | 0.27 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.27 |
| 3.60 | 21,814 | 241.60 | 23.09 | 0.29 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.29 |
| 3.80 | 23,150 | 241.80 | 23.09 | 0.31 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.31 |
| 4.00 | 24,486 | 242.00 | 23.09 | 0.32 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.32 |
| 4.20 | 25,822 | 242.20 | 23.09 | 0.34 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.34 |
| 4.40 | 27,158 | 242.40 | 23.09 | 0.36 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.36 |
| 4.60 | 28,493 | 242.60 | 23.09 | 0.37 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.37 |
| 4.80 | 29,829 | 242.80 | 23.09 | 0.39 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.39 |
| 5.00 | 31,165 | 243.00 | 23.09 | 0.40 | --- | --- | 0.00 | 0.00 | 0.00 | --- | --- | 0.40 |
| 5.20 | 32,501 | 243.20 | 23.09 | 0.41 | --- | --- | 0.30 | 0.00 | 0.00 | --- | --- | 0.71 |
| 5.40 | 33,837 | 243.40 | 23.09 | 0.43 | --- | --- | 0.84 | 0.00 | 0.00 | --- | --- | 1.27 |
| 5.60 | 35,172 | 243.60 | 23.09 | 0.44 | --- | --- | 1.55 | 0.00 | 0.00 | --- | --- | 1.99 |
| 5.80 | 36,508 | 243.80 | 23.09 | 0.45 | --- | --- | 2.38 | 0.00 | 0.00 | --- | --- | 2.84 |
| 6.00 | 37,844 | 244.00 | 23.09 | 0.47 | --- | --- | 3.33 | 0.00 | 0.00 | --- | --- | 3.80 |
| 6.20 | 39,180 | 244.20 | 23.09 | 0.48 | --- | --- | 4.38 | 0.00 | 4.77 | --- | --- | 9.62 |

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Stage / Storage / Discharge Table

| Stage ft | Storage cuft | Elevation ft | Civ A cfs | Civ B cfs | Civ C cfs | Civ D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Total cfs |
|-------------|-----------------|-----------------|--------------|--------------|--------------|--------------|-------------|-------------|-------------|-------------|--------------|--------------|
| 6.40 | 40,516 | 244.40 | 23.09 | 0.49 | --- | --- | 5.52 | 0.00 | 13.48 | --- | --- | 19.48 |
| 6.60 | 41,851 | 244.60 | 27.65 | 0.12 | --- | --- | 3.92 | 3.29 | 20.31 | --- | --- | 27.64 |
| 6.80 | 43,187 | 244.80 | 27.92 | 0.05 | --- | --- | 2.40 | 10.00 | 15.47 | --- | --- | 27.92 |
| 7.00 | 44,523 | 245.00 | 28.07 | 0.03 | --- | --- | 1.86 | 12.37 | 13.75 | --- | --- | 28.02 |
| 7.20 | 45,859 | 245.20 | 28.21 | 0.02 | --- | --- | 1.58 | 13.73 | 12.83 | --- | --- | 28.16 |
| 7.40 | 47,195 | 245.40 | 28.34 | 0.02 | --- | --- | 1.40 | 14.64 | 12.28 | --- | --- | 28.34 |
| 7.60 | 48,530 | 245.60 | 28.47 | 0.01 | --- | --- | 1.28 | 15.27 | 11.88 | --- | --- | 28.43 |
| 7.80 | 49,866 | 245.80 | 28.60 | 0.01 | --- | --- | 1.18 | 15.60 | 11.49 | --- | --- | 28.28 |
| 8.00 | 51,202 | 246.00 | 28.73 | 0.01 | --- | --- | 1.11 | 15.96 | 11.27 | --- | --- | 28.34 |
| 8.05 | 51,536 | 246.05 | 28.76 | 0.01 | --- | --- | 1.10 | 16.14 | 11.30 | --- | --- | 28.55 |
| 8.10 | 51,870 | 246.10 | 28.79 | 0.01 | --- | --- | 1.09 | 16.28 | 11.29 | --- | --- | 28.67 |
| 8.15 | 52,204 | 246.15 | 28.82 | 0.01 | --- | --- | 1.08 | 16.37 | 11.27 | --- | --- | 28.72 |
| 8.20 | 52,538 | 246.20 | 28.86 | 0.01 | --- | --- | 1.06 | 16.40 | 11.20 | --- | --- | 28.68 |
| 8.25 | 52,872 | 246.25 | 28.89 | 0.01 | --- | --- | 1.05 | 16.38 | 11.10 | --- | --- | 28.53 |
| 8.30 | 53,206 | 246.30 | 28.92 | 0.01 | --- | --- | 1.02 | 16.28 | 10.96 | --- | --- | 28.28 |
| 8.35 | 53,540 | 246.35 | 28.95 | 0.01 | --- | --- | 1.00 | 16.06 | 10.74 | --- | --- | 27.80 |
| 8.40 | 53,874 | 246.40 | 28.98 | 0.01 | --- | --- | 1.01 | 16.54 | 11.00 | --- | --- | 28.56 |
| 8.45 | 54,208 | 246.45 | 29.01 | 0.01 | --- | --- | 0.98 | 16.25 | 10.74 | --- | --- | 27.98 |
| 8.50 | 54,542 | 246.50 | 29.05 | 0.01 | --- | --- | 0.98 | 16.46 | 10.82 | --- | --- | 28.27 |

...End

Hydrograph Report

Hyd. No. 12

Basin 2 Out

Hydrograph type = Reservoir
 Storm frequency = 100 yrs
 Inflow hyd. No. = 9
 Max. Elevation = 233.92 ft

Peak discharge = 6.27 cfs
 Time interval = 2 min
 Reservoir name = Detention Basin 2
 Max. Storage = 20,659 cuft

Storage Indication method used.

Outflow hydrograph volume = 47,691 cuft

Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 716 | 5.27 | 232.38 | 6.68 | 0.26 | ---- | ---- | 0.52 | ---- | ---- | ---- | 0.043 | 0.83 |
| 720 | 7.13 | 232.58 | 6.68 | 0.28 | ---- | ---- | 0.97 | ---- | ---- | ---- | 0.044 | 1.30 |
| 724 | 9.87 | 232.85 | 6.68 | 0.31 | ---- | ---- | 1.72 | ---- | ---- | ---- | 0.045 | 2.08 |
| 728 | 11.73 | 233.17 | 6.68 | 0.34 | ---- | ---- | 2.80 | ---- | ---- | ---- | 0.046 | 3.18 |
| 732 | 11.64 | 233.49 | 6.68 | 0.36 | ---- | ---- | 4.00 | ---- | ---- | ---- | 0.047 | 4.41 |
| 736 | 10.22 | 233.73 | 6.68 | 0.38 | ---- | ---- | 4.99 | ---- | ---- | ---- | 0.047 | 5.42 |
| 740 | 8.39 | 233.87 | 6.68 | 0.39 | ---- | ---- | 5.61 | ---- | ---- | ---- | 0.048 | 6.05 |
| 744 | 6.51 | 233.92 << | 6.68 | 0.39 | ---- | ---- | 5.83 | ---- | ---- | ---- | 0.048 | 6.27 << |
| 748 | 5.13 | 233.90 | 6.68 | 0.39 | ---- | ---- | 5.75 | ---- | ---- | ---- | 0.048 | 6.19 |
| 752 | 4.13 | 233.84 | 6.68 | 0.39 | ---- | ---- | 5.49 | ---- | ---- | ---- | 0.048 | 5.93 |
| 756 | 3.26 | 233.76 | 6.68 | 0.38 | ---- | ---- | 5.13 | ---- | ---- | ---- | 0.048 | 5.56 |
| 760 | 2.59 | 233.66 | 6.68 | 0.38 | ---- | ---- | 4.72 | ---- | ---- | ---- | 0.047 | 5.14 |
| 764 | 2.15 | 233.56 | 6.68 | 0.37 | ---- | ---- | 4.30 | ---- | ---- | ---- | 0.047 | 4.71 |
| 768 | 1.89 | 233.46 | 6.68 | 0.36 | ---- | ---- | 3.90 | ---- | ---- | ---- | 0.047 | 4.31 |
| 772 | 1.73 | 233.37 | 6.68 | 0.35 | ---- | ---- | 3.54 | ---- | ---- | ---- | 0.046 | 3.94 |
| 776 | 1.63 | 233.29 | 6.68 | 0.35 | ---- | ---- | 3.23 | ---- | ---- | ---- | 0.046 | 3.62 |
| 780 | 1.52 | 233.22 | 6.68 | 0.34 | ---- | ---- | 2.95 | ---- | ---- | ---- | 0.046 | 3.34 |
| 784 | 1.42 | 233.15 | 6.68 | 0.34 | ---- | ---- | 2.71 | ---- | ---- | ---- | 0.046 | 3.09 |
| 788 | 1.34 | 233.08 | 6.68 | 0.33 | ---- | ---- | 2.49 | ---- | ---- | ---- | 0.045 | 2.87 |
| 792 | 1.27 | 233.03 | 6.68 | 0.33 | ---- | ---- | 2.29 | ---- | ---- | ---- | 0.045 | 2.66 |
| 796 | 1.22 | 232.98 | 6.68 | 0.32 | ---- | ---- | 2.12 | ---- | ---- | ---- | 0.045 | 2.49 |
| 800 | 1.19 | 232.93 | 6.68 | 0.32 | ---- | ---- | 1.97 | ---- | ---- | ---- | 0.045 | 2.33 |
| 804 | 1.16 | 232.88 | 6.68 | 0.31 | ---- | ---- | 1.84 | ---- | ---- | ---- | 0.045 | 2.20 |
| 808 | 1.13 | 232.85 | 6.68 | 0.31 | ---- | ---- | 1.72 | ---- | ---- | ---- | 0.045 | 2.07 |
| 812 | 1.11 | 232.81 | 6.68 | 0.31 | ---- | ---- | 1.61 | ---- | ---- | ---- | 0.045 | 1.96 |
| 816 | 1.08 | 232.78 | 6.68 | 0.30 | ---- | ---- | 1.51 | ---- | ---- | ---- | 0.045 | 1.86 |
| 820 | 1.05 | 232.75 | 6.68 | 0.30 | ---- | ---- | 1.43 | ---- | ---- | ---- | 0.044 | 1.78 |
| 824 | 1.03 | 232.72 | 6.68 | 0.30 | ---- | ---- | 1.36 | ---- | ---- | ---- | 0.044 | 1.70 |
| 828 | 1.00 | 232.70 | 6.68 | 0.30 | ---- | ---- | 1.29 | ---- | ---- | ---- | 0.044 | 1.63 |
| 832 | 0.97 | 232.67 | 6.68 | 0.29 | ---- | ---- | 1.22 | ---- | ---- | ---- | 0.044 | 1.56 |
| 836 | 0.94 | 232.65 | 6.68 | 0.29 | ---- | ---- | 1.16 | ---- | ---- | ---- | 0.044 | 1.49 |
| 840 | 0.92 | 232.63 | 6.68 | 0.29 | ---- | ---- | 1.10 | ---- | ---- | ---- | 0.044 | 1.43 |
| 844 | 0.89 | 232.61 | 6.68 | 0.29 | ---- | ---- | 1.05 | ---- | ---- | ---- | 0.044 | 1.38 |
| 848 | 0.87 | 232.59 | 6.68 | 0.29 | ---- | ---- | 1.00 | ---- | ---- | ---- | 0.044 | 1.33 |
| 852 | 0.85 | 232.57 | 6.68 | 0.28 | ---- | ---- | 0.96 | ---- | ---- | ---- | 0.044 | 1.29 |
| 856 | 0.83 | 232.56 | 6.68 | 0.28 | ---- | ---- | 0.92 | ---- | ---- | ---- | 0.044 | 1.25 |
| 860 | 0.82 | 232.54 | 6.68 | 0.28 | ---- | ---- | 0.88 | ---- | ---- | ---- | 0.044 | 1.21 |
| 864 | 0.80 | 232.53 | 6.68 | 0.28 | ---- | ---- | 0.85 | ---- | ---- | ---- | 0.044 | 1.17 |

Continues on next page...

Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 868 | 0.79 | 232.51 | 6.68 | 0.28 | ---- | ---- | 0.81 | ---- | ---- | ---- | 0.044 | 1.14 |
| 872 | 0.78 | 232.50 | 6.68 | 0.28 | ---- | ---- | 0.78 | ---- | ---- | ---- | 0.044 | 1.10 |
| 876 | 0.76 | 232.49 | 6.68 | 0.28 | ---- | ---- | 0.75 | ---- | ---- | ---- | 0.044 | 1.07 |
| 880 | 0.75 | 232.47 | 6.68 | 0.27 | ---- | ---- | 0.73 | ---- | ---- | ---- | 0.044 | 1.04 |
| 884 | 0.74 | 232.46 | 6.68 | 0.27 | ---- | ---- | 0.70 | ---- | ---- | ---- | 0.044 | 1.02 |
| 888 | 0.72 | 232.45 | 6.68 | 0.27 | ---- | ---- | 0.68 | ---- | ---- | ---- | 0.044 | 0.99 |
| 892 | 0.71 | 232.44 | 6.68 | 0.27 | ---- | ---- | 0.65 | ---- | ---- | ---- | 0.044 | 0.97 |
| 896 | 0.70 | 232.43 | 6.68 | 0.27 | ---- | ---- | 0.63 | ---- | ---- | ---- | 0.043 | 0.94 |
| 900 | 0.68 | 232.42 | 6.68 | 0.27 | ---- | ---- | 0.61 | ---- | ---- | ---- | 0.043 | 0.92 |
| 904 | 0.67 | 232.41 | 6.68 | 0.27 | ---- | ---- | 0.59 | ---- | ---- | ---- | 0.043 | 0.90 |
| 908 | 0.66 | 232.40 | 6.68 | 0.27 | ---- | ---- | 0.57 | ---- | ---- | ---- | 0.043 | 0.88 |
| 912 | 0.65 | 232.40 | 6.68 | 0.27 | ---- | ---- | 0.55 | ---- | ---- | ---- | 0.043 | 0.86 |
| 916 | 0.63 | 232.39 | 6.68 | 0.27 | ---- | ---- | 0.53 | ---- | ---- | ---- | 0.043 | 0.84 |
| 920 | 0.62 | 232.38 | 6.68 | 0.26 | ---- | ---- | 0.52 | ---- | ---- | ---- | 0.043 | 0.83 |
| 924 | 0.61 | 232.37 | 6.68 | 0.26 | ---- | ---- | 0.50 | ---- | ---- | ---- | 0.043 | 0.81 |
| 928 | 0.59 | 232.36 | 6.68 | 0.26 | ---- | ---- | 0.49 | ---- | ---- | ---- | 0.043 | 0.80 |
| 932 | 0.58 | 232.36 | 6.68 | 0.26 | ---- | ---- | 0.48 | ---- | ---- | ---- | 0.043 | 0.78 |
| 936 | 0.57 | 232.35 | 6.68 | 0.26 | ---- | ---- | 0.46 | ---- | ---- | ---- | 0.043 | 0.77 |
| 940 | 0.55 | 232.34 | 6.68 | 0.26 | ---- | ---- | 0.45 | ---- | ---- | ---- | 0.043 | 0.75 |
| 944 | 0.54 | 232.33 | 6.68 | 0.26 | ---- | ---- | 0.43 | ---- | ---- | ---- | 0.043 | 0.74 |
| 948 | 0.53 | 232.32 | 6.68 | 0.26 | ---- | ---- | 0.42 | ---- | ---- | ---- | 0.043 | 0.72 |
| 952 | 0.51 | 232.32 | 6.68 | 0.26 | ---- | ---- | 0.41 | ---- | ---- | ---- | 0.043 | 0.71 |
| 956 | 0.50 | 232.31 | 6.68 | 0.26 | ---- | ---- | 0.39 | ---- | ---- | ---- | 0.043 | 0.69 |
| 960 | 0.49 | 232.30 | 6.68 | 0.26 | ---- | ---- | 0.38 | ---- | ---- | ---- | 0.043 | 0.68 |
| 964 | 0.47 | 232.29 | 6.68 | 0.26 | ---- | ---- | 0.37 | ---- | ---- | ---- | 0.043 | 0.66 |
| 968 | 0.46 | 232.29 | 6.68 | 0.25 | ---- | ---- | 0.35 | ---- | ---- | ---- | 0.043 | 0.65 |
| 972 | 0.45 | 232.28 | 6.68 | 0.25 | ---- | ---- | 0.34 | ---- | ---- | ---- | 0.043 | 0.64 |

...End

Reservoir Report

Reservoir No. 2 - Detention Basin 2

Hydraflow Hydrographs by Intelisolve

Pond Data

Pond storage is based on known contour areas. Average end area method used.

Stage / Storage Table

| Stage (ft) | Elevation (ft) | Contour area (sqft) | Incr. Storage (cuft) | Total storage (cuft) |
|------------|----------------|---------------------|----------------------|----------------------|
| 0.00 | 229.33 | 00 | 0 | 0 |
| 0.67 | 230.00 | 2,454 | 822 | 822 |
| 2.67 | 232.00 | 5,689 | 8,143 | 8,965 |
| 4.67 | 234.00 | 6,522 | 12,211 | 21,176 |
| 6.67 | 236.00 | 7,413 | 13,935 | 35,111 |
| 8.67 | 238.00 | 9,192 | 16,605 | 51,716 |

Culvert / Orifice Structures

| | [A] | [B] | [C] | [D] |
|---------------|----------|--------|------|------|
| Rise in | = 6.0 | 3.0 | 0.0 | 0.0 |
| Span in | = 6.0 | 3.0 | 0.0 | 0.0 |
| No. Barrels | = 10 | 1 | 0 | 0 |
| Invert El. ft | = 228.40 | 231.00 | 0.00 | 0.00 |
| Length ft | = 40.0 | 1.0 | 0.0 | 0.0 |
| Slope % | = 1.00 | 0.00 | 0.00 | 0.00 |
| N-Value | = .013 | .013 | .000 | .000 |
| Orif. Coeff. | = 0.60 | 0.60 | 0.00 | 0.00 |
| Multi-Stage | = n/a | Yes | No | No |

Weir Structures

| | [A] | [B] | [C] | [D] |
|--------------|----------|--------|--------|------|
| Crest Len ft | = 0.66 | 20.00 | 16.00 | 0.00 |
| Crest El. ft | = 232.00 | 236.00 | 235.50 | 0.00 |
| Weir Coeff. | = 3.33 | 2.60 | 3.33 | 0.00 |
| Weir Type | = Rect | Broad | Rect | --- |
| Multi-Stage | = Yes | No | Yes | No |

Exfiltration Rate = 0.32 in/hr/sqft Tailwater Elev. = 0.00 ft

Stage / Storage / Discharge Table

Note: All outflows have been analyzed under inlet and outlet control.

| Stage ft | Storage cuft | Elevation ft | Civ A cfs | Civ B cfs | Civ C cfs | Civ D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Total cfs |
|----------|--------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-----------|
| 0.00 | 0 | 229.33 | 0.00 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.000 | 0.00 |
| 0.07 | 82 | 229.40 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.002 | 0.00 |
| 0.13 | 164 | 229.46 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.004 | 0.00 |
| 0.20 | 247 | 229.53 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.005 | 0.01 |
| 0.27 | 329 | 229.60 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.007 | 0.01 |
| 0.34 | 411 | 229.67 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.009 | 0.01 |
| 0.40 | 493 | 229.73 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.011 | 0.01 |
| 0.47 | 575 | 229.80 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.013 | 0.01 |
| 0.54 | 658 | 229.87 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.015 | 0.01 |
| 0.60 | 740 | 229.93 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.016 | 0.02 |
| 0.67 | 822 | 230.00 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.018 | 0.02 |
| 0.87 | 1,636 | 230.20 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.021 | 0.02 |
| 1.07 | 2,451 | 230.40 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.023 | 0.02 |
| 1.27 | 3,265 | 230.60 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.025 | 0.03 |
| 1.47 | 4,079 | 230.80 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.028 | 0.03 |
| 1.67 | 4,894 | 231.00 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.030 | 0.03 |
| 1.87 | 5,708 | 231.20 | 6.68 | 0.06 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.033 | 0.10 |
| 2.07 | 6,522 | 231.40 | 6.68 | 0.12 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.035 | 0.16 |
| 2.27 | 7,336 | 231.60 | 6.68 | 0.16 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.037 | 0.20 |
| 2.47 | 8,151 | 231.80 | 6.68 | 0.19 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.040 | 0.23 |
| 2.67 | 8,965 | 232.00 | 6.68 | 0.22 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.042 | 0.26 |
| 2.87 | 10,186 | 232.20 | 6.68 | 0.25 | --- | --- | 0.20 | 0.00 | 0.00 | --- | 0.043 | 0.48 |
| 3.07 | 11,407 | 232.40 | 6.68 | 0.27 | --- | --- | 0.56 | 0.00 | 0.00 | --- | 0.043 | 0.87 |
| 3.27 | 12,628 | 232.60 | 6.68 | 0.29 | --- | --- | 1.02 | 0.00 | 0.00 | --- | 0.044 | 1.35 |
| 3.47 | 13,849 | 232.80 | 6.68 | 0.31 | --- | --- | 1.57 | 0.00 | 0.00 | --- | 0.045 | 1.92 |
| 3.67 | 15,071 | 233.00 | 6.68 | 0.32 | --- | --- | 2.20 | 0.00 | 0.00 | --- | 0.045 | 2.57 |
| 3.87 | 16,292 | 233.20 | 6.68 | 0.34 | --- | --- | 2.89 | 0.00 | 0.00 | --- | 0.046 | 3.28 |
| 4.07 | 17,513 | 233.40 | 6.68 | 0.36 | --- | --- | 3.64 | 0.00 | 0.00 | --- | 0.046 | 4.04 |
| 4.27 | 18,734 | 233.60 | 6.68 | 0.37 | --- | --- | 4.45 | 0.00 | 0.00 | --- | 0.047 | 4.87 |
| 4.47 | 19,955 | 233.80 | 6.68 | 0.39 | --- | --- | 5.31 | 0.00 | 0.00 | --- | 0.048 | 5.74 |
| 4.67 | 21,176 | 234.00 | 6.68 | 0.40 | --- | --- | 6.22 | 0.00 | 0.00 | --- | 0.048 | 6.67 |
| 4.87 | 22,570 | 234.20 | 7.59 | 0.41 | --- | --- | 7.17 | 0.00 | 0.00 | --- | 0.049 | 7.64 |

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Stage / Storage / Discharge Table

| Stage ft | Storage cuft | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Total cfs |
|-------------|-----------------|-----------------|--------------|--------------|--------------|--------------|-------------|-------------|-------------|-------------|--------------|--------------|
| 5.07 | 23,963 | 234.40 | 8.60 | 0.43 | --- | --- | 8.17 | 0.00 | 0.00 | --- | 0.050 | 8.65 |
| 5.27 | 25,357 | 234.60 | 9.65 | 0.44 | --- | --- | 9.21 | 0.00 | 0.00 | --- | 0.050 | 9.70 |
| 5.47 | 26,750 | 234.80 | 10.75 | 0.45 | --- | --- | 10.30 | 0.00 | 0.00 | --- | 0.051 | 10.80 |
| 5.67 | 28,144 | 235.00 | 11.89 | 0.47 | --- | --- | 11.42 | 0.00 | 0.00 | --- | 0.052 | 11.94 |
| 5.87 | 29,537 | 235.20 | 13.03 | 0.44 | --- | --- | 12.58 | 0.00 | 0.00 | --- | 0.052 | 13.08 |
| 6.07 | 30,931 | 235.40 | 14.12 | 0.42 | --- | --- | 13.70 | 0.00 | 0.00 | --- | 0.053 | 14.17 |
| 6.27 | 32,324 | 235.60 | 15.89 | 0.37 | --- | --- | 13.84 | 0.00 | 1.68 | --- | 0.054 | 15.94 |
| 6.47 | 33,718 | 235.80 | 18.81 | 0.20 | --- | --- | 9.85 | 0.00 | 8.75 | --- | 0.054 | 18.86 |
| 6.67 | 35,111 | 236.00 | 19.86 | 0.10 | --- | --- | 5.97 | 0.00 | 13.80 | --- | 0.055 | 19.92 |
| 6.87 | 36,772 | 236.20 | 20.25 | 0.07 | --- | --- | 4.74 | 4.65 | 15.44 | --- | 0.056 | 24.95 |
| 7.07 | 38,432 | 236.40 | 20.56 | 0.05 | --- | --- | 4.01 | 13.15 | 16.50 | --- | 0.058 | 33.77 |
| 7.27 | 40,093 | 236.60 | 20.84 | 0.04 | --- | --- | 3.52 | 24.17 | 17.27 | --- | 0.059 | 45.05 |
| 7.47 | 41,753 | 236.80 | 21.10 | 0.03 | --- | --- | 3.17 | 37.21 | 17.88 | --- | 0.060 | 58.35 |
| 7.67 | 43,414 | 237.00 | 21.36 | 0.03 | --- | --- | 2.91 | 52.00 | 18.41 | --- | 0.061 | 73.40 |
| 7.87 | 45,074 | 237.20 | 21.62 | 0.02 | --- | --- | 2.71 | 68.35 | 18.85 | --- | 0.063 | 90.00 |
| 8.07 | 46,735 | 237.40 | 21.87 | 0.02 | --- | --- | 2.54 | 86.14 | 19.22 | --- | 0.064 | 107.99 |
| 8.27 | 48,395 | 237.60 | 22.12 | 0.02 | --- | --- | 2.41 | 105.24 | 19.56 | --- | 0.065 | 127.29 |
| 8.47 | 50,056 | 237.80 | 22.36 | 0.02 | --- | --- | 2.31 | 125.57 | 19.95 | --- | 0.067 | 147.91 |
| 8.67 | 51,716 | 238.00 | 22.60 | 0.01 | --- | --- | 2.21 | 147.08 | 20.20 | --- | 0.068 | 169.58 |

...End

Hydrograph Report

Hyd. No. 13

Basin 3 Out

Hydrograph type = Reservoir
 Storm frequency = 100 yrs
 Inflow hyd. No. = 10
 Max. Elevation = 225.66 ft

Peak discharge = 5.59 cfs
 Time interval = 2 min
 Reservoir name = Basin 3 (Hotel)
 Max. Storage = 28,658 cuft

Storage Indication method used.

Outflow hydrograph volume = 66,824 cuft

Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 724 | 18.19 | 224.05 | 10.70 | 0.53 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | 0.58 |
| 728 | 18.09 | 224.68 | 10.70 | 0.56 | 1.64 | ---- | ---- | ---- | ---- | ---- | ---- | 2.20 |
| 732 | 13.60 | 225.15 | 10.70 | 0.59 | 3.04 | ---- | ---- | ---- | ---- | ---- | ---- | 3.63 |
| 736 | 9.86 | 225.42 | 10.70 | 0.60 | 3.63 | ---- | 0.25 | ---- | ---- | ---- | ---- | 4.48 |
| 740 | 8.05 | 225.57 | 10.70 | 0.61 | 3.91 | ---- | 0.61 | ---- | ---- | ---- | ---- | 5.13 |
| 744 | 6.76 | 225.64 | 10.70 | 0.61 | 4.04 | ---- | 0.84 | ---- | ---- | ---- | ---- | 5.49 |
| 748 | 5.45 | 225.66 << | 10.70 | 0.61 | 4.08 | ---- | 0.90 | ---- | ---- | ---- | ---- | 5.59 << |
| 752 | 4.15 | 225.64 | 10.70 | 0.61 | 4.03 | ---- | 0.81 | ---- | ---- | ---- | ---- | 5.45 |
| 756 | 3.16 | 225.58 | 10.70 | 0.61 | 3.92 | ---- | 0.63 | ---- | ---- | ---- | ---- | 5.16 |
| 760 | 2.67 | 225.50 | 10.70 | 0.60 | 3.78 | ---- | 0.44 | ---- | ---- | ---- | ---- | 4.82 |
| 764 | 2.47 | 225.42 | 10.70 | 0.60 | 3.63 | ---- | 0.25 | ---- | ---- | ---- | ---- | 4.49 |
| 768 | 2.33 | 225.35 | 10.70 | 0.60 | 3.49 | ---- | 0.15 | ---- | ---- | ---- | ---- | 4.23 |
| 772 | 2.19 | 225.29 | 10.70 | 0.59 | 3.35 | ---- | 0.08 | ---- | ---- | ---- | ---- | 4.02 |
| 776 | 2.05 | 225.22 | 10.70 | 0.59 | 3.21 | ---- | 0.02 | ---- | ---- | ---- | ---- | 3.82 |
| 780 | 1.91 | 225.16 | 10.70 | 0.59 | 3.06 | ---- | ---- | ---- | ---- | ---- | ---- | 3.65 |
| 784 | 1.78 | 225.10 | 10.70 | 0.58 | 2.91 | ---- | ---- | ---- | ---- | ---- | ---- | 3.49 |
| 788 | 1.69 | 225.03 | 10.70 | 0.58 | 2.76 | ---- | ---- | ---- | ---- | ---- | ---- | 3.34 |
| 792 | 1.64 | 224.98 | 10.70 | 0.58 | 2.60 | ---- | ---- | ---- | ---- | ---- | ---- | 3.18 |
| 796 | 1.61 | 224.92 | 10.70 | 0.58 | 2.44 | ---- | ---- | ---- | ---- | ---- | ---- | 3.02 |
| 800 | 1.57 | 224.87 | 10.70 | 0.57 | 2.30 | ---- | ---- | ---- | ---- | ---- | ---- | 2.87 |
| 804 | 1.53 | 224.83 | 10.70 | 0.57 | 2.16 | ---- | ---- | ---- | ---- | ---- | ---- | 2.73 |
| 808 | 1.50 | 224.79 | 10.70 | 0.57 | 2.03 | ---- | ---- | ---- | ---- | ---- | ---- | 2.60 |
| 812 | 1.46 | 224.75 | 10.70 | 0.57 | 1.89 | ---- | ---- | ---- | ---- | ---- | ---- | 2.45 |
| 816 | 1.43 | 224.72 | 10.70 | 0.56 | 1.76 | ---- | ---- | ---- | ---- | ---- | ---- | 2.33 |
| 820 | 1.39 | 224.68 | 10.70 | 0.56 | 1.65 | ---- | ---- | ---- | ---- | ---- | ---- | 2.21 |
| 824 | 1.35 | 224.66 | 10.70 | 0.56 | 1.54 | ---- | ---- | ---- | ---- | ---- | ---- | 2.11 |
| 828 | 1.32 | 224.63 | 10.70 | 0.56 | 1.45 | ---- | ---- | ---- | ---- | ---- | ---- | 2.01 |
| 832 | 1.28 | 224.61 | 10.70 | 0.56 | 1.36 | ---- | ---- | ---- | ---- | ---- | ---- | 1.92 |
| 836 | 1.24 | 224.58 | 10.70 | 0.56 | 1.28 | ---- | ---- | ---- | ---- | ---- | ---- | 1.84 |
| 840 | 1.21 | 224.56 | 10.70 | 0.56 | 1.21 | ---- | ---- | ---- | ---- | ---- | ---- | 1.76 |
| 844 | 1.17 | 224.54 | 10.70 | 0.56 | 1.14 | ---- | ---- | ---- | ---- | ---- | ---- | 1.69 |
| 848 | 1.14 | 224.52 | 10.70 | 0.56 | 1.07 | ---- | ---- | ---- | ---- | ---- | ---- | 1.63 |
| 852 | 1.12 | 224.51 | 10.70 | 0.55 | 1.01 | ---- | ---- | ---- | ---- | ---- | ---- | 1.57 |
| 856 | 1.11 | 224.49 | 10.70 | 0.55 | 0.96 | ---- | ---- | ---- | ---- | ---- | ---- | 1.51 |
| 860 | 1.09 | 224.48 | 10.70 | 0.55 | 0.91 | ---- | ---- | ---- | ---- | ---- | ---- | 1.46 |
| 864 | 1.07 | 224.46 | 10.70 | 0.55 | 0.86 | ---- | ---- | ---- | ---- | ---- | ---- | 1.42 |
| 868 | 1.05 | 224.45 | 10.70 | 0.55 | 0.82 | ---- | ---- | ---- | ---- | ---- | ---- | 1.37 |
| 872 | 1.04 | 224.44 | 10.70 | 0.55 | 0.78 | ---- | ---- | ---- | ---- | ---- | ---- | 1.33 |

Continues on next page...

Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 876 | 1.02 | 224.43 | 10.70 | 0.55 | 0.75 | ---- | ---- | ---- | ---- | ---- | ---- | 1.30 |
| 880 | 1.00 | 224.42 | 10.70 | 0.55 | 0.71 | ---- | ---- | ---- | ---- | ---- | ---- | 1.26 |
| 884 | 0.98 | 224.41 | 10.70 | 0.55 | 0.68 | ---- | ---- | ---- | ---- | ---- | ---- | 1.23 |
| 888 | 0.97 | 224.40 | 10.70 | 0.55 | 0.65 | ---- | ---- | ---- | ---- | ---- | ---- | 1.20 |
| 892 | 0.95 | 224.40 | 10.70 | 0.55 | 0.63 | ---- | ---- | ---- | ---- | ---- | ---- | 1.17 |
| 896 | 0.93 | 224.39 | 10.70 | 0.55 | 0.61 | ---- | ---- | ---- | ---- | ---- | ---- | 1.16 |
| 900 | 0.91 | 224.38 | 10.70 | 0.55 | 0.59 | ---- | ---- | ---- | ---- | ---- | ---- | 1.14 |
| 904 | 0.89 | 224.37 | 10.70 | 0.55 | 0.57 | ---- | ---- | ---- | ---- | ---- | ---- | 1.12 |
| 908 | 0.88 | 224.36 | 10.70 | 0.55 | 0.55 | ---- | ---- | ---- | ---- | ---- | ---- | 1.10 |
| 912 | 0.86 | 224.35 | 10.70 | 0.55 | 0.53 | ---- | ---- | ---- | ---- | ---- | ---- | 1.08 |
| 916 | 0.84 | 224.35 | 10.70 | 0.55 | 0.51 | ---- | ---- | ---- | ---- | ---- | ---- | 1.06 |
| 920 | 0.82 | 224.34 | 10.70 | 0.55 | 0.50 | ---- | ---- | ---- | ---- | ---- | ---- | 1.04 |
| 924 | 0.81 | 224.33 | 10.70 | 0.55 | 0.48 | ---- | ---- | ---- | ---- | ---- | ---- | 1.02 |
| 928 | 0.79 | 224.32 | 10.70 | 0.55 | 0.46 | ---- | ---- | ---- | ---- | ---- | ---- | 1.01 |
| 932 | 0.77 | 224.32 | 10.70 | 0.54 | 0.44 | ---- | ---- | ---- | ---- | ---- | ---- | 0.99 |
| 936 | 0.75 | 224.31 | 10.70 | 0.54 | 0.42 | ---- | ---- | ---- | ---- | ---- | ---- | 0.97 |
| 940 | 0.73 | 224.30 | 10.70 | 0.54 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | 0.95 |
| 944 | 0.72 | 224.29 | 10.70 | 0.54 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | 0.93 |
| 948 | 0.70 | 224.28 | 10.70 | 0.54 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | 0.91 |
| 952 | 0.68 | 224.28 | 10.70 | 0.54 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | 0.89 |
| 956 | 0.66 | 224.27 | 10.70 | 0.54 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | 0.88 |
| 960 | 0.64 | 224.26 | 10.70 | 0.54 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | 0.86 |
| 964 | 0.63 | 224.25 | 10.70 | 0.54 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | 0.84 |
| 968 | 0.61 | 224.25 | 10.70 | 0.54 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | 0.82 |
| 972 | 0.61 | 224.24 | 10.70 | 0.54 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | 0.80 |
| 976 | 0.60 | 224.23 | 10.70 | 0.54 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | 0.79 |
| 980 | 0.59 | 224.22 | 10.70 | 0.54 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | 0.77 |
| 984 | 0.58 | 224.22 | 10.70 | 0.54 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | 0.76 |
| 988 | 0.57 | 224.21 | 10.70 | 0.54 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | 0.74 |
| 992 | 0.57 | 224.21 | 10.70 | 0.54 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | 0.73 |
| 996 | 0.56 | 224.20 | 10.70 | 0.54 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | 0.72 |
| 1000 | 0.55 | 224.19 | 10.70 | 0.54 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | 0.71 |
| 1004 | 0.54 | 224.19 | 10.70 | 0.54 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | 0.71 |
| 1008 | 0.53 | 224.18 | 10.70 | 0.54 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | 0.70 |
| 1012 | 0.53 | 224.18 | 10.70 | 0.54 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | 0.69 |
| 1016 | 0.52 | 224.17 | 10.70 | 0.54 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | 0.69 |
| 1020 | 0.51 | 224.16 | 10.70 | 0.54 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | 0.68 |
| 1024 | 0.50 | 224.16 | 10.70 | 0.54 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | 0.68 |
| 1028 | 0.50 | 224.15 | 10.70 | 0.54 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | 0.67 |
| 1032 | 0.49 | 224.14 | 10.70 | 0.54 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | 0.66 |
| 1036 | 0.48 | 224.14 | 10.70 | 0.54 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | 0.66 |
| 1040 | 0.47 | 224.13 | 10.70 | 0.54 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | 0.65 |
| 1044 | 0.46 | 224.13 | 10.70 | 0.53 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | 0.65 |
| 1048 | 0.46 | 224.12 | 10.70 | 0.53 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | 0.64 |
| 1052 | 0.45 | 224.11 | 10.70 | 0.53 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | 0.63 |
| 1056 | 0.44 | 224.11 | 10.70 | 0.53 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | 0.63 |
| 1060 | 0.43 | 224.10 | 10.70 | 0.53 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | 0.62 |
| 1064 | 0.42 | 224.09 | 10.70 | 0.53 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | 0.61 |
| 1068 | 0.42 | 224.08 | 10.70 | 0.53 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | 0.61 |
| 1072 | 0.41 | 224.08 | 10.70 | 0.53 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | 0.60 |
| 1076 | 0.40 | 224.07 | 10.70 | 0.53 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | 0.59 |

Continues on next page...

Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|-----------------------|-----------------------|-------------------------|----------------------|----------------------|----------------------|----------------------|---------------------|---------------------|---------------------|---------------------|----------------------|------------------------|
| 1080 | 0.39 | 224.06 | 10.70 | 0.53 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | 0.59 |
| 1084 | 0.39 | 224.06 | 10.70 | 0.53 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | 0.58 |
| 1088 | 0.38 | 224.05 | 10.70 | 0.53 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | 0.57 |
| 1092 | 0.38 | 224.04 | 10.70 | 0.53 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | 0.57 |
| 1096 | 0.38 | 224.04 | 10.70 | 0.53 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | 0.56 |

...End

Reservoir Report

Reservoir No. 3 - Basin 3 (Hotel)

Hydraflow Hydrographs by Intelisolve

Pond Data

Pond storage is based on known contour areas. Average end area method used.

Stage / Storage Table

| Stage (ft) | Elevation (ft) | Contour area (sqft) | Incr. Storage (cuft) | Total storage (cuft) |
|------------|----------------|---------------------|----------------------|----------------------|
| 0.00 | 219.00 | 00 | 0 | 0 |
| 1.00 | 220.00 | 1,406 | 703 | 703 |
| 3.00 | 222.00 | 4,776 | 6,182 | 6,885 |
| 5.00 | 224.00 | 5,971 | 10,747 | 17,632 |
| 7.00 | 226.00 | 7,278 | 13,249 | 30,881 |
| 9.00 | 228.00 | 8,709 | 15,987 | 46,868 |
| 9.50 | 228.50 | 9,086 | 4,449 | 51,317 |

Culvert / Orifice Structures

| | [A] | [B] | [C] | [D] |
|---------------|----------|--------|--------|------|
| Rise in | = 24.0 | 3.0 | 12.0 | 0.0 |
| Span in | = 24.0 | 3.0 | 12.0 | 0.0 |
| No. Barrels | = 1 | 1 | 1 | 0 |
| Invert El. ft | = 217.50 | 217.90 | 224.00 | 0.00 |
| Length ft | = 48.0 | 1.0 | 1.0 | 0.0 |
| Slope % | = 10.00 | 0.00 | 0.00 | 0.00 |
| N-Value | = .013 | .013 | .013 | .000 |
| Orif. Coeff. | = 0.60 | 0.60 | 0.60 | 0.00 |
| Multi-Stage | = n/a | Yes | Yes | No |

Weir Structures

| | [A] | [B] | [C] | [D] |
|--------------|----------|--------|--------|--------|
| Crest Len ft | = 1.00 | 2.00 | 16.00 | 90.00 |
| Crest El. ft | = 225.25 | 226.00 | 227.00 | 227.00 |
| Weir Coeff. | = 3.33 | 3.33 | 3.33 | 2.60 |
| Weir Type | = Rect | Rect | Rect | Broad |
| Multi-Stage | = Yes | Yes | Yes | Yes |

Exfiltration Rate = 0.00 in/hr/sqft Tailwater Elev. = 0.00 ft

Stage / Storage / Discharge Table

Note: All outflows have been analyzed under inlet and outlet control.

| Stage ft | Storage cuft | Elevation ft | Civ A cfs | Civ B cfs | Civ C cfs | Civ D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Total cfs |
|----------|--------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-----------|
| 0.00 | 0 | 219.00 | 0.00 | 0.00 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.00 |
| 0.10 | 70 | 219.10 | 10.70 | 0.07 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.07 |
| 0.20 | 141 | 219.20 | 10.70 | 0.11 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.11 |
| 0.30 | 211 | 219.30 | 10.70 | 0.13 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.13 |
| 0.40 | 281 | 219.40 | 10.70 | 0.15 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.15 |
| 0.50 | 352 | 219.50 | 10.70 | 0.17 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.17 |
| 0.60 | 422 | 219.60 | 10.70 | 0.18 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.18 |
| 0.70 | 492 | 219.70 | 10.70 | 0.20 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.20 |
| 0.80 | 562 | 219.80 | 10.70 | 0.21 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.21 |
| 0.90 | 633 | 219.90 | 10.70 | 0.22 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.22 |
| 1.00 | 703 | 220.00 | 10.70 | 0.24 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.24 |
| 1.20 | 1,321 | 220.20 | 10.70 | 0.26 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.26 |
| 1.40 | 1,939 | 220.40 | 10.70 | 0.28 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.28 |
| 1.60 | 2,558 | 220.60 | 10.70 | 0.30 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.30 |
| 1.80 | 3,176 | 220.80 | 10.70 | 0.32 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.32 |
| 2.00 | 3,794 | 221.00 | 10.70 | 0.33 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.33 |
| 2.20 | 4,412 | 221.20 | 10.70 | 0.35 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.35 |
| 2.40 | 5,030 | 221.40 | 10.70 | 0.37 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.37 |
| 2.60 | 5,649 | 221.60 | 10.70 | 0.38 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.38 |
| 2.80 | 6,267 | 221.80 | 10.70 | 0.40 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.40 |
| 3.00 | 6,885 | 222.00 | 10.70 | 0.41 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.41 |
| 3.20 | 7,960 | 222.20 | 10.70 | 0.42 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.42 |
| 3.40 | 9,034 | 222.40 | 10.70 | 0.44 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.44 |
| 3.60 | 10,109 | 222.60 | 10.70 | 0.45 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.45 |
| 3.80 | 11,184 | 222.80 | 10.70 | 0.46 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.46 |
| 4.00 | 12,259 | 223.00 | 10.70 | 0.47 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.47 |
| 4.20 | 13,333 | 223.20 | 10.70 | 0.48 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.48 |
| 4.40 | 14,408 | 223.40 | 10.70 | 0.50 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.50 |
| 4.60 | 15,483 | 223.60 | 10.70 | 0.51 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.51 |
| 4.80 | 16,557 | 223.80 | 10.70 | 0.52 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.52 |
| 5.00 | 17,632 | 224.00 | 10.70 | 0.53 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.53 |

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Stage / Storage / Discharge Table

| Stage ft | Storage cuft | Elevation ft | Civ A cfs | Civ B cfs | Civ C cfs | Civ D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Total cfs |
|-------------|-----------------|-----------------|--------------|--------------|--------------|--------------|-------------|-------------|-------------|-------------|--------------|--------------|
| 5.20 | 18,957 | 224.20 | 10.70 | 0.54 | 0.18 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.72 |
| 5.40 | 20,282 | 224.40 | 10.70 | 0.55 | 0.64 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 1.19 |
| 5.60 | 21,607 | 224.60 | 10.70 | 0.56 | 1.34 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 1.90 |
| 5.80 | 22,932 | 224.80 | 10.70 | 0.57 | 2.07 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 2.64 |
| 6.00 | 24,257 | 225.00 | 10.70 | 0.58 | 2.67 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 3.25 |
| 6.20 | 25,581 | 225.20 | 10.70 | 0.59 | 3.16 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 3.75 |
| 6.40 | 26,906 | 225.40 | 10.70 | 0.60 | 3.59 | --- | 0.19 | 0.00 | 0.00 | 0.00 | --- | 4.38 |
| 6.60 | 28,231 | 225.60 | 10.70 | 0.61 | 3.97 | --- | 0.69 | 0.00 | 0.00 | 0.00 | --- | 5.26 |
| 6.80 | 29,556 | 225.80 | 10.70 | 0.62 | 4.31 | --- | 1.36 | 0.00 | 0.00 | 0.00 | --- | 6.29 |
| 7.00 | 30,881 | 226.00 | 10.70 | 0.63 | 4.63 | --- | 2.16 | 0.00 | 0.00 | 0.00 | --- | 7.42 |
| 7.20 | 32,480 | 226.20 | 10.70 | 0.63 | 4.93 | --- | 3.08 | 0.60 | 0.00 | 0.00 | --- | 9.24 |
| 7.40 | 34,078 | 226.40 | 11.69 | 0.64 | 5.21 | --- | 4.11 | 1.68 | 0.00 | 0.00 | --- | 11.64 |
| 7.60 | 35,677 | 226.60 | 14.47 | 0.63 | 5.48 | --- | 5.22 | 3.10 | 0.00 | 0.00 | --- | 14.43 |
| 7.80 | 37,276 | 226.80 | 17.55 | 0.62 | 5.73 | --- | 6.43 | 4.77 | 0.00 | 0.00 | --- | 17.55 |
| 8.00 | 38,875 | 227.00 | 20.95 | 0.61 | 5.98 | --- | 7.71 | 6.66 | 0.00 | 0.00 | --- | 20.95 |
| 8.20 | 40,473 | 227.20 | 42.98 | 0.19 | 2.99 | --- | 6.61 | 7.50 | 4.76 | 20.93 | --- | 42.98 |
| 8.40 | 42,072 | 227.40 | 45.00 | 0.05 | 0.84 | --- | 2.87 | 3.56 | 6.98 | 30.65 | --- | 44.96 |
| 8.60 | 43,671 | 227.60 | 45.58 | 0.03 | 0.50 | --- | 2.13 | 2.78 | 7.43 | 32.62 | --- | 45.49 |
| 8.80 | 45,269 | 227.80 | 46.10 | 0.02 | 0.35 | --- | 1.75 | 2.38 | 7.69 | 33.77 | --- | 45.95 |
| 9.00 | 46,868 | 228.00 | 46.61 | 0.02 | 0.26 | --- | 1.53 | 2.14 | 7.90 | 34.69 | --- | 46.53 |
| 9.05 | 47,313 | 228.05 | 46.73 | 0.02 | 0.24 | --- | 1.48 | 2.09 | 7.91 | 34.75 | --- | 46.48 |
| 9.10 | 47,758 | 228.10 | 46.85 | 0.01 | 0.23 | --- | 1.43 | 2.04 | 7.92 | 34.79 | --- | 46.41 |
| 9.15 | 48,203 | 228.15 | 46.98 | 0.01 | 0.21 | --- | 1.39 | 2.00 | 7.95 | 34.93 | --- | 46.50 |
| 9.20 | 48,648 | 228.20 | 47.10 | 0.01 | 0.20 | --- | 1.37 | 1.97 | 8.02 | 35.22 | --- | 46.79 |
| 9.25 | 49,092 | 228.25 | 47.22 | 0.01 | 0.19 | --- | 1.33 | 1.94 | 8.04 | 35.33 | --- | 46.85 |
| 9.30 | 49,537 | 228.30 | 47.34 | 0.01 | 0.18 | --- | 1.30 | 1.89 | 8.01 | 35.19 | --- | 46.59 |
| 9.35 | 49,982 | 228.35 | 47.46 | 0.01 | 0.17 | --- | 1.27 | 1.87 | 8.07 | 35.43 | --- | 46.82 |
| 9.40 | 50,427 | 228.40 | 47.58 | 0.01 | 0.16 | --- | 1.25 | 1.84 | 8.07 | 35.43 | --- | 46.76 |
| 9.45 | 50,872 | 228.45 | 47.70 | 0.01 | 0.16 | --- | 1.24 | 1.84 | 8.21 | 36.07 | --- | 47.54 |
| 9.50 | 51,317 | 228.50 | 47.83 | 0.01 | 0.15 | --- | 1.20 | 1.79 | 8.08 | 35.50 | --- | 46.73 |

...End

Hydrograph Report

Hyd. No. 14

Hydrograph type = Combine
Storm frequency = 100 yrs
Inflow hyds. = 11, 12, 13

Peak discharge = 13.56 cfs
Time interval = 2 min

Hydrograph Volume = 156,118 cuft

Hydrograph Discharge Table

| Time (min) | Hyd. 11 + (cfs) | Hyd. 12 + (cfs) | Hyd. 13 = (cfs) | Outflow (cfs) |
|------------|-----------------|-----------------|-----------------|---------------|
| 716 | 0.25 | 0.83 | 0.47 | 1.79 |
| 720 | 0.27 | 1.30 | 0.50 | 2.49 |
| 724 | 0.30 | 2.08 | 0.58 | 3.63 |
| 728 | 0.33 | 3.18 | 2.20 | 6.74 |
| 732 | 0.36 | 4.41 | 3.63 | 9.70 |
| 736 | 0.38 | 5.42 | 4.48 | 11.69 |
| 740 | 0.40 | 6.05 | 5.13 | 12.90 |
| 744 | 0.63 | 6.27 << | 5.49 | 13.50 |
| 748 | 0.92 | 6.19 | 5.59 << | 13.54 |
| 752 | 1.17 | 5.93 | 5.45 | 13.13 |
| 756 | 1.34 | 5.56 | 5.16 | 12.39 |
| 760 | 1.44 | 5.14 | 4.82 | 11.54 |
| 764 | 1.48 | 4.71 | 4.49 | 10.66 |
| 768 | 1.50 | 4.31 | 4.23 | 9.92 |
| 772 | 1.50 | 3.94 | 4.02 | 9.25 |
| 776 | 1.48 | 3.62 | 3.82 | 8.68 |
| 780 | 1.46 | 3.34 | 3.65 | 8.17 |
| 784 | 1.43 | 3.09 | 3.49 | 7.71 |
| 788 | 1.40 | 2.87 | 3.34 | 7.30 |
| 792 | 1.36 | 2.66 | 3.18 | 6.91 |
| 796 | 1.32 | 2.49 | 3.02 | 6.54 |
| 800 | 1.29 | 2.33 | 2.87 | 6.20 |
| 804 | 1.26 | 2.20 | 2.73 | 5.89 |
| 808 | 1.23 | 2.07 | 2.60 | 5.63 |
| 812 | 1.20 | 1.96 | 2.45 | 5.37 |
| 816 | 1.18 | 1.86 | 2.33 | 5.13 |
| 820 | 1.15 | 1.78 | 2.21 | 4.92 |
| 824 | 1.12 | 1.70 | 2.11 | 4.72 |
| 828 | 1.10 | 1.63 | 2.01 | 4.53 |
| 832 | 1.07 | 1.56 | 1.92 | 4.36 |
| 836 | 1.05 | 1.49 | 1.84 | 4.20 |
| 840 | 1.02 | 1.43 | 1.76 | 4.05 |
| 844 | 1.00 | 1.38 | 1.69 | 3.91 |
| 848 | 0.98 | 1.33 | 1.63 | 3.77 |
| 852 | 0.95 | 1.29 | 1.57 | 3.65 |
| 856 | 0.93 | 1.25 | 1.51 | 3.54 |
| 860 | 0.91 | 1.21 | 1.46 | 3.44 |
| 864 | 0.89 | 1.17 | 1.42 | 3.35 |

Continues on next page...

Hydrograph Discharge Table

| Time (min) | Hyd. 11 + (cfs) | Hyd. 12 + (cfs) | Hyd. 13 = (cfs) | Outflow (cfs) |
|---------------|--------------------|--------------------|--------------------|------------------|
| 868 | 0.87 | 1.14 | 1.37 | 3.26 |
| 872 | 0.85 | 1.10 | 1.33 | 3.18 |
| 876 | 0.83 | 1.07 | 1.30 | 3.10 |
| 880 | 0.81 | 1.04 | 1.26 | 3.02 |
| 884 | 0.80 | 1.02 | 1.23 | 2.95 |
| 888 | 0.78 | 0.99 | 1.20 | 2.88 |
| 892 | 0.76 | 0.97 | 1.17 | 2.82 |
| 896 | 0.75 | 0.94 | 1.16 | 2.77 |
| 900 | 0.73 | 0.92 | 1.14 | 2.72 |
| 904 | 0.72 | 0.90 | 1.12 | 2.67 |
| 908 | 0.71 | 0.88 | 1.10 | 2.62 |
| 912 | 0.70 | 0.86 | 1.08 | 2.57 |
| 916 | 0.69 | 0.84 | 1.06 | 2.53 |
| 920 | 0.68 | 0.83 | 1.04 | 2.49 |
| 924 | 0.67 | 0.81 | 1.02 | 2.44 |
| 928 | 0.67 | 0.80 | 1.01 | 2.40 |
| 932 | 0.66 | 0.78 | 0.99 | 2.36 |
| 936 | 0.65 | 0.77 | 0.97 | 2.32 |
| 940 | 0.64 | 0.75 | 0.95 | 2.27 |
| 944 | 0.63 | 0.74 | 0.93 | 2.23 |
| 948 | 0.62 | 0.72 | 0.91 | 2.19 |
| 952 | 0.61 | 0.71 | 0.89 | 2.15 |
| 956 | 0.60 | 0.69 | 0.88 | 2.10 |
| 960 | 0.59 | 0.68 | 0.86 | 2.06 |
| 964 | 0.58 | 0.66 | 0.84 | 2.02 |
| 968 | 0.57 | 0.65 | 0.82 | 1.98 |
| 972 | 0.56 | 0.64 | 0.80 | 1.94 |
| 976 | 0.55 | 0.62 | 0.79 | 1.91 |
| 980 | 0.54 | 0.61 | 0.77 | 1.88 |
| 984 | 0.53 | 0.60 | 0.76 | 1.84 |
| 988 | 0.52 | 0.58 | 0.74 | 1.81 |
| 992 | 0.52 | 0.57 | 0.73 | 1.78 |
| 996 | 0.51 | 0.56 | 0.72 | 1.75 |
| 1000 | 0.50 | 0.55 | 0.71 | 1.73 |
| 1004 | 0.49 | 0.54 | 0.71 | 1.71 |
| 1008 | 0.48 | 0.53 | 0.70 | 1.69 |
| 1012 | 0.47 | 0.52 | 0.69 | 1.67 |
| 1016 | 0.47 | 0.51 | 0.69 | 1.65 |
| 1020 | 0.46 | 0.50 | 0.68 | 1.63 |
| 1024 | 0.45 | 0.49 | 0.68 | 1.61 |
| 1028 | 0.45 | 0.48 | 0.67 | 1.59 |
| 1032 | 0.44 | 0.48 | 0.66 | 1.57 |
| 1036 | 0.43 | 0.47 | 0.66 | 1.55 |
| 1040 | 0.42 | 0.47 | 0.65 | 1.53 |
| 1044 | 0.42 | 0.46 | 0.65 | 1.51 |
| 1048 | 0.41 | 0.46 | 0.64 | 1.49 |
| 1052 | 0.40 | 0.45 | 0.63 | 1.47 |
| 1056 | 0.40 | 0.45 | 0.63 | 1.46 |
| 1060 | 0.40 | 0.44 | 0.62 | 1.44 |
| 1064 | 0.40 | 0.44 | 0.61 | 1.43 |
| 1068 | 0.40 | 0.43 | 0.61 | 1.42 |

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Hydrograph Discharge Table

| Time (min) | Hyd. 11 + (cfs) | Hyd. 12 + (cfs) | Hyd. 13 = (cfs) | Outflow (cfs) |
|-----------------------|----------------------------|----------------------------|----------------------------|--------------------------|
| 1072 | 0.40 | 0.43 | 0.60 | 1.41 |
| 1076 | 0.40 | 0.42 | 0.59 | 1.39 |
| 1080 | 0.40 | 0.42 | 0.59 | 1.38 |
| 1084 | 0.40 | 0.41 | 0.58 | 1.37 |

...End

Hydrograph Discharge Table

| Time (min) | Hyd. 11 + (cfs) | Hyd. 12 + (cfs) | Hyd. 13 = (cfs) | Outflow (cfs) |
|---------------|--------------------|--------------------|--------------------|------------------|
| 868 | 0.87 | 1.14 | 1.37 | 3.26 |
| 872 | 0.85 | 1.10 | 1.33 | 3.18 |
| 876 | 0.83 | 1.07 | 1.30 | 3.10 |
| 880 | 0.81 | 1.04 | 1.26 | 3.02 |
| 884 | 0.80 | 1.02 | 1.23 | 2.95 |
| 888 | 0.78 | 0.99 | 1.20 | 2.88 |
| 892 | 0.76 | 0.97 | 1.17 | 2.82 |
| 896 | 0.75 | 0.94 | 1.16 | 2.77 |
| 900 | 0.73 | 0.92 | 1.14 | 2.72 |
| 904 | 0.72 | 0.90 | 1.12 | 2.67 |
| 908 | 0.71 | 0.88 | 1.10 | 2.62 |
| 912 | 0.70 | 0.86 | 1.08 | 2.57 |
| 916 | 0.69 | 0.84 | 1.06 | 2.53 |
| 920 | 0.68 | 0.83 | 1.04 | 2.49 |
| 924 | 0.67 | 0.81 | 1.02 | 2.44 |
| 928 | 0.67 | 0.80 | 1.01 | 2.40 |
| 932 | 0.66 | 0.78 | 0.99 | 2.36 |
| 936 | 0.65 | 0.77 | 0.97 | 2.32 |
| 940 | 0.64 | 0.75 | 0.95 | 2.27 |
| 944 | 0.63 | 0.74 | 0.93 | 2.23 |
| 948 | 0.62 | 0.72 | 0.91 | 2.19 |
| 952 | 0.61 | 0.71 | 0.89 | 2.15 |
| 956 | 0.60 | 0.69 | 0.88 | 2.10 |
| 960 | 0.59 | 0.68 | 0.86 | 2.06 |
| 964 | 0.58 | 0.66 | 0.84 | 2.02 |
| 968 | 0.57 | 0.65 | 0.82 | 1.98 |
| 972 | 0.56 | 0.64 | 0.80 | 1.94 |
| 976 | 0.55 | 0.62 | 0.79 | 1.91 |
| 980 | 0.54 | 0.61 | 0.77 | 1.88 |
| 984 | 0.53 | 0.60 | 0.76 | 1.84 |
| 988 | 0.52 | 0.58 | 0.74 | 1.81 |
| 992 | 0.52 | 0.57 | 0.73 | 1.78 |
| 996 | 0.51 | 0.56 | 0.72 | 1.75 |
| 1000 | 0.50 | 0.55 | 0.71 | 1.73 |
| 1004 | 0.49 | 0.54 | 0.71 | 1.71 |
| 1008 | 0.48 | 0.53 | 0.70 | 1.69 |
| 1012 | 0.47 | 0.52 | 0.69 | 1.67 |
| 1016 | 0.47 | 0.51 | 0.69 | 1.65 |
| 1020 | 0.46 | 0.50 | 0.68 | 1.63 |
| 1024 | 0.45 | 0.49 | 0.68 | 1.61 |
| 1028 | 0.45 | 0.48 | 0.67 | 1.59 |
| 1032 | 0.44 | 0.48 | 0.66 | 1.57 |
| 1036 | 0.43 | 0.47 | 0.66 | 1.55 |
| 1040 | 0.42 | 0.47 | 0.65 | 1.53 |
| 1044 | 0.42 | 0.46 | 0.65 | 1.51 |
| 1048 | 0.41 | 0.46 | 0.64 | 1.49 |
| 1052 | 0.40 | 0.45 | 0.63 | 1.47 |
| 1056 | 0.40 | 0.45 | 0.63 | 1.46 |
| 1060 | 0.40 | 0.44 | 0.62 | 1.44 |
| 1064 | 0.40 | 0.44 | 0.61 | 1.43 |
| 1068 | 0.40 | 0.43 | 0.61 | 1.42 |

Continues on next page...

Hydrograph Discharge Table

| Time (min) | Hyd. 11 + (cfs) | Hyd. 12 + (cfs) | Hyd. 13 = (cfs) | Outflow (cfs) |
|-----------------------|----------------------------|----------------------------|----------------------------|--------------------------|
| 1072 | 0.40 | 0.43 | 0.60 | 1.41 |
| 1076 | 0.40 | 0.42 | 0.59 | 1.39 |
| 1080 | 0.40 | 0.42 | 0.59 | 1.38 |
| 1084 | 0.40 | 0.41 | 0.58 | 1.37 |

...End

APPENDIX "D"
EMERGENCY SPILLWAY ROUTING

Hydrograph Return Period Recap

| Hyd. No. | Hydrograph type (origin) | Inflow Hyd(s) | Peak Outflow (cfs) | | | | | | | | Hydrograph description |
|----------|--------------------------|---------------|--------------------|------|------|------|-------|-------|-------|--------|------------------------|
| | | | 1-Yr | 2-Yr | 3-Yr | 5-Yr | 10-Yr | 25-Yr | 50-Yr | 100-Yr | |
| 1 | SCS Runoff | ---- | 2.47 | 3.26 | ---- | ---- | 6.21 | 7.37 | 8.70 | 10.02 | Post Subarea 1a |
| 2 | SCS Runoff | ---- | 0.03 | 0.09 | ---- | ---- | 0.40 | 0.54 | 0.72 | 0.91 | Post Subarea 1b |
| 3 | SCS Runoff | ---- | 3.14 | 4.02 | ---- | ---- | 7.26 | 8.53 | 9.96 | 11.39 | Post Subarea 2a |
| 4 | SCS Runoff | ---- | 0.03 | 0.09 | ---- | ---- | 0.38 | 0.53 | 0.70 | 0.88 | Post Subarea 2b |
| 5 | SCS Runoff | ---- | 4.47 | 5.89 | ---- | ---- | 11.18 | 13.26 | 15.64 | 18.02 | Post Subarea 3a |
| 6 | SCS Runoff | ---- | 0.04 | 0.11 | ---- | ---- | 0.50 | 0.68 | 0.91 | 1.14 | Post Subarea 3b |
| 7 | Combine | 1, 2, | 2.51 | 3.34 | ---- | ---- | 6.52 | 7.79 | 9.25 | 10.71 | Basin 1 In |
| 8 | Combine | 3, 4, | 3.17 | 4.09 | ---- | ---- | 7.51 | 8.86 | 10.39 | 11.93 | Basin 2 In |
| 9 | Combine | 5, 6, | 4.51 | 6.00 | ---- | ---- | 11.65 | 13.90 | 16.49 | 19.08 | Basin 3 In |
| 10 | Reservoir | 7 | 0.00 | 0.00 | ---- | ---- | 0.00 | 0.14 | 0.42 | 0.88 | Basin 1 Out |
| 11 | Reservoir | 8 | 0.00 | 0.00 | ---- | ---- | 0.00 | 0.17 | 0.58 | 1.14 | Basin 2 Out |
| 12 | Reservoir | 9 | 0.00 | 0.00 | ---- | ---- | 0.24 | 0.63 | 1.43 | 5.00 | Basin 3 Out |

Proj. file: freeboard.gpw

Run date: 10-08-2004

Hydrograph Summary Report

| Hyd. No. | Hydrograph type (origin) | Peak flow (cfs) | Time interval (min) | Time to peak (min) | Volume (cuft) | Inflow hyd(s) | Maximum elevation (ft) | Maximum storage (cuft) | Hydrograph description | |
|---------------------------|--------------------------|-----------------|---------------------|-----------------------|---------------|---------------|------------------------|------------------------|------------------------|--|
| 1 | SCS Runoff | 10.02 | 2 | 728 | 39,402 | --- | ---- | ---- | Post Subarea 1a | |
| 2 | SCS Runoff | 0.91 | 2 | 724 | 2,783 | --- | ---- | ---- | Post Subarea 1b | |
| 3 | SCS Runoff | 11.39 | 2 | 730 | 48,324 | --- | ---- | ---- | Post Subarea 2a | |
| 4 | SCS Runoff | 0.88 | 2 | 724 | 2,683 | --- | ---- | ---- | Post Subarea 2b | |
| 5 | SCS Runoff | 18.02 | 2 | 726 | 63,345 | --- | ---- | ---- | Post Subarea 3a | |
| 6 | SCS Runoff | 1.14 | 2 | 724 | 3,478 | --- | ---- | ---- | Post Subarea 3b | |
| 7 | Combine | 10.71 | 2 | 728 | 42,185 | 1, 2, | ---- | ---- | Basin 1 In | |
| 8 | Combine | 11.93 | 2 | 730 | 51,007 | 3, 4, | ---- | ---- | Basin 2 In | |
| 9 | Combine | 19.08 | 2 | 726 | 66,824 | 5, 6, | ---- | ---- | Basin 3 In | |
| 10 | Reservoir | 0.88 | 2 | 822 | 12,797 | 7 | 244.45 | 40,874 | Basin 1 Out | |
| 11 | Reservoir | 1.14 | 2 | 808 | 15,897 | 8 | 236.05 | 35,517 | Basin 2 Out | |
| 12 | Reservoir | 5.00 | 2 | 750 | 27,949 | 9 | 227.05 | 39,256 | Basin 3 Out | |
| Proj. file: freeboard.gpw | | | | Return Period: 100 yr | | | Run date: 10-08-2004 | | | |

Hydrograph Report

Hyd. No. 10

Basin 1 Out

Hydrograph type = Reservoir
 Storm frequency = 100 yrs
 Inflow hyd. No. = 7
 Max. Elevation = 244.45 ft

Peak discharge = 0.88 cfs
 Time interval = 2 min
 Reservoir name = Retention Basin N
 Max. Storage = 40,874 cuft

Storage Indication method used.

Outflow hydrograph volume = 12,797 cuft

Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 804 | 0.99 | 244.43 | ---- | ---- | ---- | ---- | ---- | 0.45 | ---- | ---- | ---- | 0.45 |
| 808 | 0.96 | 244.44 | ---- | ---- | ---- | ---- | ---- | 0.69 | ---- | ---- | ---- | 0.69 |
| 812 | 0.94 | 244.45 | ---- | ---- | ---- | ---- | ---- | 0.80 | ---- | ---- | ---- | 0.80 |
| 816 | 0.92 | 244.45 | ---- | ---- | ---- | ---- | ---- | 0.86 | ---- | ---- | ---- | 0.86 |
| 820 | 0.89 | 244.45 | ---- | ---- | ---- | ---- | ---- | 0.88 | ---- | ---- | ---- | 0.88 |
| 824 | 0.87 | 244.45 | ---- | ---- | ---- | ---- | ---- | 0.88 | ---- | ---- | ---- | 0.88 |
| 828 | 0.85 | 244.45 | ---- | ---- | ---- | ---- | ---- | 0.87 | ---- | ---- | ---- | 0.87 |
| 832 | 0.83 | 244.45 | ---- | ---- | ---- | ---- | ---- | 0.86 | ---- | ---- | ---- | 0.86 |
| 836 | 0.80 | 244.45 | ---- | ---- | ---- | ---- | ---- | 0.84 | ---- | ---- | ---- | 0.84 |
| 840 | 0.78 | 244.45 | ---- | ---- | ---- | ---- | ---- | 0.82 | ---- | ---- | ---- | 0.82 |
| 844 | 0.76 | 244.45 | ---- | ---- | ---- | ---- | ---- | 0.79 | ---- | ---- | ---- | 0.79 |
| 848 | 0.74 | 244.45 | ---- | ---- | ---- | ---- | ---- | 0.77 | ---- | ---- | ---- | 0.77 |
| 852 | 0.72 | 244.45 | ---- | ---- | ---- | ---- | ---- | 0.75 | ---- | ---- | ---- | 0.75 |
| 856 | 0.71 | 244.44 | ---- | ---- | ---- | ---- | ---- | 0.74 | ---- | ---- | ---- | 0.74 |
| 860 | 0.70 | 244.44 | ---- | ---- | ---- | ---- | ---- | 0.72 | ---- | ---- | ---- | 0.72 |
| 864 | 0.69 | 244.44 | ---- | ---- | ---- | ---- | ---- | 0.71 | ---- | ---- | ---- | 0.71 |
| 868 | 0.67 | 244.44 | ---- | ---- | ---- | ---- | ---- | 0.70 | ---- | ---- | ---- | 0.70 |
| 872 | 0.66 | 244.44 | ---- | ---- | ---- | ---- | ---- | 0.68 | ---- | ---- | ---- | 0.68 |
| 876 | 0.65 | 244.44 | ---- | ---- | ---- | ---- | ---- | 0.67 | ---- | ---- | ---- | 0.67 |
| 880 | 0.64 | 244.44 | ---- | ---- | ---- | ---- | ---- | 0.66 | ---- | ---- | ---- | 0.66 |
| 884 | 0.63 | 244.44 | ---- | ---- | ---- | ---- | ---- | 0.65 | ---- | ---- | ---- | 0.65 |
| 888 | 0.62 | 244.44 | ---- | ---- | ---- | ---- | ---- | 0.64 | ---- | ---- | ---- | 0.64 |
| 892 | 0.61 | 244.44 | ---- | ---- | ---- | ---- | ---- | 0.63 | ---- | ---- | ---- | 0.63 |
| 896 | 0.60 | 244.44 | ---- | ---- | ---- | ---- | ---- | 0.62 | ---- | ---- | ---- | 0.62 |
| 900 | 0.59 | 244.44 | ---- | ---- | ---- | ---- | ---- | 0.60 | ---- | ---- | ---- | 0.60 |
| 904 | 0.57 | 244.44 | ---- | ---- | ---- | ---- | ---- | 0.59 | ---- | ---- | ---- | 0.59 |
| 908 | 0.56 | 244.44 | ---- | ---- | ---- | ---- | ---- | 0.58 | ---- | ---- | ---- | 0.58 |
| 912 | 0.55 | 244.43 | ---- | ---- | ---- | ---- | ---- | 0.57 | ---- | ---- | ---- | 0.57 |
| 916 | 0.54 | 244.43 | ---- | ---- | ---- | ---- | ---- | 0.56 | ---- | ---- | ---- | 0.56 |
| 920 | 0.53 | 244.43 | ---- | ---- | ---- | ---- | ---- | 0.55 | ---- | ---- | ---- | 0.55 |
| 924 | 0.52 | 244.43 | ---- | ---- | ---- | ---- | ---- | 0.54 | ---- | ---- | ---- | 0.54 |
| 928 | 0.51 | 244.43 | ---- | ---- | ---- | ---- | ---- | 0.53 | ---- | ---- | ---- | 0.53 |
| 932 | 0.50 | 244.43 | ---- | ---- | ---- | ---- | ---- | 0.51 | ---- | ---- | ---- | 0.51 |
| 936 | 0.48 | 244.43 | ---- | ---- | ---- | ---- | ---- | 0.50 | ---- | ---- | ---- | 0.50 |
| 940 | 0.47 | 244.43 | ---- | ---- | ---- | ---- | ---- | 0.49 | ---- | ---- | ---- | 0.49 |
| 944 | 0.46 | 244.43 | ---- | ---- | ---- | ---- | ---- | 0.48 | ---- | ---- | ---- | 0.48 |
| 948 | 0.45 | 244.43 | ---- | ---- | ---- | ---- | ---- | 0.47 | ---- | ---- | ---- | 0.47 |
| 952 | 0.44 | 244.43 | ---- | ---- | ---- | ---- | ---- | 0.46 | ---- | ---- | ---- | 0.46 |

Continues on next page...

Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 956 | 0.43 | 244.43 | ---- | ---- | ---- | ---- | ---- | 0.45 | ---- | ---- | ---- | 0.45 |
| 960 | 0.42 | 244.43 | ---- | ---- | ---- | ---- | ---- | 0.43 | ---- | ---- | ---- | 0.43 |
| 964 | 0.40 | 244.43 | ---- | ---- | ---- | ---- | ---- | 0.42 | ---- | ---- | ---- | 0.42 |
| 968 | 0.40 | 244.43 | ---- | ---- | ---- | ---- | ---- | 0.41 | ---- | ---- | ---- | 0.41 |
| 972 | 0.39 | 244.42 | ---- | ---- | ---- | ---- | ---- | 0.40 | ---- | ---- | ---- | 0.40 |
| 976 | 0.38 | 244.42 | ---- | ---- | ---- | ---- | ---- | 0.39 | ---- | ---- | ---- | 0.39 |
| 980 | 0.38 | 244.42 | ---- | ---- | ---- | ---- | ---- | 0.39 | ---- | ---- | ---- | 0.39 |
| 984 | 0.37 | 244.42 | ---- | ---- | ---- | ---- | ---- | 0.38 | ---- | ---- | ---- | 0.38 |
| 988 | 0.37 | 244.42 | ---- | ---- | ---- | ---- | ---- | 0.38 | ---- | ---- | ---- | 0.38 |
| 992 | 0.36 | 244.42 | ---- | ---- | ---- | ---- | ---- | 0.37 | ---- | ---- | ---- | 0.37 |
| 996 | 0.36 | 244.42 | ---- | ---- | ---- | ---- | ---- | 0.37 | ---- | ---- | ---- | 0.37 |
| 1000 | 0.35 | 244.42 | ---- | ---- | ---- | ---- | ---- | 0.36 | ---- | ---- | ---- | 0.36 |
| 1004 | 0.35 | 244.42 | ---- | ---- | ---- | ---- | ---- | 0.36 | ---- | ---- | ---- | 0.36 |
| 1008 | 0.34 | 244.42 | ---- | ---- | ---- | ---- | ---- | 0.35 | ---- | ---- | ---- | 0.35 |
| 1012 | 0.34 | 244.42 | ---- | ---- | ---- | ---- | ---- | 0.35 | ---- | ---- | ---- | 0.35 |
| 1016 | 0.33 | 244.42 | ---- | ---- | ---- | ---- | ---- | 0.34 | ---- | ---- | ---- | 0.34 |
| 1020 | 0.33 | 244.42 | ---- | ---- | ---- | ---- | ---- | 0.34 | ---- | ---- | ---- | 0.34 |
| 1024 | 0.32 | 244.42 | ---- | ---- | ---- | ---- | ---- | 0.33 | ---- | ---- | ---- | 0.33 |
| 1028 | 0.32 | 244.42 | ---- | ---- | ---- | ---- | ---- | 0.33 | ---- | ---- | ---- | 0.33 |
| 1032 | 0.31 | 244.42 | ---- | ---- | ---- | ---- | ---- | 0.32 | ---- | ---- | ---- | 0.32 |
| 1036 | 0.31 | 244.42 | ---- | ---- | ---- | ---- | ---- | 0.32 | ---- | ---- | ---- | 0.32 |
| 1040 | 0.30 | 244.42 | ---- | ---- | ---- | ---- | ---- | 0.31 | ---- | ---- | ---- | 0.31 |
| 1044 | 0.30 | 244.42 | ---- | ---- | ---- | ---- | ---- | 0.31 | ---- | ---- | ---- | 0.31 |
| 1048 | 0.29 | 244.42 | ---- | ---- | ---- | ---- | ---- | 0.30 | ---- | ---- | ---- | 0.30 |
| 1052 | 0.29 | 244.42 | ---- | ---- | ---- | ---- | ---- | 0.30 | ---- | ---- | ---- | 0.30 |
| 1056 | 0.28 | 244.42 | ---- | ---- | ---- | ---- | ---- | 0.29 | ---- | ---- | ---- | 0.29 |
| 1060 | 0.28 | 244.42 | ---- | ---- | ---- | ---- | ---- | 0.29 | ---- | ---- | ---- | 0.29 |
| 1064 | 0.27 | 244.42 | ---- | ---- | ---- | ---- | ---- | 0.28 | ---- | ---- | ---- | 0.28 |
| 1068 | 0.27 | 244.42 | ---- | ---- | ---- | ---- | ---- | 0.28 | ---- | ---- | ---- | 0.28 |
| 1072 | 0.26 | 244.42 | ---- | ---- | ---- | ---- | ---- | 0.27 | ---- | ---- | ---- | 0.27 |
| 1076 | 0.26 | 244.42 | ---- | ---- | ---- | ---- | ---- | 0.27 | ---- | ---- | ---- | 0.27 |
| 1080 | 0.25 | 244.42 | ---- | ---- | ---- | ---- | ---- | 0.26 | ---- | ---- | ---- | 0.26 |
| 1084 | 0.25 | 244.42 | ---- | ---- | ---- | ---- | ---- | 0.26 | ---- | ---- | ---- | 0.26 |
| 1088 | 0.24 | 244.42 | ---- | ---- | ---- | ---- | ---- | 0.25 | ---- | ---- | ---- | 0.25 |
| 1092 | 0.24 | 244.42 | ---- | ---- | ---- | ---- | ---- | 0.25 | ---- | ---- | ---- | 0.25 |
| 1096 | 0.24 | 244.41 | ---- | ---- | ---- | ---- | ---- | 0.24 | ---- | ---- | ---- | 0.24 |
| 1100 | 0.24 | 244.41 | ---- | ---- | ---- | ---- | ---- | 0.24 | ---- | ---- | ---- | 0.24 |
| 1104 | 0.24 | 244.41 | ---- | ---- | ---- | ---- | ---- | 0.24 | ---- | ---- | ---- | 0.24 |
| 1108 | 0.23 | 244.41 | ---- | ---- | ---- | ---- | ---- | 0.24 | ---- | ---- | ---- | 0.24 |
| 1112 | 0.23 | 244.41 | ---- | ---- | ---- | ---- | ---- | 0.24 | ---- | ---- | ---- | 0.24 |
| 1116 | 0.23 | 244.41 | ---- | ---- | ---- | ---- | ---- | 0.23 | ---- | ---- | ---- | 0.23 |
| 1120 | 0.23 | 244.41 | ---- | ---- | ---- | ---- | ---- | 0.23 | ---- | ---- | ---- | 0.23 |
| 1124 | 0.23 | 244.41 | ---- | ---- | ---- | ---- | ---- | 0.23 | ---- | ---- | ---- | 0.23 |
| 1128 | 0.23 | 244.41 | ---- | ---- | ---- | ---- | ---- | 0.23 | ---- | ---- | ---- | 0.23 |
| 1132 | 0.23 | 244.41 | ---- | ---- | ---- | ---- | ---- | 0.23 | ---- | ---- | ---- | 0.23 |
| 1136 | 0.22 | 244.41 | ---- | ---- | ---- | ---- | ---- | 0.23 | ---- | ---- | ---- | 0.23 |
| 1140 | 0.22 | 244.41 | ---- | ---- | ---- | ---- | ---- | 0.23 | ---- | ---- | ---- | 0.23 |
| 1144 | 0.22 | 244.41 | ---- | ---- | ---- | ---- | ---- | 0.22 | ---- | ---- | ---- | 0.22 |
| 1148 | 0.22 | 244.41 | ---- | ---- | ---- | ---- | ---- | 0.22 | ---- | ---- | ---- | 0.22 |
| 1152 | 0.22 | 244.41 | ---- | ---- | ---- | ---- | ---- | 0.22 | ---- | ---- | ---- | 0.22 |

...End

Reservoir Report

Reservoir No. 1 - Retention Basin No. 1

Hydraflow Hydrographs by Intelsolve

Pond Data

Pond storage is based on known contour areas. Average end area method used.

Stage / Storage Table

| Stage (ft) | Elevation (ft) | Contour area (sqft) | Incr. Storage (cuft) | Total storage (cuft) |
|------------|----------------|---------------------|----------------------|----------------------|
| 0.00 | 238.00 | 4,449 | 0 | 0 |
| 2.00 | 240.00 | 6,679 | 11,128 | 11,128 |
| 4.00 | 242.00 | 6,679 | 13,358 | 24,486 |
| 6.00 | 244.00 | 6,679 | 13,358 | 37,844 |
| 8.00 | 246.00 | 6,679 | 13,358 | 51,202 |
| 8.50 | 246.50 | 6,679 | 3,340 | 54,542 |

Culvert / Orifice Structures

| | [A] | [B] | [C] | [D] |
|---------------|--------|------|------|------|
| Rise in | = 0.0 | 0.0 | 0.0 | 0.0 |
| Span in | = 0.0 | 0.0 | 0.0 | 0.0 |
| No. Barrels | = 0 | 0 | 0 | 0 |
| Invert El. ft | = 0.00 | 0.00 | 0.00 | 0.00 |
| Length ft | = 0.0 | 0.0 | 0.0 | 0.0 |
| Slope % | = 0.00 | 0.00 | 0.00 | 0.00 |
| N-Value | = .013 | .013 | .000 | .000 |
| Orif. Coeff. | = 0.60 | 0.60 | 0.00 | 0.00 |
| Multi-Stage | = n/a | No | No | No |

Weir Structures

| | [A] | [B] | [C] | [D] |
|--------------|--------|--------|------|------|
| Crest Len ft | = 0.00 | 40.00 | 0.00 | 0.00 |
| Crest El. ft | = 0.00 | 244.50 | 0.00 | 0.00 |
| Weir Coeff. | = 3.33 | 2.60 | 3.33 | 0.00 |
| Weir Type | = --- | Broad | --- | --- |
| Multi-Stage | = No | No | No | No |

Exfiltration Rate = 0.00 in/hr/sqft Tailwater Elev. = 0.00 ft

Stage / Storage / Discharge Table

Note: All outflows have been analyzed under inlet and outlet control.

| Stage ft | Storage cuft | Elevation ft | Civ A cfs | Civ B cfs | Civ C cfs | Civ D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Total cfs |
|----------|--------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-----------|
| 0.00 | 0 | 238.00 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 0.20 | 1,113 | 238.20 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 0.40 | 2,226 | 238.40 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 0.60 | 3,338 | 238.60 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 0.80 | 4,451 | 238.80 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 1.00 | 5,564 | 239.00 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 1.20 | 6,677 | 239.20 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 1.40 | 7,790 | 239.40 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 1.60 | 8,902 | 239.60 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 1.80 | 10,015 | 239.80 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 2.00 | 11,128 | 240.00 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 2.20 | 12,464 | 240.20 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 2.40 | 13,800 | 240.40 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 2.60 | 15,135 | 240.60 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 2.80 | 16,471 | 240.80 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 3.00 | 17,807 | 241.00 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 3.20 | 19,143 | 241.20 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 3.40 | 20,479 | 241.40 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 3.60 | 21,814 | 241.60 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 3.80 | 23,150 | 241.80 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 4.00 | 24,486 | 242.00 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 4.20 | 25,822 | 242.20 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 4.40 | 27,158 | 242.40 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 4.60 | 28,493 | 242.60 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 4.80 | 29,829 | 242.80 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 5.00 | 31,165 | 243.00 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 5.20 | 32,501 | 243.20 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 5.40 | 33,837 | 243.40 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 5.60 | 35,172 | 243.60 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 5.80 | 36,508 | 243.80 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 6.00 | 37,844 | 244.00 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 6.20 | 39,180 | 244.20 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |

Continues on next page...

Stage / Storage / Discharge Table

| Stage ft | Storage cuft | Elevation ft | Civ A cfs | Civ B cfs | Civ C cfs | Civ D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Total cfs |
|-------------|-----------------|-----------------|--------------|--------------|--------------|--------------|-------------|-------------|-------------|-------------|--------------|--------------|
| 6.40 | 40,516 | 244.40 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 6.60 | 41,851 | 244.60 | --- | --- | --- | --- | --- | 3.29 | --- | --- | --- | 3.29 |
| 6.80 | 43,187 | 244.80 | --- | --- | --- | --- | --- | 17.09 | --- | --- | --- | 17.09 |
| 7.00 | 44,523 | 245.00 | --- | --- | --- | --- | --- | 36.77 | --- | --- | --- | 36.77 |
| 7.20 | 45,859 | 245.20 | --- | --- | --- | --- | --- | 60.91 | --- | --- | --- | 60.91 |
| 7.40 | 47,195 | 245.40 | --- | --- | --- | --- | --- | 88.79 | --- | --- | --- | 88.79 |
| 7.60 | 48,530 | 245.60 | --- | --- | --- | --- | --- | 119.98 | --- | --- | --- | 119.98 |
| 7.80 | 49,866 | 245.80 | --- | --- | --- | --- | --- | 154.15 | --- | --- | --- | 154.15 |
| 8.00 | 51,202 | 246.00 | --- | --- | --- | --- | --- | 191.06 | --- | --- | --- | 191.06 |
| 8.05 | 51,536 | 246.05 | --- | --- | --- | --- | --- | 200.69 | --- | --- | --- | 200.69 |
| 8.10 | 51,870 | 246.10 | --- | --- | --- | --- | --- | 210.48 | --- | --- | --- | 210.48 |
| 8.15 | 52,204 | 246.15 | --- | --- | --- | --- | --- | 220.43 | --- | --- | --- | 220.43 |
| 8.20 | 52,538 | 246.20 | --- | --- | --- | --- | --- | 230.52 | --- | --- | --- | 230.52 |
| 8.25 | 52,872 | 246.25 | --- | --- | --- | --- | --- | 240.77 | --- | --- | --- | 240.77 |
| 8.30 | 53,206 | 246.30 | --- | --- | --- | --- | --- | 251.16 | --- | --- | --- | 251.16 |
| 8.35 | 53,540 | 246.35 | --- | --- | --- | --- | --- | 261.70 | --- | --- | --- | 261.70 |
| 8.40 | 53,874 | 246.40 | --- | --- | --- | --- | --- | 272.38 | --- | --- | --- | 272.38 |
| 8.45 | 54,208 | 246.45 | --- | --- | --- | --- | --- | 283.20 | --- | --- | --- | 283.20 |
| 8.50 | 54,542 | 246.50 | --- | --- | --- | --- | --- | 294.16 | --- | --- | --- | 294.16 |

...End

Hydrograph Report

Hyd. No. 11

Basin 2 Out

Hydrograph type = Reservoir
 Storm frequency = 100 yrs
 Inflow hyd. No. = 8
 Max. Elevation = 236.05 ft

Peak discharge = 1.14 cfs
 Time interval = 2 min
 Reservoir name = Detention Basin 2
 Max. Storage = 35,517 cuft

Storage Indication method used.

Outflow hydrograph volume = 15,897 cuft

Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 792 | 1.27 | 236.03 | ---- | ---- | ---- | ---- | ---- | 0.70 | ---- | ---- | ---- | 0.70 |
| 796 | 1.22 | 236.04 | ---- | ---- | ---- | ---- | ---- | 0.97 | ---- | ---- | ---- | 0.97 |
| 800 | 1.19 | 236.05 | ---- | ---- | ---- | ---- | ---- | 1.08 | ---- | ---- | ---- | 1.08 |
| 804 | 1.16 | 236.05 | ---- | ---- | ---- | ---- | ---- | 1.13 | ---- | ---- | ---- | 1.13 |
| 808 | 1.13 | 236.05 << | ---- | ---- | ---- | ---- | ---- | 1.14 | ---- | ---- | ---- | 1.14 << |
| 812 | 1.11 | 236.05 | ---- | ---- | ---- | ---- | ---- | 1.13 | ---- | ---- | ---- | 1.13 |
| 816 | 1.08 | 236.05 | ---- | ---- | ---- | ---- | ---- | 1.11 | ---- | ---- | ---- | 1.11 |
| 820 | 1.05 | 236.05 | ---- | ---- | ---- | ---- | ---- | 1.09 | ---- | ---- | ---- | 1.09 |
| 824 | 1.03 | 236.05 | ---- | ---- | ---- | ---- | ---- | 1.06 | ---- | ---- | ---- | 1.06 |
| 828 | 1.00 | 236.04 | ---- | ---- | ---- | ---- | ---- | 1.04 | ---- | ---- | ---- | 1.04 |
| 832 | 0.97 | 236.04 | ---- | ---- | ---- | ---- | ---- | 1.01 | ---- | ---- | ---- | 1.01 |
| 836 | 0.94 | 236.04 | ---- | ---- | ---- | ---- | ---- | 0.98 | ---- | ---- | ---- | 0.98 |
| 840 | 0.92 | 236.04 | ---- | ---- | ---- | ---- | ---- | 0.96 | ---- | ---- | ---- | 0.96 |
| 844 | 0.89 | 236.04 | ---- | ---- | ---- | ---- | ---- | 0.93 | ---- | ---- | ---- | 0.93 |
| 848 | 0.87 | 236.04 | ---- | ---- | ---- | ---- | ---- | 0.90 | ---- | ---- | ---- | 0.90 |
| 852 | 0.85 | 236.04 | ---- | ---- | ---- | ---- | ---- | 0.88 | ---- | ---- | ---- | 0.88 |
| 856 | 0.83 | 236.04 | ---- | ---- | ---- | ---- | ---- | 0.86 | ---- | ---- | ---- | 0.86 |
| 860 | 0.82 | 236.04 | ---- | ---- | ---- | ---- | ---- | 0.84 | ---- | ---- | ---- | 0.84 |
| 864 | 0.80 | 236.04 | ---- | ---- | ---- | ---- | ---- | 0.82 | ---- | ---- | ---- | 0.82 |
| 868 | 0.79 | 236.03 | ---- | ---- | ---- | ---- | ---- | 0.81 | ---- | ---- | ---- | 0.81 |
| 872 | 0.78 | 236.03 | ---- | ---- | ---- | ---- | ---- | 0.80 | ---- | ---- | ---- | 0.80 |
| 876 | 0.76 | 236.03 | ---- | ---- | ---- | ---- | ---- | 0.78 | ---- | ---- | ---- | 0.78 |
| 880 | 0.75 | 236.03 | ---- | ---- | ---- | ---- | ---- | 0.77 | ---- | ---- | ---- | 0.77 |
| 884 | 0.74 | 236.03 | ---- | ---- | ---- | ---- | ---- | 0.76 | ---- | ---- | ---- | 0.76 |
| 888 | 0.72 | 236.03 | ---- | ---- | ---- | ---- | ---- | 0.74 | ---- | ---- | ---- | 0.74 |
| 892 | 0.71 | 236.03 | ---- | ---- | ---- | ---- | ---- | 0.73 | ---- | ---- | ---- | 0.73 |
| 896 | 0.70 | 236.03 | ---- | ---- | ---- | ---- | ---- | 0.72 | ---- | ---- | ---- | 0.72 |
| 900 | 0.68 | 236.03 | ---- | ---- | ---- | ---- | ---- | 0.70 | ---- | ---- | ---- | 0.70 |
| 904 | 0.67 | 236.03 | ---- | ---- | ---- | ---- | ---- | 0.69 | ---- | ---- | ---- | 0.69 |
| 908 | 0.66 | 236.03 | ---- | ---- | ---- | ---- | ---- | 0.68 | ---- | ---- | ---- | 0.68 |
| 912 | 0.65 | 236.03 | ---- | ---- | ---- | ---- | ---- | 0.66 | ---- | ---- | ---- | 0.67 |
| 916 | 0.63 | 236.03 | ---- | ---- | ---- | ---- | ---- | 0.65 | ---- | ---- | ---- | 0.65 |
| 920 | 0.62 | 236.03 | ---- | ---- | ---- | ---- | ---- | 0.64 | ---- | ---- | ---- | 0.64 |
| 924 | 0.61 | 236.03 | ---- | ---- | ---- | ---- | ---- | 0.63 | ---- | ---- | ---- | 0.63 |
| 928 | 0.59 | 236.03 | ---- | ---- | ---- | ---- | ---- | 0.61 | ---- | ---- | ---- | 0.61 |
| 932 | 0.58 | 236.03 | ---- | ---- | ---- | ---- | ---- | 0.60 | ---- | ---- | ---- | 0.60 |
| 936 | 0.57 | 236.03 | ---- | ---- | ---- | ---- | ---- | 0.59 | ---- | ---- | ---- | 0.59 |
| 940 | 0.55 | 236.02 | ---- | ---- | ---- | ---- | ---- | 0.57 | ---- | ---- | ---- | 0.57 |

Continues on next page...

Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 944 | 0.54 | 236.02 | ---- | ---- | ---- | ---- | ---- | 0.56 | ---- | ---- | ---- | 0.56 |
| 948 | 0.53 | 236.02 | ---- | ---- | ---- | ---- | ---- | 0.55 | ---- | ---- | ---- | 0.55 |
| 952 | 0.51 | 236.02 | ---- | ---- | ---- | ---- | ---- | 0.53 | ---- | ---- | ---- | 0.53 |
| 956 | 0.50 | 236.02 | ---- | ---- | ---- | ---- | ---- | 0.52 | ---- | ---- | ---- | 0.52 |
| 960 | 0.49 | 236.02 | ---- | ---- | ---- | ---- | ---- | 0.51 | ---- | ---- | ---- | 0.51 |
| 964 | 0.47 | 236.02 | ---- | ---- | ---- | ---- | ---- | 0.49 | ---- | ---- | ---- | 0.49 |
| 968 | 0.46 | 236.02 | ---- | ---- | ---- | ---- | ---- | 0.48 | ---- | ---- | ---- | 0.48 |
| 972 | 0.45 | 236.02 | ---- | ---- | ---- | ---- | ---- | 0.47 | ---- | ---- | ---- | 0.47 |
| 976 | 0.45 | 236.02 | ---- | ---- | ---- | ---- | ---- | 0.46 | ---- | ---- | ---- | 0.46 |
| 980 | 0.44 | 236.02 | ---- | ---- | ---- | ---- | ---- | 0.45 | ---- | ---- | ---- | 0.45 |
| 984 | 0.43 | 236.02 | ---- | ---- | ---- | ---- | ---- | 0.44 | ---- | ---- | ---- | 0.44 |
| 988 | 0.43 | 236.02 | ---- | ---- | ---- | ---- | ---- | 0.44 | ---- | ---- | ---- | 0.44 |
| 992 | 0.42 | 236.02 | ---- | ---- | ---- | ---- | ---- | 0.43 | ---- | ---- | ---- | 0.43 |
| 996 | 0.42 | 236.02 | ---- | ---- | ---- | ---- | ---- | 0.42 | ---- | ---- | ---- | 0.42 |
| 1000 | 0.41 | 236.02 | ---- | ---- | ---- | ---- | ---- | 0.42 | ---- | ---- | ---- | 0.42 |
| 1004 | 0.40 | 236.02 | ---- | ---- | ---- | ---- | ---- | 0.41 | ---- | ---- | ---- | 0.41 |
| 1008 | 0.40 | 236.02 | ---- | ---- | ---- | ---- | ---- | 0.41 | ---- | ---- | ---- | 0.41 |
| 1012 | 0.39 | 236.02 | ---- | ---- | ---- | ---- | ---- | 0.40 | ---- | ---- | ---- | 0.40 |
| 1016 | 0.39 | 236.02 | ---- | ---- | ---- | ---- | ---- | 0.40 | ---- | ---- | ---- | 0.40 |
| 1020 | 0.38 | 236.02 | ---- | ---- | ---- | ---- | ---- | 0.39 | ---- | ---- | ---- | 0.39 |
| 1024 | 0.38 | 236.02 | ---- | ---- | ---- | ---- | ---- | 0.38 | ---- | ---- | ---- | 0.38 |
| 1028 | 0.37 | 236.02 | ---- | ---- | ---- | ---- | ---- | 0.38 | ---- | ---- | ---- | 0.38 |
| 1032 | 0.36 | 236.02 | ---- | ---- | ---- | ---- | ---- | 0.37 | ---- | ---- | ---- | 0.37 |
| 1036 | 0.36 | 236.02 | ---- | ---- | ---- | ---- | ---- | 0.37 | ---- | ---- | ---- | 0.37 |
| 1040 | 0.35 | 236.02 | ---- | ---- | ---- | ---- | ---- | 0.36 | ---- | ---- | ---- | 0.36 |
| 1044 | 0.35 | 236.02 | ---- | ---- | ---- | ---- | ---- | 0.36 | ---- | ---- | ---- | 0.36 |
| 1048 | 0.34 | 236.02 | ---- | ---- | ---- | ---- | ---- | 0.35 | ---- | ---- | ---- | 0.35 |
| 1052 | 0.34 | 236.01 | ---- | ---- | ---- | ---- | ---- | 0.34 | ---- | ---- | ---- | 0.34 |
| 1056 | 0.33 | 236.01 | ---- | ---- | ---- | ---- | ---- | 0.34 | ---- | ---- | ---- | 0.34 |
| 1060 | 0.32 | 236.01 | ---- | ---- | ---- | ---- | ---- | 0.33 | ---- | ---- | ---- | 0.33 |
| 1064 | 0.32 | 236.01 | ---- | ---- | ---- | ---- | ---- | 0.33 | ---- | ---- | ---- | 0.33 |
| 1068 | 0.31 | 236.01 | ---- | ---- | ---- | ---- | ---- | 0.32 | ---- | ---- | ---- | 0.32 |
| 1072 | 0.31 | 236.01 | ---- | ---- | ---- | ---- | ---- | 0.31 | ---- | ---- | ---- | 0.31 |
| 1076 | 0.30 | 236.01 | ---- | ---- | ---- | ---- | ---- | 0.31 | ---- | ---- | ---- | 0.31 |
| 1080 | 0.29 | 236.01 | ---- | ---- | ---- | ---- | ---- | 0.30 | ---- | ---- | ---- | 0.30 |
| 1084 | 0.29 | 236.01 | ---- | ---- | ---- | ---- | ---- | 0.30 | ---- | ---- | ---- | 0.30 |
| 1088 | 0.28 | 236.01 | ---- | ---- | ---- | ---- | ---- | 0.29 | ---- | ---- | ---- | 0.29 |
| 1092 | 0.28 | 236.01 | ---- | ---- | ---- | ---- | ---- | 0.29 | ---- | ---- | ---- | 0.29 |

...End

Reservoir Report

Reservoir No. 2 - Detention Basin 2

Hydraflow Hydrographs by Intellisolve

Pond Data

Pond storage is based on known contour areas. Average end area method used.

Stage / Storage Table

| Stage (ft) | Elevation (ft) | Contour area (sqft) | Incr. Storage (cuft) | Total storage (cuft) |
|------------|----------------|---------------------|----------------------|----------------------|
| 0.00 | 229.33 | 00 | 0 | 0 |
| 0.67 | 230.00 | 2,454 | 822 | 822 |
| 2.67 | 232.00 | 5,689 | 8,143 | 8,965 |
| 4.67 | 234.00 | 6,522 | 12,211 | 21,176 |
| 6.67 | 236.00 | 7,413 | 13,935 | 35,111 |
| 8.67 | 238.00 | 9,192 | 16,605 | 51,716 |

Culvert / Orifice Structures

| | [A] | [B] | [C] | [D] |
|---------------|--------|------|------|------|
| Rise in | = 0.0 | 0.0 | 0.0 | 0.0 |
| Span in | = 0.0 | 0.0 | 0.0 | 0.0 |
| No. Barrels | = 0 | 0 | 0 | 0 |
| Invert El. ft | = 0.00 | 0.00 | 0.00 | 0.00 |
| Length ft | = 0.0 | 0.0 | 0.0 | 0.0 |
| Slope % | = 0.00 | 0.00 | 0.00 | 0.00 |
| N-Value | = .013 | .013 | .000 | .000 |
| Orif. Coeff. | = 0.60 | 0.60 | 0.00 | 0.00 |
| Multi-Stage | = n/a | No | No | No |

Weir Structures

| | [A] | [B] | [C] | [D] |
|--------------|--------|--------|------|------|
| Crest Len ft | = 0.00 | 20.00 | 0.00 | 0.00 |
| Crest El. ft | = 0.00 | 236.00 | 0.00 | 0.00 |
| Weir Coeff. | = 3.33 | 2.60 | 3.33 | 0.00 |
| Weir Type | = --- | Broad | --- | --- |
| Multi-Stage | = No | No | No | No |

Exfiltration Rate = 0.00 in/hr/sqft Tailwater Elev. = 0.00 ft

Note: All outflows have been analyzed under inlet and outlet control.

Stage / Storage / Discharge Table

| Stage ft | Storage cuft | Elevation ft | Civ A cfs | Civ B cfs | Civ C cfs | Civ D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Total cfs |
|----------|--------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-----------|
| 0.00 | 0 | 229.33 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 0.07 | 82 | 229.40 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 0.13 | 164 | 229.46 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 0.20 | 247 | 229.53 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 0.27 | 329 | 229.60 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 0.34 | 411 | 229.67 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 0.40 | 493 | 229.73 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 0.47 | 575 | 229.80 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 0.54 | 658 | 229.87 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 0.60 | 740 | 229.93 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 0.67 | 822 | 230.00 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 0.87 | 1,636 | 230.20 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 1.07 | 2,451 | 230.40 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 1.27 | 3,265 | 230.60 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 1.47 | 4,079 | 230.80 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 1.67 | 4,894 | 231.00 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 1.87 | 5,708 | 231.20 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 2.07 | 6,522 | 231.40 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 2.27 | 7,336 | 231.60 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 2.47 | 8,151 | 231.80 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 2.67 | 8,965 | 232.00 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 2.87 | 10,186 | 232.20 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 3.07 | 11,407 | 232.40 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 3.27 | 12,628 | 232.60 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 3.47 | 13,849 | 232.80 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 3.67 | 15,071 | 233.00 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 3.87 | 16,292 | 233.20 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 4.07 | 17,513 | 233.40 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 4.27 | 18,734 | 233.60 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 4.47 | 19,955 | 233.80 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 4.67 | 21,176 | 234.00 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 4.87 | 22,570 | 234.20 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |

Continues on next page...

Stage / Storage / Discharge Table

| Stage ft | Storage cuft | Elevation ft | Civ A cfs | Civ B cfs | Civ C cfs | Civ D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Total cfs |
|-------------|-----------------|-----------------|--------------|--------------|--------------|--------------|-------------|-------------|-------------|-------------|--------------|--------------|
| 5.07 | 23,963 | 234.40 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 5.27 | 25,357 | 234.60 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 5.47 | 26,750 | 234.80 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 5.67 | 28,144 | 235.00 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 5.87 | 29,537 | 235.20 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 6.07 | 30,931 | 235.40 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 6.27 | 32,324 | 235.60 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 6.47 | 33,718 | 235.80 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 6.67 | 35,111 | 236.00 | --- | --- | --- | --- | --- | 0.00 | --- | --- | --- | 0.00 |
| 6.87 | 36,772 | 236.20 | --- | --- | --- | --- | --- | 4.65 | --- | --- | --- | 4.65 |
| 7.07 | 38,432 | 236.40 | --- | --- | --- | --- | --- | 13.15 | --- | --- | --- | 13.15 |
| 7.27 | 40,093 | 236.60 | --- | --- | --- | --- | --- | 24.17 | --- | --- | --- | 24.17 |
| 7.47 | 41,753 | 236.80 | --- | --- | --- | --- | --- | 37.21 | --- | --- | --- | 37.21 |
| 7.67 | 43,414 | 237.00 | --- | --- | --- | --- | --- | 52.00 | --- | --- | --- | 52.00 |
| 7.87 | 45,074 | 237.20 | --- | --- | --- | --- | --- | 68.35 | --- | --- | --- | 68.35 |
| 8.07 | 46,735 | 237.40 | --- | --- | --- | --- | --- | 86.14 | --- | --- | --- | 86.14 |
| 8.27 | 48,395 | 237.60 | --- | --- | --- | --- | --- | 105.24 | --- | --- | --- | 105.24 |
| 8.47 | 50,056 | 237.80 | --- | --- | --- | --- | --- | 125.57 | --- | --- | --- | 125.57 |
| 8.67 | 51,716 | 238.00 | --- | --- | --- | --- | --- | 147.08 | --- | --- | --- | 147.08 |

...End

Hydrograph Report

Hyd. No. 12

Basin 3 Out

Hydrograph type = Reservoir
Storm frequency = 100 yrs
Inflow hyd. No. = 9
Max. Elevation = 227.05 ft

Peak discharge = 5.00 cfs
Time interval = 2 min
Reservoir name = Basin 3 (Hotel)
Max. Storage = 39,256 cuft

Storage Indication method used.

Outflow hydrograph volume = 27,949 cuft

Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 748 | 5.45 | 227.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 4.09 | ---- | 4.09 |
| 752 | 4.15 | 227.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 4.53 | ---- | 4.53 |
| 756 | 3.16 | 227.03 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 3.45 | ---- | 3.45 |
| 760 | 2.67 | 227.03 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 2.81 | ---- | 2.81 |
| 764 | 2.47 | 227.02 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 2.52 | ---- | 2.52 |
| 768 | 2.33 | 227.02 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 2.37 | ---- | 2.37 |
| 772 | 2.19 | 227.02 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 2.23 | ---- | 2.23 |
| 776 | 2.05 | 227.02 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 2.09 | ---- | 2.09 |
| 780 | 1.91 | 227.02 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 1.95 | ---- | 1.95 |
| 784 | 1.78 | 227.02 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 1.82 | ---- | 1.82 |
| 788 | 1.69 | 227.02 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 1.72 | ---- | 1.72 |
| 792 | 1.64 | 227.02 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 1.66 | ---- | 1.66 |
| 796 | 1.61 | 227.02 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 1.62 | ---- | 1.62 |
| 800 | 1.57 | 227.02 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 1.58 | ---- | 1.58 |
| 804 | 1.53 | 227.01 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 1.55 | ---- | 1.55 |
| 808 | 1.50 | 227.01 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 1.51 | ---- | 1.51 |
| 812 | 1.46 | 227.01 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 1.47 | ---- | 1.47 |
| 816 | 1.43 | 227.01 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 1.44 | ---- | 1.44 |
| 820 | 1.39 | 227.01 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 1.40 | ---- | 1.40 |
| 824 | 1.35 | 227.01 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 1.36 | ---- | 1.36 |
| 828 | 1.32 | 227.01 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 1.33 | ---- | 1.33 |
| 832 | 1.28 | 227.01 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 1.29 | ---- | 1.29 |
| 836 | 1.24 | 227.01 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 1.25 | ---- | 1.25 |

...End

Reservoir Report

Reservoir No. 3 - Basin 3 (Hotel)

Hydraflow Hydrographs by Intellisolve

Pond Data

Pond storage is based on known contour areas. Average end area method used.

Stage / Storage Table

| Stage (ft) | Elevation (ft) | Contour area (sqft) | Incr. Storage (cuft) | Total storage (cuft) |
|------------|----------------|---------------------|----------------------|----------------------|
| 0.00 | 219.00 | 00 | 0 | 0 |
| 1.00 | 220.00 | 1,406 | 703 | 703 |
| 3.00 | 222.00 | 4,776 | 6,182 | 6,885 |
| 5.00 | 224.00 | 5,971 | 10,747 | 17,632 |
| 7.00 | 226.00 | 7,278 | 13,249 | 30,881 |
| 9.00 | 228.00 | 8,709 | 15,987 | 46,868 |
| 9.50 | 228.50 | 9,086 | 4,449 | 51,317 |

Culvert / Orifice Structures

| | [A] | [B] | [C] | [D] |
|---------------|--------|------|------|------|
| Rise in | = 0.0 | 0.0 | 0.0 | 0.0 |
| Span in | = 0.0 | 0.0 | 0.0 | 0.0 |
| No. Barrels | = 0 | 0 | 0 | 0 |
| Invert El. ft | = 0.00 | 0.00 | 0.00 | 0.00 |
| Length ft | = 0.0 | 0.0 | 0.0 | 0.0 |
| Slope % | = 0.00 | 0.00 | 0.00 | 0.00 |
| N-Value | = .013 | .013 | .013 | .000 |
| Orif. Coeff. | = 0.60 | 0.60 | 0.60 | 0.00 |
| Multi-Stage | = n/a | No | No | No |

Weir Structures

| | [A] | [B] | [C] | [D] |
|--------------|--------|------|------|--------|
| Crest Len ft | = 0.00 | 0.00 | 0.00 | 90.00 |
| Crest El. ft | = 0.00 | 0.00 | 0.00 | 227.00 |
| Weir Coeff. | = 3.33 | 3.33 | 3.33 | 2.60 |
| Weir Type | = --- | --- | --- | Broad |
| Multi-Stage | = No | No | No | No |

Exfiltration Rate = 0.00 in/hr/sqft Tailwater Elev. = 0.00 ft

Stage / Storage / Discharge Table

Note: All outflows have been analyzed under inlet and outlet control.

| Stage ft | Storage cuft | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Total cfs |
|----------|--------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-----------|
| 0.00 | 0 | 219.00 | --- | --- | --- | --- | --- | --- | --- | 0.00 | --- | 0.00 |
| 0.10 | 70 | 219.10 | --- | --- | --- | --- | --- | --- | --- | 0.00 | --- | 0.00 |
| 0.20 | 141 | 219.20 | --- | --- | --- | --- | --- | --- | --- | 0.00 | --- | 0.00 |
| 0.30 | 211 | 219.30 | --- | --- | --- | --- | --- | --- | --- | 0.00 | --- | 0.00 |
| 0.40 | 281 | 219.40 | --- | --- | --- | --- | --- | --- | --- | 0.00 | --- | 0.00 |
| 0.50 | 352 | 219.50 | --- | --- | --- | --- | --- | --- | --- | 0.00 | --- | 0.00 |
| 0.60 | 422 | 219.60 | --- | --- | --- | --- | --- | --- | --- | 0.00 | --- | 0.00 |
| 0.70 | 492 | 219.70 | --- | --- | --- | --- | --- | --- | --- | 0.00 | --- | 0.00 |
| 0.80 | 562 | 219.80 | --- | --- | --- | --- | --- | --- | --- | 0.00 | --- | 0.00 |
| 0.90 | 633 | 219.90 | --- | --- | --- | --- | --- | --- | --- | 0.00 | --- | 0.00 |
| 1.00 | 703 | 220.00 | --- | --- | --- | --- | --- | --- | --- | 0.00 | --- | 0.00 |
| 1.20 | 1,321 | 220.20 | --- | --- | --- | --- | --- | --- | --- | 0.00 | --- | 0.00 |
| 1.40 | 1,939 | 220.40 | --- | --- | --- | --- | --- | --- | --- | 0.00 | --- | 0.00 |
| 1.60 | 2,558 | 220.60 | --- | --- | --- | --- | --- | --- | --- | 0.00 | --- | 0.00 |
| 1.80 | 3,176 | 220.80 | --- | --- | --- | --- | --- | --- | --- | 0.00 | --- | 0.00 |
| 2.00 | 3,794 | 221.00 | --- | --- | --- | --- | --- | --- | --- | 0.00 | --- | 0.00 |
| 2.20 | 4,412 | 221.20 | --- | --- | --- | --- | --- | --- | --- | 0.00 | --- | 0.00 |
| 2.40 | 5,030 | 221.40 | --- | --- | --- | --- | --- | --- | --- | 0.00 | --- | 0.00 |
| 2.60 | 5,649 | 221.60 | --- | --- | --- | --- | --- | --- | --- | 0.00 | --- | 0.00 |
| 2.80 | 6,267 | 221.80 | --- | --- | --- | --- | --- | --- | --- | 0.00 | --- | 0.00 |
| 3.00 | 6,885 | 222.00 | --- | --- | --- | --- | --- | --- | --- | 0.00 | --- | 0.00 |
| 3.20 | 7,960 | 222.20 | --- | --- | --- | --- | --- | --- | --- | 0.00 | --- | 0.00 |
| 3.40 | 9,034 | 222.40 | --- | --- | --- | --- | --- | --- | --- | 0.00 | --- | 0.00 |
| 3.60 | 10,109 | 222.60 | --- | --- | --- | --- | --- | --- | --- | 0.00 | --- | 0.00 |
| 3.80 | 11,184 | 222.80 | --- | --- | --- | --- | --- | --- | --- | 0.00 | --- | 0.00 |
| 4.00 | 12,259 | 223.00 | --- | --- | --- | --- | --- | --- | --- | 0.00 | --- | 0.00 |
| 4.20 | 13,333 | 223.20 | --- | --- | --- | --- | --- | --- | --- | 0.00 | --- | 0.00 |
| 4.40 | 14,408 | 223.40 | --- | --- | --- | --- | --- | --- | --- | 0.00 | --- | 0.00 |
| 4.60 | 15,483 | 223.60 | --- | --- | --- | --- | --- | --- | --- | 0.00 | --- | 0.00 |
| 4.80 | 16,557 | 223.80 | --- | --- | --- | --- | --- | --- | --- | 0.00 | --- | 0.00 |
| 5.00 | 17,632 | 224.00 | --- | --- | --- | --- | --- | --- | --- | 0.00 | --- | 0.00 |

Continues on next page...

Stage / Storage / Discharge Table

| Stage ft | Storage cuft | Elevation ft | Civ A cfs | Civ B cfs | Civ C cfs | Civ D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Total cfs |
|-------------|-----------------|-----------------|--------------|--------------|--------------|--------------|-------------|-------------|-------------|-------------|--------------|--------------|
| 5.20 | 18,957 | 224.20 | --- | --- | --- | --- | --- | --- | --- | 0.00 | --- | 0.00 |
| 5.40 | 20,282 | 224.40 | --- | --- | --- | --- | --- | --- | --- | 0.00 | --- | 0.00 |
| 5.60 | 21,607 | 224.60 | --- | --- | --- | --- | --- | --- | --- | 0.00 | --- | 0.00 |
| 5.80 | 22,932 | 224.80 | --- | --- | --- | --- | --- | --- | --- | 0.00 | --- | 0.00 |
| 6.00 | 24,257 | 225.00 | --- | --- | --- | --- | --- | --- | --- | 0.00 | --- | 0.00 |
| 6.20 | 25,581 | 225.20 | --- | --- | --- | --- | --- | --- | --- | 0.00 | --- | 0.00 |
| 6.40 | 26,906 | 225.40 | --- | --- | --- | --- | --- | --- | --- | 0.00 | --- | 0.00 |
| 6.60 | 28,231 | 225.60 | --- | --- | --- | --- | --- | --- | --- | 0.00 | --- | 0.00 |
| 6.80 | 29,556 | 225.80 | --- | --- | --- | --- | --- | --- | --- | 0.00 | --- | 0.00 |
| 7.00 | 30,881 | 226.00 | --- | --- | --- | --- | --- | --- | --- | 0.00 | --- | 0.00 |
| 7.20 | 32,480 | 226.20 | --- | --- | --- | --- | --- | --- | --- | 0.00 | --- | 0.00 |
| 7.40 | 34,078 | 226.40 | --- | --- | --- | --- | --- | --- | --- | 0.00 | --- | 0.00 |
| 7.60 | 35,677 | 226.60 | --- | --- | --- | --- | --- | --- | --- | 0.00 | --- | 0.00 |
| 7.80 | 37,276 | 226.80 | --- | --- | --- | --- | --- | --- | --- | 0.00 | --- | 0.00 |
| 8.00 | 38,875 | 227.00 | --- | --- | --- | --- | --- | --- | --- | 0.00 | --- | 0.00 |
| 8.20 | 40,473 | 227.20 | --- | --- | --- | --- | --- | --- | --- | 20.93 | --- | 20.93 |
| 8.40 | 42,072 | 227.40 | --- | --- | --- | --- | --- | --- | --- | 59.19 | --- | 59.19 |
| 8.60 | 43,671 | 227.60 | --- | --- | --- | --- | --- | --- | --- | 108.75 | --- | 108.75 |
| 8.80 | 45,269 | 227.80 | --- | --- | --- | --- | --- | --- | --- | 167.43 | --- | 167.43 |
| 9.00 | 46,868 | 228.00 | --- | --- | --- | --- | --- | --- | --- | 234.00 | --- | 234.00 |
| 9.05 | 47,313 | 228.05 | --- | --- | --- | --- | --- | --- | --- | 251.77 | --- | 251.77 |
| 9.10 | 47,758 | 228.10 | --- | --- | --- | --- | --- | --- | --- | 269.97 | --- | 269.97 |
| 9.15 | 48,203 | 228.15 | --- | --- | --- | --- | --- | --- | --- | 288.58 | --- | 288.58 |
| 9.20 | 48,648 | 228.20 | --- | --- | --- | --- | --- | --- | --- | 307.61 | --- | 307.61 |
| 9.25 | 49,092 | 228.25 | --- | --- | --- | --- | --- | --- | --- | 327.03 | --- | 327.03 |
| 9.30 | 49,537 | 228.30 | --- | --- | --- | --- | --- | --- | --- | 346.85 | --- | 346.85 |
| 9.35 | 49,982 | 228.35 | --- | --- | --- | --- | --- | --- | --- | 367.05 | --- | 367.05 |
| 9.40 | 50,427 | 228.40 | --- | --- | --- | --- | --- | --- | --- | 387.63 | --- | 387.63 |
| 9.45 | 50,872 | 228.45 | --- | --- | --- | --- | --- | --- | --- | 408.58 | --- | 408.58 |
| 9.50 | 51,317 | 228.50 | --- | --- | --- | --- | --- | --- | --- | 429.89 | --- | 429.89 |

...End

APPENDIX "E"
WATER QUALITY COMPUTATIONS

Water Quality Calculations

Water quality criteria as found in NJAC 7:8 for residential sites, requires detention of 90% of the rainfall volume from 1¼" of rainfall over a 2-hour period or a 1-year, 24-hour Type III frequency rainfall for 18-hours. Retention basins are required to have a permanent water pool equal to between 1 and 3 times the runoff volume generated from the design storm.

Hydrograph Return Period Recap

| Hyd. No. | Hydrograph type (origin) | Inflow Hyd(s) | Peak Outflow (cfs) | | | | | | | | Hydrograph description |
|----------|--------------------------|---------------|--------------------|------|-------|------|-------|-------|-------|--------|------------------------|
| | | | 1-Yr | 2-Yr | 3-Yr | 5-Yr | 10-Yr | 25-Yr | 50-Yr | 100-Yr | |
| 1 | SCS Runoff | --- | 0.95 | 2.12 | ----- | 5.56 | 8.97 | 12.27 | 16.30 | 20.55 | Predevelopment |
| 2 | SCS Runoff | ----- | 2.47 | 3.26 | ----- | 4.89 | 6.21 | 7.37 | 8.70 | 10.02 | Post Subarea 1a |
| 3 | SCS Runoff | ----- | 0.03 | 0.09 | --- | 0.24 | 0.40 | 0.54 | 0.72 | 0.91 | Post Subarea 1b |
| 4 | SCS Runoff | ----- | 3.14 | 4.02 | ----- | 5.82 | 7.26 | 8.53 | 9.96 | 11.39 | Post Subarea 2a |
| 5 | SCS Runoff | ----- | 0.03 | 0.09 | --- | 0.24 | 0.38 | 0.53 | 0.70 | 0.88 | Post Subarea 2b |
| 6 | SCS Runoff | ----- | 4.47 | 5.89 | --- | 8.81 | 11.18 | 13.26 | 15.64 | 18.02 | Post Subarea 3a |
| 7 | SCS Runoff | ----- | 0.04 | 0.11 | ----- | 0.31 | 0.50 | 0.68 | 0.91 | 1.14 | Post Subarea 3b |
| 8 | Combine | 2, 3, | 2.51 | 3.34 | ----- | 5.09 | 6.52 | 7.79 | 9.25 | 10.71 | Basin 1 In |
| 9 | Combine | 4, 5, | 3.17 | 4.09 | ----- | 5.98 | 7.51 | 8.86 | 10.39 | 11.93 | Basin 2 In |
| 10 | Combine | 6, 7, | 4.51 | 6.00 | ----- | 9.11 | 11.65 | 13.90 | 16.49 | 19.08 | Basin 3 In |
| 11 | Reservoir | 8 | 0.19 | 0.23 | ----- | 0.30 | 0.35 | 0.39 | 0.76 | 1.50 | Basin 1 Out |
| 12 | Reservoir | 9 | 0.22 | 0.40 | --- | 1.39 | 2.53 | 3.63 | 4.95 | 6.27 | Basin 2 Out |
| 13 | Reservoir | 10 | 0.41 | 0.45 | ----- | 0.52 | 1.15 | 2.45 | 3.80 | 5.59 | Basin 3 Out |
| 14 | Combine | 11, 12, 13 | 0.82 | 1.10 | ----- | 2.47 | 4.21 | 7.01 | 9.95 | 13.56 | |

Hydrograph Summary Report

| Hyd. No. | Hydrograph type (origin) | Peak flow (cfs) | Time interval (min) | Time to peak (min) | Volume (cuft) | Inflow hyd(s) | Maximum elevation (ft) | Maximum storage (cuft) | Hydrograph description |
|----------|--------------------------|-----------------|---------------------|--------------------|---------------|---------------|------------------------|------------------------|------------------------|
| 1 | SCS Runoff | 0.95 | 2 | 742 | 7,566 | --- | --- | --- | Predevelopment |
| 2 | SCS Runoff | 2.47 | 2 | 728 | 9,529 | --- | --- | --- | Post Subarea 1a |
| 3 | SCS Runoff | 0.03 | 2 | 728 | 246 | --- | --- | --- | Post Subarea 1b |
| 4 | SCS Runoff | 3.14 | 2 | 730 | 12,761 | --- | --- | --- | Post Subarea 2a |
| 5 | SCS Runoff | 0.03 | 2 | 728 | 238 | --- | --- | --- | Post Subarea 2b |
| 6 | SCS Runoff | 4.47 | 2 | 726 | 15,319 | --- | --- | --- | Post Subarea 3a |
| 7 | SCS Runoff | 0.04 | 2 | 728 | 308 | --- | --- | --- | Post Subarea 3b |
| 8 | Combine | 2.51 | 2 | 728 | 9,775 | 2, 3, | --- | --- | Basin 1 In |
| 9 | Combine | 3.17 | 2 | 730 | 12,999 | 4, 5, | --- | --- | Basin 2 In |
| 10 | Combine | 4.51 | 2 | 726 | 15,627 | 6, 7, | --- | --- | Basin 3 In |
| 11 | Reservoir | 0.19 | 2 | 868 | 9,736 | 8 | 240.79 | 16,427 | Basin 1 Out |
| 12 | Reservoir | 0.22 | 2 | 888 | 10,081 | 9 | 231.74 | 7,891 | Basin 2 Out |
| 13 | Reservoir | 0.41 | 2 | 814 | 15,627 | 10 | 222.01 | 6,951 | Basin 3 Out |
| 14 | Combine | 0.82 | 2 | 850 | 35,444 | 11, 12, 13 | --- | --- | |

Proj. file: ansuya.basin.9-30-04.gpw Return Period: 1 yr

Run date: 10-08-2004

Hydrograph Report

Hyd. No. 12

Basin 2 Out

Hydrograph type = Reservoir
 Storm frequency = 1 yrs
 Inflow hyd. No. = 9
 Max. Elevation = 231.74 ft

Peak discharge = 0.22 cfs
 Time interval = 2 min
 Reservoir name = Detention Basin 2
 Max. Storage = 7,891 cuft

Storage Indication method used.

Outflow hydrograph volume = 10,081 cuft

Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 724 | 2.38 | 230.45 | 6.68 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.024 | 0.02 |
| 728 | 3.04 | 230.61 | 6.68 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.025 | 0.03 |
| 732 | 3.14 | 230.79 | 6.68 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.028 | 0.03 |
| 736 | 2.83 | 230.97 | 6.68 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.030 | 0.03 |
| 740 | 2.37 | 231.12 | 6.68 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | 0.032 | 0.07 |
| 744 | 1.87 | 231.24 | 6.68 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | 0.033 | 0.11 |
| 748 | 1.50 | 231.33 | 6.68 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | 0.034 | 0.14 |
| 752 | 1.22 | 231.40 | 6.68 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | 0.035 | 0.16 |
| 756 | 0.97 | 231.45 | 6.68 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | 0.036 | 0.17 |
| 760 | 0.77 | 231.49 | 6.68 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | 0.036 | 0.18 |
| 764 | 0.64 | 231.52 | 6.68 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | 0.036 | 0.18 |
| 768 | 0.56 | 231.55 | 6.68 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | 0.037 | 0.19 |
| 772 | 0.52 | 231.57 | 6.68 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | 0.037 | 0.19 |
| 776 | 0.48 | 231.59 | 6.68 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | 0.037 | 0.20 |
| 780 | 0.45 | 231.60 | 6.68 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | 0.037 | 0.20 |
| 784 | 0.43 | 231.62 | 6.68 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | 0.038 | 0.20 |
| 788 | 0.40 | 231.63 | 6.68 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | 0.038 | 0.21 |
| 792 | 0.38 | 231.64 | 6.68 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | 0.038 | 0.21 |
| 796 | 0.37 | 231.65 | 6.68 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | 0.038 | 0.21 |
| 800 | 0.36 | 231.66 | 6.68 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | 0.038 | 0.21 |
| 804 | 0.35 | 231.67 | 6.68 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | 0.038 | 0.21 |
| 808 | 0.34 | 231.67 | 6.68 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | 0.038 | 0.21 |
| 812 | 0.33 | 231.68 | 6.68 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | 0.038 | 0.21 |
| 816 | 0.33 | 231.69 | 6.68 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | 0.038 | 0.22 |
| 820 | 0.32 | 231.70 | 6.68 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | 0.038 | 0.22 |
| 824 | 0.31 | 231.70 | 6.68 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | 0.039 | 0.22 |
| 828 | 0.30 | 231.71 | 6.68 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | 0.039 | 0.22 |
| 832 | 0.30 | 231.71 | 6.68 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | 0.039 | 0.22 |
| 836 | 0.29 | 231.72 | 6.68 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | 0.039 | 0.22 |
| 840 | 0.28 | 231.72 | 6.68 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | 0.039 | 0.22 |
| 844 | 0.27 | 231.72 | 6.68 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | 0.039 | 0.22 |
| 848 | 0.26 | 231.72 | 6.68 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | 0.039 | 0.22 |
| 852 | 0.26 | 231.73 | 6.68 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | 0.039 | 0.22 |
| 856 | 0.25 | 231.73 | 6.68 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | 0.039 | 0.22 |
| 860 | 0.25 | 231.73 | 6.68 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | 0.039 | 0.22 |
| 864 | 0.25 | 231.73 | 6.68 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | 0.039 | 0.22 |
| 868 | 0.24 | 231.73 | 6.68 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | 0.039 | 0.22 |
| 872 | 0.24 | 231.73 | 6.68 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | 0.039 | 0.22 |

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Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|---------------|---------------|-----------------|--------------|--------------|--------------|--------------|-------------|-------------|-------------|-------------|--------------|----------------|
| 876 | 0.23 | 231.74 | 6.68 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | 0.039 | 0.22 |
| 880 | 0.23 | 231.74 | 6.68 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | 0.039 | 0.22 |
| 884 | 0.23 | 231.74 | 6.68 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | 0.039 | 0.22 |
| 888 | 0.22 | 231.74 << | 6.68 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | 0.039 | 0.22 << |
| 892 | 0.22 | 231.74 | 6.68 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | 0.039 | 0.22 |
| 896 | 0.21 | 231.74 | 6.68 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | 0.039 | 0.22 |
| 900 | 0.21 | 231.74 | 6.68 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | 0.039 | 0.22 |
| 904 | 0.21 | 231.73 | 6.68 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | 0.039 | 0.22 |
| 908 | 0.20 | 231.73 | 6.68 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | 0.039 | 0.22 |
| 912 | 0.20 | 231.73 | 6.68 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | 0.039 | 0.22 |
| 916 | 0.20 | 231.73 | 6.68 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | 0.039 | 0.22 |
| 920 | 0.19 | 231.73 | 6.68 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | 0.039 | 0.22 |
| 924 | 0.19 | 231.73 | 6.68 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | 0.039 | 0.22 |
| 928 | 0.18 | 231.72 | 6.68 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | 0.039 | 0.22 |
| 932 | 0.18 | 231.72 | 6.68 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | 0.039 | 0.22 |
| 936 | 0.18 | 231.72 | 6.68 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | 0.039 | 0.22 |
| 940 | 0.17 | 231.72 | 6.68 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | 0.039 | 0.22 |
| 944 | 0.17 | 231.71 | 6.68 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | 0.039 | 0.22 |
| 948 | 0.16 | 231.71 | 6.68 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | 0.039 | 0.22 |
| 952 | 0.16 | 231.71 | 6.68 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | 0.039 | 0.22 |
| 956 | 0.16 | 231.70 | 6.68 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | 0.039 | 0.22 |
| 960 | 0.15 | 231.70 | 6.68 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | 0.039 | 0.22 |
| 964 | 0.15 | 231.70 | 6.68 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | 0.039 | 0.22 |
| 968 | 0.14 | 231.69 | 6.68 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | 0.038 | 0.22 |
| 972 | 0.14 | 231.69 | 6.68 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | 0.038 | 0.22 |
| 976 | 0.14 | 231.68 | 6.68 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | 0.038 | 0.21 |
| 980 | 0.14 | 231.68 | 6.68 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | 0.038 | 0.21 |
| 984 | 0.13 | 231.67 | 6.68 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | 0.038 | 0.21 |
| 988 | 0.13 | 231.67 | 6.68 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | 0.038 | 0.21 |
| 992 | 0.13 | 231.67 | 6.68 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | 0.038 | 0.21 |
| 996 | 0.13 | 231.66 | 6.68 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | 0.038 | 0.21 |
| 1000 | 0.13 | 231.66 | 6.68 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | 0.038 | 0.21 |
| 1004 | 0.13 | 231.65 | 6.68 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | 0.038 | 0.21 |
| 1008 | 0.12 | 231.65 | 6.68 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | 0.038 | 0.21 |
| 1012 | 0.12 | 231.64 | 6.68 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | 0.038 | 0.21 |
| 1016 | 0.12 | 231.64 | 6.68 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | 0.038 | 0.21 |
| 1020 | 0.12 | 231.63 | 6.68 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | 0.038 | 0.21 |
| 1024 | 0.12 | 231.63 | 6.68 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | 0.038 | 0.20 |
| 1028 | 0.12 | 231.62 | 6.68 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | 0.038 | 0.20 |
| 1032 | 0.11 | 231.62 | 6.68 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | 0.038 | 0.20 |
| 1036 | 0.11 | 231.61 | 6.68 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | 0.037 | 0.20 |
| 1040 | 0.11 | 231.60 | 6.68 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | 0.037 | 0.20 |
| 1044 | 0.11 | 231.60 | 6.68 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | 0.037 | 0.20 |
| 1048 | 0.11 | 231.59 | 6.68 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | 0.037 | 0.20 |
| 1052 | 0.10 | 231.59 | 6.68 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | 0.037 | 0.20 |
| 1056 | 0.10 | 231.58 | 6.68 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | 0.037 | 0.20 |
| 1060 | 0.10 | 231.58 | 6.68 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | 0.037 | 0.20 |
| 1064 | 0.10 | 231.57 | 6.68 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | 0.037 | 0.19 |
| 1068 | 0.10 | 231.57 | 6.68 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | 0.037 | 0.19 |
| 1072 | 0.10 | 231.56 | 6.68 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | 0.037 | 0.19 |
| 1076 | 0.09 | 231.55 | 6.68 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | 0.037 | 0.19 |

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Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Civ A cfs | Civ B cfs | Civ C cfs | Civ D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 1080 | 0.09 | 231.55 | 6.68 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | 0.037 | 0.19 |
| 1084 | 0.09 | 231.54 | 6.68 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | 0.037 | 0.19 |
| 1088 | 0.09 | 231.54 | 6.68 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | 0.037 | 0.19 |
| 1092 | 0.09 | 231.53 | 6.68 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | 0.037 | 0.19 |
| 1096 | 0.09 | 231.53 | 6.68 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | 0.036 | 0.18 |
| 1100 | 0.09 | 231.52 | 6.68 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | 0.036 | 0.18 |
| 1104 | 0.09 | 231.51 | 6.68 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | 0.036 | 0.18 |
| 1108 | 0.09 | 231.51 | 6.68 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | 0.036 | 0.18 |
| 1112 | 0.08 | 231.50 | 6.68 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | 0.036 | 0.18 |
| 1116 | 0.08 | 231.50 | 6.68 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | 0.036 | 0.18 |
| 1120 | 0.08 | 231.49 | 6.68 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | 0.036 | 0.18 |
| 1124 | 0.08 | 231.49 | 6.68 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | 0.036 | 0.18 |
| 1128 | 0.08 | 231.48 | 6.68 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | 0.036 | 0.18 |
| 1132 | 0.08 | 231.48 | 6.68 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | 0.036 | 0.17 |
| 1136 | 0.08 | 231.47 | 6.68 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | 0.036 | 0.17 |
| 1140 | 0.08 | 231.46 | 6.68 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | 0.036 | 0.17 |
| 1144 | 0.08 | 231.46 | 6.68 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | 0.036 | 0.17 |
| 1148 | 0.08 | 231.45 | 6.68 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | 0.036 | 0.17 |
| 1152 | 0.08 | 231.45 | 6.68 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | 0.036 | 0.17 |
| 1156 | 0.08 | 231.44 | 6.68 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | 0.035 | 0.17 |
| 1160 | 0.08 | 231.44 | 6.68 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | 0.035 | 0.17 |
| 1164 | 0.08 | 231.43 | 6.68 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | 0.035 | 0.17 |
| 1168 | 0.08 | 231.43 | 6.68 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | 0.035 | 0.16 |
| 1172 | 0.08 | 231.42 | 6.68 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | 0.035 | 0.16 |
| 1176 | 0.08 | 231.42 | 6.68 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | 0.035 | 0.16 |
| 1180 | 0.08 | 231.41 | 6.68 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | 0.035 | 0.16 |
| 1184 | 0.08 | 231.41 | 6.68 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | 0.035 | 0.16 |
| 1188 | 0.07 | 231.40 | 6.68 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | 0.035 | 0.16 |
| 1192 | 0.07 | 231.40 | 6.68 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | 0.035 | 0.16 |
| 1196 | 0.07 | 231.39 | 6.68 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | 0.035 | 0.16 |
| 1200 | 0.07 | 231.39 | 6.68 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | 0.035 | 0.16 |
| 1204 | 0.07 | 231.38 | 6.68 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | 0.035 | 0.15 |
| 1208 | 0.07 | 231.38 | 6.68 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | 0.035 | 0.15 |
| 1212 | 0.07 | 231.37 | 6.68 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | 0.035 | 0.15 |
| 1216 | 0.07 | 231.37 | 6.68 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | 0.035 | 0.15 |
| 1220 | 0.07 | 231.36 | 6.68 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | 0.035 | 0.15 |
| 1224 | 0.07 | 231.36 | 6.68 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | 0.034 | 0.15 |
| 1228 | 0.07 | 231.36 | 6.68 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | 0.034 | 0.15 |
| 1232 | 0.07 | 231.35 | 6.68 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | 0.034 | 0.14 |
| 1236 | 0.07 | 231.35 | 6.68 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | 0.034 | 0.14 |
| 1240 | 0.07 | 231.34 | 6.68 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | 0.034 | 0.14 |
| 1244 | 0.07 | 231.34 | 6.68 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | 0.034 | 0.14 |
| 1248 | 0.07 | 231.33 | 6.68 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | 0.034 | 0.14 |
| 1252 | 0.07 | 231.33 | 6.68 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | 0.034 | 0.14 |
| 1256 | 0.07 | 231.33 | 6.68 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | 0.034 | 0.14 |
| 1260 | 0.07 | 231.32 | 6.68 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | 0.034 | 0.13 |
| 1264 | 0.06 | 231.32 | 6.68 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | 0.034 | 0.13 |
| 1268 | 0.06 | 231.31 | 6.68 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | 0.034 | 0.13 |
| 1272 | 0.06 | 231.31 | 6.68 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | 0.034 | 0.13 |
| 1276 | 0.06 | 231.31 | 6.68 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | 0.034 | 0.13 |
| 1280 | 0.06 | 231.30 | 6.68 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | 0.034 | 0.13 |

Continues on next page...

Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 1284 | 0.06 | 231.30 | 6.68 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | 0.034 | 0.13 |
| 1288 | 0.06 | 231.29 | 6.68 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | 0.034 | 0.13 |
| 1292 | 0.06 | 231.29 | 6.68 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | 0.034 | 0.13 |
| 1296 | 0.06 | 231.29 | 6.68 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | 0.034 | 0.12 |
| 1300 | 0.06 | 231.28 | 6.68 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | 0.034 | 0.12 |
| 1304 | 0.06 | 231.28 | 6.68 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | 0.033 | 0.12 |
| 1308 | 0.06 | 231.28 | 6.68 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | 0.033 | 0.12 |
| 1312 | 0.06 | 231.27 | 6.68 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | 0.033 | 0.12 |
| 1316 | 0.06 | 231.27 | 6.68 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | 0.033 | 0.12 |
| 1320 | 0.06 | 231.26 | 6.68 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | 0.033 | 0.12 |
| 1324 | 0.07 | 231.26 | 6.68 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | 0.033 | 0.12 |
| 1328 | 0.07 | 231.26 | 6.68 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | 0.033 | 0.12 |
| 1332 | 0.07 | 231.26 | 6.68 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | 0.033 | 0.11 |
| 1336 | 0.07 | 231.25 | 6.68 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | 0.033 | 0.11 |
| 1340 | 0.07 | 231.25 | 6.68 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | 0.033 | 0.11 |
| 1344 | 0.06 | 231.25 | 6.68 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | 0.033 | 0.11 |
| 1348 | 0.06 | 231.24 | 6.68 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | 0.033 | 0.11 |
| 1352 | 0.06 | 231.24 | 6.68 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | 0.033 | 0.11 |
| 1356 | 0.06 | 231.24 | 6.68 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | 0.033 | 0.11 |
| 1360 | 0.06 | 231.24 | 6.68 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | 0.033 | 0.11 |
| 1364 | 0.06 | 231.23 | 6.68 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | 0.033 | 0.11 |
| 1368 | 0.06 | 231.23 | 6.68 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | 0.033 | 0.11 |
| 1372 | 0.06 | 231.23 | 6.68 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | 0.033 | 0.11 |
| 1376 | 0.06 | 231.22 | 6.68 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | 0.033 | 0.10 |
| 1380 | 0.05 | 231.22 | 6.68 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | 0.033 | 0.10 |
| 1384 | 0.05 | 231.22 | 6.68 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | 0.033 | 0.10 |
| 1388 | 0.05 | 231.22 | 6.68 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | 0.033 | 0.10 |
| 1392 | 0.05 | 231.21 | 6.68 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | 0.033 | 0.10 |
| 1396 | 0.05 | 231.21 | 6.68 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | 0.033 | 0.10 |
| 1400 | 0.05 | 231.21 | 6.68 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | 0.033 | 0.10 |
| 1404 | 0.05 | 231.20 | 6.68 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | 0.033 | 0.10 |
| 1408 | 0.05 | 231.20 | 6.68 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | 0.033 | 0.10 |
| 1412 | 0.05 | 231.20 | 6.68 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | 0.033 | 0.10 |
| 1416 | 0.05 | 231.20 | 6.68 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | 0.033 | 0.10 |
| 1420 | 0.05 | 231.19 | 6.68 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | 0.032 | 0.10 |
| 1424 | 0.05 | 231.19 | 6.68 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | 0.032 | 0.09 |
| 1428 | 0.05 | 231.19 | 6.68 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | 0.032 | 0.09 |
| 1432 | 0.05 | 231.19 | 6.68 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | 0.032 | 0.09 |
| 1436 | 0.05 | 231.18 | 6.68 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | 0.032 | 0.09 |
| 1440 | 0.05 | 231.18 | 6.68 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | 0.032 | 0.09 |
| 1444 | 0.04 | 231.18 | 6.68 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | 0.032 | 0.09 |
| 1448 | 0.03 | 231.17 | 6.68 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | 0.032 | 0.09 |
| 1452 | 0.02 | 231.17 | 6.68 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | 0.032 | 0.09 |
| 1456 | 0.01 | 231.17 | 6.68 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | 0.032 | 0.09 |
| 1460 | 0.00 | 231.16 | 6.68 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | 0.032 | 0.08 |
| 1464 | 0.00 | 231.16 | 6.68 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | 0.032 | 0.08 |
| 1468 | 0.00 | 231.15 | 6.68 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | 0.032 | 0.08 |
| 1472 | 0.00 | 231.15 | 6.68 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | 0.032 | 0.08 |
| 1476 | 0.00 | 231.14 | 6.68 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | 0.032 | 0.08 |
| 1480 | 0.00 | 231.14 | 6.68 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | 0.032 | 0.08 |
| 1484 | 0.00 | 231.13 | 6.68 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | 0.032 | 0.08 |

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Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 1488 | 0.00 | 231.13 | 6.68 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | 0.032 | 0.07 |
| 1492 | 0.00 | 231.13 | 6.68 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | 0.032 | 0.07 |
| 1496 | 0.00 | 231.12 | 6.68 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | 0.032 | 0.07 |
| 1500 | 0.00 | 231.12 | 6.68 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | 0.032 | 0.07 |
| 1504 | 0.00 | 231.11 | 6.68 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | 0.032 | 0.07 |
| 1508 | 0.00 | 231.11 | 6.68 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | 0.031 | 0.07 |
| 1512 | 0.00 | 231.10 | 6.68 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | 0.031 | 0.07 |
| 1516 | 0.00 | 231.10 | 6.68 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | 0.031 | 0.06 |
| 1520 | 0.00 | 231.10 | 6.68 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | 0.031 | 0.06 |
| 1524 | 0.00 | 231.09 | 6.68 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | 0.031 | 0.06 |
| 1528 | 0.00 | 231.09 | 6.68 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | 0.031 | 0.06 |
| 1532 | 0.00 | 231.09 | 6.68 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | 0.031 | 0.06 |
| 1536 | 0.00 | 231.08 | 6.68 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | 0.031 | 0.06 |
| 1540 | 0.00 | 231.08 | 6.68 | 0.03 | ---- | ---- | ---- | ---- | ---- | ---- | 0.031 | 0.06 |
| 1544 | 0.00 | 231.08 | 6.68 | 0.02 | ---- | ---- | ---- | ---- | ---- | ---- | 0.031 | 0.06 |
| 1548 | 0.00 | 231.07 | 6.68 | 0.02 | ---- | ---- | ---- | ---- | ---- | ---- | 0.031 | 0.05 |
| 1552 | 0.00 | 231.07 | 6.68 | 0.02 | ---- | ---- | ---- | ---- | ---- | ---- | 0.031 | 0.05 |
| 1556 | 0.00 | 231.07 | 6.68 | 0.02 | ---- | ---- | ---- | ---- | ---- | ---- | 0.031 | 0.05 |
| 1560 | 0.00 | 231.06 | 6.68 | 0.02 | ---- | ---- | ---- | ---- | ---- | ---- | 0.031 | 0.05 |
| 1564 | 0.00 | 231.06 | 6.68 | 0.02 | ---- | ---- | ---- | ---- | ---- | ---- | 0.031 | 0.05 |
| 1568 | 0.00 | 231.06 | 6.68 | 0.02 | ---- | ---- | ---- | ---- | ---- | ---- | 0.031 | 0.05 |
| 1572 | 0.00 | 231.05 | 6.68 | 0.02 | ---- | ---- | ---- | ---- | ---- | ---- | 0.031 | 0.05 |
| 1576 | 0.00 | 231.05 | 6.68 | 0.02 | ---- | ---- | ---- | ---- | ---- | ---- | 0.031 | 0.05 |
| 1580 | 0.00 | 231.05 | 6.68 | 0.02 | ---- | ---- | ---- | ---- | ---- | ---- | 0.031 | 0.05 |
| 1584 | 0.00 | 231.05 | 6.68 | 0.02 | ---- | ---- | ---- | ---- | ---- | ---- | 0.031 | 0.05 |
| 1588 | 0.00 | 231.04 | 6.68 | 0.01 | ---- | ---- | ---- | ---- | ---- | ---- | 0.031 | 0.04 |
| 1592 | 0.00 | 231.04 | 6.68 | 0.01 | ---- | ---- | ---- | ---- | ---- | ---- | 0.031 | 0.04 |
| 1596 | 0.00 | 231.04 | 6.68 | 0.01 | ---- | ---- | ---- | ---- | ---- | ---- | 0.031 | 0.04 |
| 1600 | 0.00 | 231.04 | 6.68 | 0.01 | ---- | ---- | ---- | ---- | ---- | ---- | 0.031 | 0.04 |
| 1604 | 0.00 | 231.03 | 6.68 | 0.01 | ---- | ---- | ---- | ---- | ---- | ---- | 0.031 | 0.04 |
| 1608 | 0.00 | 231.03 | 6.68 | 0.01 | ---- | ---- | ---- | ---- | ---- | ---- | 0.031 | 0.04 |
| 1612 | 0.00 | 231.03 | 6.68 | 0.01 | ---- | ---- | ---- | ---- | ---- | ---- | 0.031 | 0.04 |
| 1616 | 0.00 | 231.03 | 6.68 | 0.01 | ---- | ---- | ---- | ---- | ---- | ---- | 0.030 | 0.04 |
| 1620 | 0.00 | 231.02 | 6.68 | 0.01 | ---- | ---- | ---- | ---- | ---- | ---- | 0.030 | 0.04 |
| 1624 | 0.00 | 231.02 | 6.68 | 0.01 | ---- | ---- | ---- | ---- | ---- | ---- | 0.030 | 0.04 |
| 1628 | 0.00 | 231.02 | 6.68 | 0.01 | ---- | ---- | ---- | ---- | ---- | ---- | 0.030 | 0.04 |
| 1632 | 0.00 | 231.02 | 6.68 | 0.01 | ---- | ---- | ---- | ---- | ---- | ---- | 0.030 | 0.04 |
| 1636 | 0.00 | 231.02 | 6.68 | 0.01 | ---- | ---- | ---- | ---- | ---- | ---- | 0.030 | 0.04 |
| 1640 | 0.00 | 231.01 | 6.68 | 0.00 | ---- | ---- | ---- | ---- | ---- | ---- | 0.030 | 0.03 |
| 1644 | 0.00 | 231.01 | 6.68 | 0.00 | ---- | ---- | ---- | ---- | ---- | ---- | 0.030 | 0.03 |
| 1648 | 0.00 | 231.01 | 6.68 | 0.00 | ---- | ---- | ---- | ---- | ---- | ---- | 0.030 | 0.03 |
| 1652 | 0.00 | 231.01 | 6.68 | 0.00 | ---- | ---- | ---- | ---- | ---- | ---- | 0.030 | 0.03 |
| 1656 | 0.00 | 231.01 | 6.68 | 0.00 | ---- | ---- | ---- | ---- | ---- | ---- | 0.030 | 0.03 |
| 1660 | 0.00 | 231.00 | 6.68 | 0.00 | ---- | ---- | ---- | ---- | ---- | ---- | 0.030 | 0.03 |
| 1664 | 0.00 | 231.00 | 6.68 | 0.00 | ---- | ---- | ---- | ---- | ---- | ---- | 0.030 | 0.03 |
| 1668 | 0.00 | 231.00 | 6.68 | 0.00 | ---- | ---- | ---- | ---- | ---- | ---- | 0.030 | 0.03 |
| 1672 | 0.00 | 231.00 | 6.68 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.030 | 0.03 |
| 1676 | 0.00 | 231.00 | 6.68 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.030 | 0.03 |
| 1680 | 0.00 | 230.99 | 6.68 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.030 | 0.03 |
| 1684 | 0.00 | 230.99 | 6.68 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.030 | 0.03 |
| 1688 | 0.00 | 230.99 | 6.68 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.030 | 0.03 |

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Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 2712 | 0.00 | 230.58 | 6.68 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.025 | 0.03 |
| 2716 | 0.00 | 230.57 | 6.68 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.025 | 0.03 |
| 2720 | 0.00 | 230.57 | 6.68 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.025 | 0.03 |
| 2724 | 0.00 | 230.57 | 6.68 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.025 | 0.03 |
| 2728 | 0.00 | 230.57 | 6.68 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.025 | 0.03 |
| 2732 | 0.00 | 230.57 | 6.68 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.025 | 0.02 |
| 2736 | 0.00 | 230.57 | 6.68 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.025 | 0.02 |
| 2740 | 0.00 | 230.57 | 6.68 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.025 | 0.02 |
| 2744 | 0.00 | 230.56 | 6.68 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.025 | 0.02 |
| 2748 | 0.00 | 230.56 | 6.68 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.025 | 0.02 |
| 2752 | 0.00 | 230.56 | 6.68 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.025 | 0.02 |
| 2756 | 0.00 | 230.56 | 6.68 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.025 | 0.02 |
| 2760 | 0.00 | 230.56 | 6.68 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.025 | 0.02 |
| 2764 | 0.00 | 230.56 | 6.68 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.025 | 0.02 |
| 2768 | 0.00 | 230.56 | 6.68 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.025 | 0.02 |
| 2772 | 0.00 | 230.55 | 6.68 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.025 | 0.02 |
| 2776 | 0.00 | 230.55 | 6.68 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.025 | 0.02 |
| 2780 | 0.00 | 230.55 | 6.68 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.025 | 0.02 |
| 2784 | 0.00 | 230.55 | 6.68 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.025 | 0.02 |
| 2788 | 0.00 | 230.55 | 6.68 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.025 | 0.02 |
| 2792 | 0.00 | 230.55 | 6.68 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.025 | 0.02 |
| 2796 | 0.00 | 230.55 | 6.68 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.025 | 0.02 |
| 2800 | 0.00 | 230.54 | 6.68 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.025 | 0.02 |
| 2804 | 0.00 | 230.54 | 6.68 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.025 | 0.02 |
| 2808 | 0.00 | 230.54 | 6.68 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.025 | 0.02 |
| 2812 | 0.00 | 230.54 | 6.68 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.025 | 0.02 |
| 2816 | 0.00 | 230.54 | 6.68 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.025 | 0.02 |
| 2820 | 0.00 | 230.54 | 6.68 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.025 | 0.02 |
| 2824 | 0.00 | 230.54 | 6.68 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.025 | 0.02 |
| 2828 | 0.00 | 230.53 | 6.68 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.025 | 0.02 |
| 2832 | 0.00 | 230.53 | 6.68 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.025 | 0.02 |
| 2836 | 0.00 | 230.53 | 6.68 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.025 | 0.02 |
| 2840 | 0.00 | 230.53 | 6.68 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.025 | 0.02 |
| 2844 | 0.00 | 230.53 | 6.68 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.025 | 0.02 |
| 2848 | 0.00 | 230.53 | 6.68 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.024 | 0.02 |
| 2852 | 0.00 | 230.53 | 6.68 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.024 | 0.02 |
| 2856 | 0.00 | 230.52 | 6.68 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.024 | 0.02 |
| 2860 | 0.00 | 230.52 | 6.68 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.024 | 0.02 |
| 2864 | 0.00 | 230.52 | 6.68 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.024 | 0.02 |
| 2868 | 0.00 | 230.52 | 6.68 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.024 | 0.02 |
| 2872 | 0.00 | 230.52 | 6.68 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.024 | 0.02 |
| 2876 | 0.00 | 230.52 | 6.68 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.024 | 0.02 |
| 2880 | 0.00 | 230.52 | 6.68 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.024 | 0.02 |

...End

Reservoir Report

Reservoir No. 2 - Detention Basin 2

Hydraflow Hydrographs by Intelisolve

Pond Data

Pond storage is based on known contour areas. Average end area method used.

Stage / Storage Table

| Stage (ft) | Elevation (ft) | Contour area (sqft) | Incr. Storage (cuft) | Total storage (cuft) |
|------------|----------------|---------------------|----------------------|----------------------|
| 0.00 | 229.33 | 00 | 0 | 0 |
| 0.67 | 230.00 | 2,454 | 822 | 822 |
| 2.67 | 232.00 | 5,689 | 8,143 | 8,965 |
| 4.67 | 234.00 | 6,522 | 12,211 | 21,176 |
| 6.67 | 236.00 | 7,413 | 13,935 | 35,111 |
| 8.67 | 238.00 | 9,192 | 16,605 | 51,716 |

Culvert / Orifice Structures

| | [A] | [B] | [C] | [D] |
|---------------|----------|--------|------|------|
| Rise in | = 6.0 | 3.0 | 0.0 | 0.0 |
| Span in | = 6.0 | 3.0 | 0.0 | 0.0 |
| No. Barrels | = 10 | 1 | 0 | 0 |
| Invert El. ft | = 228.40 | 231.00 | 0.00 | 0.00 |
| Length ft | = 40.0 | 1.0 | 0.0 | 0.0 |
| Slope % | = 1.00 | 0.00 | 0.00 | 0.00 |
| N-Value | = .013 | .013 | .000 | .000 |
| Orif. Coeff. | = 0.60 | 0.60 | 0.00 | 0.00 |
| Multi-Stage | = n/a | Yes | No | No |

Weir Structures

| | [A] | [B] | [C] | [D] |
|--------------|----------|--------|--------|------|
| Crest Len ft | = 0.66 | 20.00 | 16.00 | 0.00 |
| Crest El. ft | = 232.00 | 236.00 | 235.50 | 0.00 |
| Weir Coeff. | = 3.33 | 2.60 | 3.33 | 0.00 |
| Weir Type | = Rect | Broad | Rect | --- |
| Multi-Stage | = Yes | No | Yes | No |

Exfiltration Rate = 0.32 in/hr/sqft Tailwater Elev. = 0.00 ft

Note: All outflows have been analyzed under inlet and outlet control.

Stage / Storage / Discharge Table

| Stage ft | Storage cuft | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Total cfs |
|----------|--------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-----------|
| 0.00 | 0 | 229.33 | 0.00 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.000 | 0.00 |
| 0.07 | 82 | 229.40 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.002 | 0.00 |
| 0.13 | 164 | 229.46 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.004 | 0.00 |
| 0.20 | 247 | 229.53 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.005 | 0.01 |
| 0.27 | 329 | 229.60 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.007 | 0.01 |
| 0.34 | 411 | 229.67 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.009 | 0.01 |
| 0.40 | 493 | 229.73 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.011 | 0.01 |
| 0.47 | 575 | 229.80 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.013 | 0.01 |
| 0.54 | 658 | 229.87 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.015 | 0.01 |
| 0.60 | 740 | 229.93 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.016 | 0.02 |
| 0.67 | 822 | 230.00 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.018 | 0.02 |
| 0.87 | 1,636 | 230.20 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.021 | 0.02 |
| 1.07 | 2,451 | 230.40 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.023 | 0.02 |
| 1.27 | 3,265 | 230.60 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.025 | 0.03 |
| 1.47 | 4,079 | 230.80 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.028 | 0.03 |
| 1.67 | 4,894 | 231.00 | 6.68 | 0.00 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.030 | 0.03 |
| 1.87 | 5,708 | 231.20 | 6.68 | 0.06 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.033 | 0.10 |
| 2.07 | 6,522 | 231.40 | 6.68 | 0.12 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.035 | 0.16 |
| 2.27 | 7,336 | 231.60 | 6.68 | 0.16 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.037 | 0.20 |
| 2.47 | 8,151 | 231.80 | 6.68 | 0.19 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.040 | 0.23 |
| 2.67 | 8,965 | 232.00 | 6.68 | 0.22 | --- | --- | 0.00 | 0.00 | 0.00 | --- | 0.042 | 0.26 |
| 2.87 | 10,186 | 232.20 | 6.68 | 0.25 | --- | --- | 0.20 | 0.00 | 0.00 | --- | 0.043 | 0.48 |
| 3.07 | 11,407 | 232.40 | 6.68 | 0.27 | --- | --- | 0.56 | 0.00 | 0.00 | --- | 0.043 | 0.87 |
| 3.27 | 12,628 | 232.60 | 6.68 | 0.29 | --- | --- | 1.02 | 0.00 | 0.00 | --- | 0.044 | 1.35 |
| 3.47 | 13,849 | 232.80 | 6.68 | 0.31 | --- | --- | 1.57 | 0.00 | 0.00 | --- | 0.045 | 1.92 |
| 3.67 | 15,071 | 233.00 | 6.68 | 0.32 | --- | --- | 2.20 | 0.00 | 0.00 | --- | 0.045 | 2.57 |
| 3.87 | 16,292 | 233.20 | 6.68 | 0.34 | --- | --- | 2.89 | 0.00 | 0.00 | --- | 0.046 | 3.28 |
| 4.07 | 17,513 | 233.40 | 6.68 | 0.36 | --- | --- | 3.64 | 0.00 | 0.00 | --- | 0.046 | 4.04 |
| 4.27 | 18,734 | 233.60 | 6.68 | 0.37 | --- | --- | 4.45 | 0.00 | 0.00 | --- | 0.047 | 4.87 |
| 4.47 | 19,955 | 233.80 | 6.68 | 0.39 | --- | --- | 5.31 | 0.00 | 0.00 | --- | 0.048 | 5.74 |
| 4.67 | 21,176 | 234.00 | 6.68 | 0.40 | --- | --- | 6.22 | 0.00 | 0.00 | --- | 0.048 | 6.67 |
| 4.87 | 22,570 | 234.20 | 7.59 | 0.41 | --- | --- | 7.17 | 0.00 | 0.00 | --- | 0.049 | 7.64 |

Continues on next page...

Stage / Storage / Discharge Table

| Stage ft | Storage cuft | Elevation ft | Civ A cfs | Civ B cfs | Civ C cfs | Civ D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Total cfs |
|-------------|-----------------|-----------------|--------------|--------------|--------------|--------------|-------------|-------------|-------------|-------------|--------------|--------------|
| 5.07 | 23,963 | 234.40 | 8.60 | 0.43 | --- | --- | 8.17 | 0.00 | 0.00 | --- | 0.050 | 8.65 |
| 5.27 | 25,357 | 234.60 | 9.65 | 0.44 | --- | --- | 9.21 | 0.00 | 0.00 | --- | 0.050 | 9.70 |
| 5.47 | 26,750 | 234.80 | 10.75 | 0.45 | --- | --- | 10.30 | 0.00 | 0.00 | --- | 0.051 | 10.80 |
| 5.67 | 28,144 | 235.00 | 11.89 | 0.47 | --- | --- | 11.42 | 0.00 | 0.00 | --- | 0.052 | 11.94 |
| 5.87 | 29,537 | 235.20 | 13.03 | 0.44 | --- | --- | 12.58 | 0.00 | 0.00 | --- | 0.052 | 13.08 |
| 6.07 | 30,931 | 235.40 | 14.12 | 0.42 | --- | --- | 13.70 | 0.00 | 0.00 | --- | 0.053 | 14.17 |
| 6.27 | 32,324 | 235.60 | 15.89 | 0.37 | --- | --- | 13.84 | 0.00 | 1.68 | --- | 0.054 | 15.94 |
| 6.47 | 33,718 | 235.80 | 18.81 | 0.20 | --- | --- | 9.85 | 0.00 | 8.75 | --- | 0.054 | 18.86 |
| 6.67 | 35,111 | 236.00 | 19.86 | 0.10 | --- | --- | 5.97 | 0.00 | 13.80 | --- | 0.055 | 19.92 |
| 6.87 | 36,772 | 236.20 | 20.25 | 0.07 | --- | --- | 4.74 | 4.65 | 15.44 | --- | 0.056 | 24.95 |
| 7.07 | 38,432 | 236.40 | 20.56 | 0.05 | --- | --- | 4.01 | 13.15 | 16.50 | --- | 0.058 | 33.77 |
| 7.27 | 40,093 | 236.60 | 20.84 | 0.04 | --- | --- | 3.52 | 24.17 | 17.27 | --- | 0.059 | 45.05 |
| 7.47 | 41,753 | 236.80 | 21.10 | 0.03 | --- | --- | 3.17 | 37.21 | 17.88 | --- | 0.060 | 58.35 |
| 7.67 | 43,414 | 237.00 | 21.36 | 0.03 | --- | --- | 2.91 | 52.00 | 18.41 | --- | 0.061 | 73.40 |
| 7.87 | 45,074 | 237.20 | 21.62 | 0.02 | --- | --- | 2.71 | 68.35 | 18.85 | --- | 0.063 | 90.00 |
| 8.07 | 46,735 | 237.40 | 21.87 | 0.02 | --- | --- | 2.54 | 86.14 | 19.22 | --- | 0.064 | 107.99 |
| 8.27 | 48,395 | 237.60 | 22.12 | 0.02 | --- | --- | 2.41 | 105.24 | 19.56 | --- | 0.065 | 127.29 |
| 8.47 | 50,056 | 237.80 | 22.36 | 0.02 | --- | --- | 2.31 | 125.57 | 19.95 | --- | 0.067 | 147.91 |
| 8.67 | 51,716 | 238.00 | 22.60 | 0.01 | --- | --- | 2.21 | 147.08 | 20.20 | --- | 0.068 | 169.58 |

...End

Hydrograph Report

Hyd. No. 13

Basin 3 Out

Hydrograph type = Reservoir
 Storm frequency = 1 yrs
 Inflow hyd. No. = 10
 Max. Elevation = 222.01 ft

Peak discharge = 0.41 cfs
 Time interval = 2 min
 Reservoir name = Basin 3 (Hotel)
 Max. Storage = 6,951 cuft

Storage Indication method used.

Outflow hydrograph volume = 15,627 cuft

Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Civ A cfs | Civ B cfs | Civ C cfs | Civ D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 596 | 0.06 | 219.06 | 5.93 | 0.04 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.04 |
| 600 | 0.06 | 219.06 | 6.45 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 604 | 0.06 | 219.07 | 6.98 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 608 | 0.07 | 219.07 | 7.54 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |
| 612 | 0.07 | 219.08 | 8.14 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |
| 616 | 0.08 | 219.08 | 8.79 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |
| 620 | 0.09 | 219.09 | 9.50 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 624 | 0.09 | 219.10 | 10.24 | 0.07 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.07 |
| 628 | 0.10 | 219.10 | 10.70 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 632 | 0.11 | 219.11 | 10.70 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 636 | 0.11 | 219.12 | 10.70 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 640 | 0.12 | 219.13 | 10.70 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 644 | 0.13 | 219.15 | 10.70 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 648 | 0.14 | 219.16 | 10.70 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 652 | 0.15 | 219.18 | 10.70 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 656 | 0.15 | 219.19 | 10.70 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 660 | 0.16 | 219.21 | 10.70 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.11 |
| 664 | 0.17 | 219.23 | 10.70 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.11 |
| 668 | 0.19 | 219.25 | 10.70 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.12 |
| 672 | 0.21 | 219.28 | 10.70 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.12 |
| 676 | 0.23 | 219.31 | 10.70 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 680 | 0.26 | 219.35 | 10.70 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 684 | 0.28 | 219.39 | 10.70 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 688 | 0.31 | 219.44 | 10.70 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |
| 692 | 0.34 | 219.50 | 10.70 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 696 | 0.42 | 219.57 | 10.70 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 700 | 0.58 | 219.67 | 10.70 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 704 | 0.80 | 219.84 | 10.70 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 708 | 1.06 | 220.02 | 10.70 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 712 | 1.36 | 220.09 | 10.70 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 716 | 1.73 | 220.19 | 10.70 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 720 | 2.68 | 220.34 | 10.70 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 724 | 4.17 | 220.58 | 10.70 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 728 | 4.40 | 220.90 | 10.70 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 732 | 3.45 | 221.18 | 10.70 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 736 | 2.56 | 221.39 | 10.70 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 740 | 2.13 | 221.54 | 10.70 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 744 | 1.81 | 221.66 | 10.70 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |

Continues on next page...

Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 748 | 1.48 | 221.76 | 10.70 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 752 | 1.14 | 221.83 | 10.70 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 756 | 0.87 | 221.88 | 10.70 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 760 | 0.74 | 221.91 | 10.70 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 764 | 0.68 | 221.93 | 10.70 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 768 | 0.64 | 221.95 | 10.70 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.41 |
| 772 | 0.61 | 221.97 | 10.70 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.41 |
| 776 | 0.57 | 221.98 | 10.70 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.41 |
| 780 | 0.53 | 221.99 | 10.70 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.41 |
| 784 | 0.50 | 222.00 | 10.70 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.41 |
| 788 | 0.48 | 222.00 | 10.70 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.41 |
| 792 | 0.46 | 222.01 | 10.70 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.41 |
| 796 | 0.45 | 222.01 | 10.70 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.41 |
| 800 | 0.44 | 222.01 | 10.70 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.41 |
| 804 | 0.43 | 222.01 | 10.70 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.41 |
| 808 | 0.42 | 222.01 | 10.70 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.41 |
| 812 | 0.41 | 222.01 | 10.70 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.41 |
| 816 | 0.40 | 222.01 | 10.70 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.41 |
| 820 | 0.40 | 222.01 | 10.70 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.41 |
| 824 | 0.39 | 222.01 | 10.70 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.41 |
| 828 | 0.38 | 222.01 | 10.70 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.41 |
| 832 | 0.37 | 222.01 | 10.70 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.41 |
| 836 | 0.36 | 222.01 | 10.70 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.41 |
| 840 | 0.35 | 222.00 | 10.70 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.41 |
| 844 | 0.34 | 222.00 | 10.70 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.41 |
| 848 | 0.33 | 221.99 | 10.70 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.41 |
| 852 | 0.32 | 221.99 | 10.70 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.41 |
| 856 | 0.32 | 221.98 | 10.70 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.41 |
| 860 | 0.31 | 221.97 | 10.70 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.41 |
| 864 | 0.31 | 221.97 | 10.70 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.41 |
| 868 | 0.30 | 221.96 | 10.70 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.41 |
| 872 | 0.30 | 221.95 | 10.70 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.41 |
| 876 | 0.29 | 221.94 | 10.70 | 0.41 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.41 |
| 880 | 0.29 | 221.93 | 10.70 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 884 | 0.29 | 221.92 | 10.70 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 888 | 0.28 | 221.91 | 10.70 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 892 | 0.28 | 221.90 | 10.70 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 896 | 0.27 | 221.89 | 10.70 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 900 | 0.27 | 221.88 | 10.70 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 904 | 0.26 | 221.87 | 10.70 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 908 | 0.26 | 221.86 | 10.70 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 912 | 0.25 | 221.85 | 10.70 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 916 | 0.25 | 221.84 | 10.70 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 920 | 0.24 | 221.83 | 10.70 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 924 | 0.24 | 221.82 | 10.70 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 928 | 0.23 | 221.80 | 10.70 | 0.40 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.40 |
| 932 | 0.23 | 221.79 | 10.70 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 936 | 0.22 | 221.78 | 10.70 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 940 | 0.22 | 221.76 | 10.70 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 944 | 0.21 | 221.75 | 10.70 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 948 | 0.20 | 221.73 | 10.70 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |

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Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 952 | 0.20 | 221.72 | 10.70 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 956 | 0.19 | 221.71 | 10.70 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 960 | 0.19 | 221.69 | 10.70 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 964 | 0.18 | 221.67 | 10.70 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 968 | 0.18 | 221.66 | 10.70 | 0.39 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.39 |
| 972 | 0.18 | 221.64 | 10.70 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 976 | 0.18 | 221.63 | 10.70 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 980 | 0.17 | 221.61 | 10.70 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 984 | 0.17 | 221.59 | 10.70 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 988 | 0.17 | 221.58 | 10.70 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 992 | 0.17 | 221.56 | 10.70 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 996 | 0.16 | 221.55 | 10.70 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1000 | 0.16 | 221.53 | 10.70 | 0.38 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.38 |
| 1004 | 0.16 | 221.51 | 10.70 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1008 | 0.16 | 221.50 | 10.70 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1012 | 0.16 | 221.48 | 10.70 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1016 | 0.15 | 221.46 | 10.70 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1020 | 0.15 | 221.45 | 10.70 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1024 | 0.15 | 221.43 | 10.70 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1028 | 0.15 | 221.41 | 10.70 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1032 | 0.14 | 221.39 | 10.70 | 0.37 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.37 |
| 1036 | 0.14 | 221.38 | 10.70 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1040 | 0.14 | 221.36 | 10.70 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1044 | 0.14 | 221.34 | 10.70 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1048 | 0.14 | 221.32 | 10.70 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1052 | 0.13 | 221.31 | 10.70 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1056 | 0.13 | 221.29 | 10.70 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1060 | 0.13 | 221.27 | 10.70 | 0.36 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.36 |
| 1064 | 0.13 | 221.25 | 10.70 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1068 | 0.12 | 221.24 | 10.70 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1072 | 0.12 | 221.22 | 10.70 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1076 | 0.12 | 221.20 | 10.70 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1080 | 0.12 | 221.18 | 10.70 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1084 | 0.12 | 221.16 | 10.70 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1088 | 0.11 | 221.15 | 10.70 | 0.35 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.35 |
| 1092 | 0.11 | 221.13 | 10.70 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1096 | 0.11 | 221.11 | 10.70 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1100 | 0.11 | 221.09 | 10.70 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1104 | 0.11 | 221.08 | 10.70 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1108 | 0.11 | 221.06 | 10.70 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1112 | 0.11 | 221.04 | 10.70 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1116 | 0.11 | 221.02 | 10.70 | 0.34 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.34 |
| 1120 | 0.11 | 221.00 | 10.70 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1124 | 0.11 | 220.99 | 10.70 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1128 | 0.11 | 220.97 | 10.70 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1132 | 0.11 | 220.95 | 10.70 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1136 | 0.11 | 220.93 | 10.70 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1140 | 0.10 | 220.92 | 10.70 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1144 | 0.10 | 220.90 | 10.70 | 0.33 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.33 |
| 1148 | 0.10 | 220.88 | 10.70 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1152 | 0.10 | 220.87 | 10.70 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |

Continues on next page...

Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 1156 | 0.10 | 220.85 | 10.70 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1160 | 0.10 | 220.83 | 10.70 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1164 | 0.10 | 220.81 | 10.70 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1168 | 0.10 | 220.80 | 10.70 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1172 | 0.10 | 220.78 | 10.70 | 0.32 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.32 |
| 1176 | 0.10 | 220.76 | 10.70 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1180 | 0.10 | 220.75 | 10.70 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1184 | 0.10 | 220.73 | 10.70 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1188 | 0.10 | 220.71 | 10.70 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1192 | 0.10 | 220.70 | 10.70 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1196 | 0.10 | 220.68 | 10.70 | 0.31 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.31 |
| 1200 | 0.09 | 220.66 | 10.70 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1204 | 0.09 | 220.65 | 10.70 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1208 | 0.09 | 220.63 | 10.70 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1212 | 0.09 | 220.62 | 10.70 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1216 | 0.09 | 220.60 | 10.70 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1220 | 0.09 | 220.58 | 10.70 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1224 | 0.09 | 220.57 | 10.70 | 0.30 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.30 |
| 1228 | 0.09 | 220.55 | 10.70 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1232 | 0.09 | 220.54 | 10.70 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1236 | 0.09 | 220.52 | 10.70 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1240 | 0.09 | 220.50 | 10.70 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1244 | 0.09 | 220.49 | 10.70 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1248 | 0.09 | 220.47 | 10.70 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1252 | 0.09 | 220.46 | 10.70 | 0.29 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.29 |
| 1256 | 0.08 | 220.44 | 10.70 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 1260 | 0.08 | 220.43 | 10.70 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 1264 | 0.08 | 220.41 | 10.70 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 1268 | 0.08 | 220.40 | 10.70 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 1272 | 0.08 | 220.38 | 10.70 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 1276 | 0.08 | 220.37 | 10.70 | 0.28 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.28 |
| 1280 | 0.08 | 220.35 | 10.70 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 1284 | 0.08 | 220.34 | 10.70 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 1288 | 0.08 | 220.32 | 10.70 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 1292 | 0.08 | 220.31 | 10.70 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 1296 | 0.08 | 220.29 | 10.70 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 1300 | 0.08 | 220.28 | 10.70 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 1304 | 0.08 | 220.26 | 10.70 | 0.27 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.27 |
| 1308 | 0.08 | 220.25 | 10.70 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 1312 | 0.07 | 220.23 | 10.70 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 1316 | 0.07 | 220.22 | 10.70 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 1320 | 0.07 | 220.20 | 10.70 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 1324 | 0.10 | 220.19 | 10.70 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 1328 | 0.11 | 220.18 | 10.70 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 1332 | 0.09 | 220.17 | 10.70 | 0.26 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.26 |
| 1336 | 0.08 | 220.15 | 10.70 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 1340 | 0.08 | 220.14 | 10.70 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 1344 | 0.08 | 220.13 | 10.70 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 1348 | 0.08 | 220.11 | 10.70 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 1352 | 0.07 | 220.10 | 10.70 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |
| 1356 | 0.07 | 220.09 | 10.70 | 0.25 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.25 |

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Hydrograph Discharge Table

| Time (min) | Inflow cfs | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Outflow cfs |
|------------|------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-------------|
| 1360 | 0.07 | 220.07 | 10.70 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 1364 | 0.07 | 220.06 | 10.70 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 1368 | 0.07 | 220.05 | 10.70 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 1372 | 0.07 | 220.03 | 10.70 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 1376 | 0.07 | 220.02 | 10.70 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 1380 | 0.07 | 220.01 | 10.70 | 0.24 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.24 |
| 1384 | 0.07 | 219.97 | 10.70 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 1388 | 0.07 | 219.92 | 10.70 | 0.23 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.23 |
| 1392 | 0.07 | 219.87 | 10.70 | 0.22 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.22 |
| 1396 | 0.07 | 219.82 | 10.70 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 1400 | 0.07 | 219.77 | 10.70 | 0.21 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.21 |
| 1404 | 0.07 | 219.72 | 10.70 | 0.20 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.20 |
| 1408 | 0.07 | 219.68 | 10.70 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 1412 | 0.07 | 219.64 | 10.70 | 0.19 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.19 |
| 1416 | 0.07 | 219.59 | 10.70 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 1420 | 0.07 | 219.56 | 10.70 | 0.18 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.18 |
| 1424 | 0.06 | 219.52 | 10.70 | 0.17 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.17 |
| 1428 | 0.06 | 219.48 | 10.70 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |
| 1432 | 0.06 | 219.45 | 10.70 | 0.16 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.16 |
| 1436 | 0.06 | 219.42 | 10.70 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 1440 | 0.06 | 219.39 | 10.70 | 0.15 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.15 |
| 1444 | 0.05 | 219.36 | 10.70 | 0.14 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.14 |
| 1448 | 0.02 | 219.32 | 10.70 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 1452 | 0.00 | 219.28 | 10.70 | 0.13 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.13 |
| 1456 | 0.00 | 219.24 | 10.70 | 0.12 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.12 |
| 1460 | 0.00 | 219.20 | 10.70 | 0.11 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.11 |
| 1464 | 0.00 | 219.17 | 10.70 | 0.10 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.10 |
| 1468 | 0.00 | 219.14 | 10.70 | 0.09 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.09 |
| 1472 | 0.00 | 219.11 | 10.70 | 0.08 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.08 |
| 1476 | 0.00 | 219.09 | 9.11 | 0.06 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.06 |
| 1480 | 0.00 | 219.07 | 7.06 | 0.05 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.05 |

...End

Reservoir Report

Reservoir No. 3 - Basin 3 (Hotel)

Hydraflow Hydrographs by Intelisolve

Pond Data

Pond storage is based on known contour areas. Average end area method used.

Stage / Storage Table

| Stage (ft) | Elevation (ft) | Contour area (sqft) | Incr. Storage (cuft) | Total storage (cuft) |
|------------|----------------|---------------------|----------------------|----------------------|
| 0.00 | 219.00 | 00 | 0 | 0 |
| 1.00 | 220.00 | 1,406 | 703 | 703 |
| 3.00 | 222.00 | 4,776 | 6,182 | 6,885 |
| 5.00 | 224.00 | 5,971 | 10,747 | 17,632 |
| 7.00 | 226.00 | 7,278 | 13,249 | 30,881 |
| 9.00 | 228.00 | 8,709 | 15,987 | 46,868 |
| 9.50 | 228.50 | 9,086 | 4,449 | 51,317 |

Culvert / Orifice Structures

| | [A] | [B] | [C] | [D] |
|---------------|----------|--------|--------|------|
| Rise in | = 24.0 | 3.0 | 12.0 | 0.0 |
| Span in | = 24.0 | 3.0 | 12.0 | 0.0 |
| No. Barrels | = 1 | 1 | 1 | 0 |
| Invert El. ft | = 217.50 | 217.90 | 224.00 | 0.00 |
| Length ft | = 48.0 | 1.0 | 1.0 | 0.0 |
| Slope % | = 10.00 | 0.00 | 0.00 | 0.00 |
| N-Value | = .013 | .013 | .013 | .000 |
| Orif. Coeff. | = 0.60 | 0.60 | 0.60 | 0.00 |
| Multi-Stage | = n/a | Yes | Yes | No |

Weir Structures

| | [A] | [B] | [C] | [D] |
|--------------|----------|--------|--------|--------|
| Crest Len ft | = 1.00 | 2.00 | 16.00 | 90.00 |
| Crest El. ft | = 225.25 | 226.00 | 227.00 | 227.00 |
| Weir Coeff. | = 3.33 | 3.33 | 3.33 | 2.60 |
| Weir Type | = Rect | Rect | Rect | Broad |
| Multi-Stage | = Yes | Yes | Yes | Yes |

Exfiltration Rate = 0.00 in/hr/sqft Tailwater Elev. = 0.00 ft

Stage / Storage / Discharge Table

Note: All outflows have been analyzed under inlet and outlet control.

| Stage ft | Storage cuft | Elevation ft | Civ A cfs | Civ B cfs | Civ C cfs | Civ D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Total cfs |
|----------|--------------|--------------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-----------|
| 0.00 | 0 | 219.00 | 0.00 | 0.00 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.00 |
| 0.10 | 70 | 219.10 | 10.70 | 0.07 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.07 |
| 0.20 | 141 | 219.20 | 10.70 | 0.11 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.11 |
| 0.30 | 211 | 219.30 | 10.70 | 0.13 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.13 |
| 0.40 | 281 | 219.40 | 10.70 | 0.15 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.15 |
| 0.50 | 352 | 219.50 | 10.70 | 0.17 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.17 |
| 0.60 | 422 | 219.60 | 10.70 | 0.18 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.18 |
| 0.70 | 492 | 219.70 | 10.70 | 0.20 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.20 |
| 0.80 | 562 | 219.80 | 10.70 | 0.21 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.21 |
| 0.90 | 633 | 219.90 | 10.70 | 0.22 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.22 |
| 1.00 | 703 | 220.00 | 10.70 | 0.24 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.24 |
| 1.20 | 1,321 | 220.20 | 10.70 | 0.26 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.26 |
| 1.40 | 1,939 | 220.40 | 10.70 | 0.28 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.28 |
| 1.60 | 2,558 | 220.60 | 10.70 | 0.30 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.30 |
| 1.80 | 3,176 | 220.80 | 10.70 | 0.32 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.32 |
| 2.00 | 3,794 | 221.00 | 10.70 | 0.33 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.33 |
| 2.20 | 4,412 | 221.20 | 10.70 | 0.35 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.35 |
| 2.40 | 5,030 | 221.40 | 10.70 | 0.37 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.37 |
| 2.60 | 5,649 | 221.60 | 10.70 | 0.38 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.38 |
| 2.80 | 6,267 | 221.80 | 10.70 | 0.40 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.40 |
| 3.00 | 6,885 | 222.00 | 10.70 | 0.41 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.41 |
| 3.20 | 7,960 | 222.20 | 10.70 | 0.42 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.42 |
| 3.40 | 9,034 | 222.40 | 10.70 | 0.44 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.44 |
| 3.60 | 10,109 | 222.60 | 10.70 | 0.45 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.45 |
| 3.80 | 11,184 | 222.80 | 10.70 | 0.46 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.46 |
| 4.00 | 12,259 | 223.00 | 10.70 | 0.47 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.47 |
| 4.20 | 13,333 | 223.20 | 10.70 | 0.48 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.48 |
| 4.40 | 14,408 | 223.40 | 10.70 | 0.50 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.50 |
| 4.60 | 15,483 | 223.60 | 10.70 | 0.51 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.51 |
| 4.80 | 16,557 | 223.80 | 10.70 | 0.52 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.52 |
| 5.00 | 17,632 | 224.00 | 10.70 | 0.53 | 0.00 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.53 |

Continues on next page...

Stage / Storage / Discharge Table

| Stage ft | Storage cuft | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | Clv D cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | Total cfs |
|-------------|-----------------|-----------------|--------------|--------------|--------------|--------------|-------------|-------------|-------------|-------------|--------------|--------------|
| 5.20 | 18,957 | 224.20 | 10.70 | 0.54 | 0.18 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 0.72 |
| 5.40 | 20,282 | 224.40 | 10.70 | 0.55 | 0.64 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 1.19 |
| 5.60 | 21,607 | 224.60 | 10.70 | 0.56 | 1.34 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 1.90 |
| 5.80 | 22,932 | 224.80 | 10.70 | 0.57 | 2.07 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 2.64 |
| 6.00 | 24,257 | 225.00 | 10.70 | 0.58 | 2.67 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 3.25 |
| 6.20 | 25,581 | 225.20 | 10.70 | 0.59 | 3.16 | --- | 0.00 | 0.00 | 0.00 | 0.00 | --- | 3.75 |
| 6.40 | 26,906 | 225.40 | 10.70 | 0.60 | 3.59 | --- | 0.19 | 0.00 | 0.00 | 0.00 | --- | 4.38 |
| 6.60 | 28,231 | 225.60 | 10.70 | 0.61 | 3.97 | --- | 0.69 | 0.00 | 0.00 | 0.00 | --- | 5.26 |
| 6.80 | 29,556 | 225.80 | 10.70 | 0.62 | 4.31 | --- | 1.36 | 0.00 | 0.00 | 0.00 | --- | 6.29 |
| 7.00 | 30,881 | 226.00 | 10.70 | 0.63 | 4.63 | --- | 2.16 | 0.00 | 0.00 | 0.00 | --- | 7.42 |
| 7.20 | 32,480 | 226.20 | 10.70 | 0.63 | 4.93 | --- | 3.08 | 0.60 | 0.00 | 0.00 | --- | 9.24 |
| 7.40 | 34,078 | 226.40 | 11.69 | 0.64 | 5.21 | --- | 4.11 | 1.68 | 0.00 | 0.00 | --- | 11.64 |
| 7.60 | 35,677 | 226.60 | 14.47 | 0.63 | 5.48 | --- | 5.22 | 3.10 | 0.00 | 0.00 | --- | 14.43 |
| 7.80 | 37,276 | 226.80 | 17.55 | 0.62 | 5.73 | --- | 6.43 | 4.77 | 0.00 | 0.00 | --- | 17.55 |
| 8.00 | 38,875 | 227.00 | 20.95 | 0.61 | 5.98 | --- | 7.71 | 6.66 | 0.00 | 0.00 | --- | 20.95 |
| 8.20 | 40,473 | 227.20 | 42.98 | 0.19 | 2.99 | --- | 6.61 | 7.50 | 4.76 | 20.93 | --- | 42.98 |
| 8.40 | 42,072 | 227.40 | 45.00 | 0.05 | 0.84 | --- | 2.87 | 3.56 | 6.98 | 30.65 | --- | 44.96 |
| 8.60 | 43,671 | 227.60 | 45.58 | 0.03 | 0.50 | --- | 2.13 | 2.78 | 7.43 | 32.62 | --- | 45.49 |
| 8.80 | 45,269 | 227.80 | 46.10 | 0.02 | 0.35 | --- | 1.75 | 2.38 | 7.69 | 33.77 | --- | 45.95 |
| 9.00 | 46,868 | 228.00 | 46.61 | 0.02 | 0.26 | --- | 1.53 | 2.14 | 7.90 | 34.69 | --- | 46.53 |
| 9.05 | 47,313 | 228.05 | 46.73 | 0.02 | 0.24 | --- | 1.48 | 2.09 | 7.91 | 34.75 | --- | 46.48 |
| 9.10 | 47,758 | 228.10 | 46.85 | 0.01 | 0.23 | --- | 1.43 | 2.04 | 7.92 | 34.79 | --- | 46.41 |
| 9.15 | 48,203 | 228.15 | 46.98 | 0.01 | 0.21 | --- | 1.39 | 2.00 | 7.95 | 34.93 | --- | 46.50 |
| 9.20 | 48,648 | 228.20 | 47.10 | 0.01 | 0.20 | --- | 1.37 | 1.97 | 8.02 | 35.22 | --- | 46.79 |
| 9.25 | 49,092 | 228.25 | 47.22 | 0.01 | 0.19 | --- | 1.33 | 1.94 | 8.04 | 35.33 | --- | 46.85 |
| 9.30 | 49,537 | 228.30 | 47.34 | 0.01 | 0.18 | --- | 1.30 | 1.89 | 8.01 | 35.19 | --- | 46.59 |
| 9.35 | 49,982 | 228.35 | 47.46 | 0.01 | 0.17 | --- | 1.27 | 1.87 | 8.07 | 35.43 | --- | 46.82 |
| 9.40 | 50,427 | 228.40 | 47.58 | 0.01 | 0.16 | --- | 1.25 | 1.84 | 8.07 | 35.43 | --- | 46.76 |
| 9.45 | 50,872 | 228.45 | 47.70 | 0.01 | 0.16 | --- | 1.24 | 1.84 | 8.21 | 36.07 | --- | 47.54 |
| 9.50 | 51,317 | 228.50 | 47.83 | 0.01 | 0.15 | --- | 1.20 | 1.79 | 8.08 | 35.50 | --- | 46.73 |

...End

Hydrograph Report

Hyd. No. 14

Hydrograph type = Combine
Storm frequency = 1 yrs
Inflow hyds. = 11, 12, 13

Peak discharge = 0.82 cfs
Time interval = 2 min

Hydrograph Volume = 35,444 cuft

Hydrograph Discharge Table

| Time (min) | Hyd. 11 + (cfs) | Hyd. 12 + (cfs) | Hyd. 13 = (cfs) | Outflow (cfs) |
|------------|-----------------|-----------------|-----------------|---------------|
| 624 | 0.01 | 0.01 | 0.07 | 0.09 |
| 628 | 0.01 | 0.01 | 0.08 | 0.09 |
| 632 | 0.01 | 0.01 | 0.08 | 0.09 |
| 636 | 0.01 | 0.01 | 0.08 | 0.10 |
| 640 | 0.01 | 0.01 | 0.09 | 0.10 |
| 644 | 0.01 | 0.01 | 0.09 | 0.11 |
| 648 | 0.01 | 0.01 | 0.09 | 0.11 |
| 652 | 0.01 | 0.01 | 0.10 | 0.12 |
| 656 | 0.01 | 0.01 | 0.10 | 0.13 |
| 660 | 0.01 | 0.01 | 0.11 | 0.13 |
| 664 | 0.01 | 0.01 | 0.11 | 0.14 |
| 668 | 0.02 | 0.01 | 0.12 | 0.15 |
| 672 | 0.02 | 0.02 | 0.12 | 0.16 |
| 676 | 0.02 | 0.02 | 0.13 | 0.17 |
| 680 | 0.02 | 0.02 | 0.14 | 0.18 |
| 684 | 0.02 | 0.02 | 0.15 | 0.19 |
| 688 | 0.02 | 0.02 | 0.16 | 0.20 |
| 692 | 0.02 | 0.02 | 0.17 | 0.21 |
| 696 | 0.03 | 0.02 | 0.18 | 0.22 |
| 700 | 0.03 | 0.02 | 0.19 | 0.24 |
| 704 | 0.03 | 0.02 | 0.22 | 0.27 |
| 708 | 0.04 | 0.02 | 0.24 | 0.30 |
| 712 | 0.05 | 0.02 | 0.25 | 0.31 |
| 716 | 0.05 | 0.02 | 0.26 | 0.33 |
| 720 | 0.07 | 0.02 | 0.27 | 0.36 |
| 724 | 0.08 | 0.02 | 0.30 | 0.40 |
| 728 | 0.11 | 0.03 | 0.33 | 0.46 |
| 732 | 0.13 | 0.03 | 0.35 | 0.51 |
| 736 | 0.14 | 0.03 | 0.36 | 0.54 |
| 740 | 0.16 | 0.07 | 0.38 | 0.60 |
| 744 | 0.16 | 0.11 | 0.39 | 0.66 |
| 748 | 0.17 | 0.14 | 0.39 | 0.70 |
| 752 | 0.17 | 0.16 | 0.40 | 0.73 |
| 756 | 0.18 | 0.17 | 0.40 | 0.75 |
| 760 | 0.18 | 0.18 | 0.40 | 0.76 |
| 764 | 0.18 | 0.18 | 0.40 | 0.77 |
| 768 | 0.18 | 0.19 | 0.41 | 0.78 |
| 772 | 0.18 | 0.19 | 0.41 | 0.78 |

Continues on next page...

Hydrograph Discharge Table

| Time (min) | Hyd. 11 + (cfs) | Hyd. 12 + (cfs) | Hyd. 13 = (cfs) | Outflow (cfs) |
|---------------|--------------------|--------------------|--------------------|------------------|
| 776 | 0.18 | 0.20 | 0.41 | 0.79 |
| 780 | 0.19 | 0.20 | 0.41 | 0.80 |
| 784 | 0.19 | 0.20 | 0.41 | 0.80 |
| 788 | 0.19 | 0.21 | 0.41 | 0.80 |
| 792 | 0.19 | 0.21 | 0.41 | 0.80 |
| 796 | 0.19 | 0.21 | 0.41 | 0.81 |
| 800 | 0.19 | 0.21 | 0.41 | 0.81 |
| 804 | 0.19 | 0.21 | 0.41 | 0.81 |
| 808 | 0.19 | 0.21 | 0.41 | 0.81 |
| 812 | 0.19 | 0.21 | 0.41 | 0.81 |
| 816 | 0.19 | 0.22 | 0.41 | 0.82 |
| 820 | 0.19 | 0.22 | 0.41 | 0.82 |
| 824 | 0.19 | 0.22 | 0.41 | 0.82 |
| 828 | 0.19 | 0.22 | 0.41 | 0.82 |
| 832 | 0.19 | 0.22 | 0.41 | 0.82 |
| 836 | 0.19 | 0.22 | 0.41 | 0.82 |
| 840 | 0.19 | 0.22 | 0.41 | 0.82 |
| 844 | 0.19 | 0.22 | 0.41 | 0.82 |
| 848 | 0.19 | 0.22 | 0.41 | 0.82 |
| 852 | 0.19 | 0.22 | 0.41 | 0.82 |
| 856 | 0.19 | 0.22 | 0.41 | 0.82 |
| 860 | 0.19 | 0.22 | 0.41 | 0.82 |
| 864 | 0.19 | 0.22 | 0.41 | 0.82 |
| 868 | 0.19 << | 0.22 | 0.41 | 0.82 |
| 872 | 0.19 | 0.22 | 0.41 | 0.82 |
| 876 | 0.19 | 0.22 | 0.41 | 0.82 |
| 880 | 0.19 | 0.22 | 0.40 | 0.82 |
| 884 | 0.19 | 0.22 | 0.40 | 0.82 |
| 888 | 0.19 | 0.22 << | 0.40 | 0.82 |
| 892 | 0.19 | 0.22 | 0.40 | 0.82 |
| 896 | 0.19 | 0.22 | 0.40 | 0.82 |
| 900 | 0.19 | 0.22 | 0.40 | 0.82 |
| 904 | 0.19 | 0.22 | 0.40 | 0.82 |
| 908 | 0.19 | 0.22 | 0.40 | 0.81 |
| 912 | 0.19 | 0.22 | 0.40 | 0.81 |
| 916 | 0.19 | 0.22 | 0.40 | 0.81 |
| 920 | 0.19 | 0.22 | 0.40 | 0.81 |
| 924 | 0.19 | 0.22 | 0.40 | 0.81 |
| 928 | 0.19 | 0.22 | 0.40 | 0.81 |
| 932 | 0.19 | 0.22 | 0.39 | 0.81 |
| 936 | 0.19 | 0.22 | 0.39 | 0.80 |
| 940 | 0.19 | 0.22 | 0.39 | 0.80 |
| 944 | 0.19 | 0.22 | 0.39 | 0.80 |
| 948 | 0.19 | 0.22 | 0.39 | 0.80 |
| 952 | 0.19 | 0.22 | 0.39 | 0.80 |
| 956 | 0.19 | 0.22 | 0.39 | 0.80 |
| 960 | 0.19 | 0.22 | 0.39 | 0.79 |
| 964 | 0.19 | 0.22 | 0.39 | 0.79 |
| 968 | 0.19 | 0.22 | 0.39 | 0.79 |
| 972 | 0.19 | 0.22 | 0.38 | 0.79 |
| 976 | 0.19 | 0.21 | 0.38 | 0.78 |

Continues on next page...

Hydrograph Discharge Table

| Time (min) | Hyd. 11 + (cfs) | Hyd. 12 + (cfs) | Hyd. 13 = (cfs) | Outflow (cfs) |
|---------------|--------------------|--------------------|--------------------|------------------|
| 980 | 0.19 | 0.21 | 0.38 | 0.78 |
| 984 | 0.19 | 0.21 | 0.38 | 0.78 |
| 988 | 0.19 | 0.21 | 0.38 | 0.78 |
| 992 | 0.19 | 0.21 | 0.38 | 0.77 |
| 996 | 0.18 | 0.21 | 0.38 | 0.77 |
| 1000 | 0.18 | 0.21 | 0.38 | 0.77 |
| 1004 | 0.18 | 0.21 | 0.37 | 0.77 |
| 1008 | 0.18 | 0.21 | 0.37 | 0.76 |
| 1012 | 0.18 | 0.21 | 0.37 | 0.76 |
| 1016 | 0.18 | 0.21 | 0.37 | 0.76 |
| 1020 | 0.18 | 0.21 | 0.37 | 0.76 |
| 1024 | 0.18 | 0.20 | 0.37 | 0.75 |
| 1028 | 0.18 | 0.20 | 0.37 | 0.75 |
| 1032 | 0.18 | 0.20 | 0.37 | 0.75 |
| 1036 | 0.18 | 0.20 | 0.36 | 0.75 |
| 1040 | 0.18 | 0.20 | 0.36 | 0.74 |
| 1044 | 0.18 | 0.20 | 0.36 | 0.74 |
| 1048 | 0.18 | 0.20 | 0.36 | 0.74 |
| 1052 | 0.18 | 0.20 | 0.36 | 0.73 |
| 1056 | 0.18 | 0.20 | 0.36 | 0.73 |
| 1060 | 0.18 | 0.20 | 0.36 | 0.73 |
| 1064 | 0.18 | 0.19 | 0.35 | 0.73 |
| 1068 | 0.18 | 0.19 | 0.35 | 0.72 |
| 1072 | 0.18 | 0.19 | 0.35 | 0.72 |
| 1076 | 0.17 | 0.19 | 0.35 | 0.72 |
| 1080 | 0.17 | 0.19 | 0.35 | 0.71 |
| 1084 | 0.17 | 0.19 | 0.35 | 0.71 |
| 1088 | 0.17 | 0.19 | 0.35 | 0.71 |
| 1092 | 0.17 | 0.19 | 0.34 | 0.70 |
| 1096 | 0.17 | 0.18 | 0.34 | 0.70 |
| 1100 | 0.17 | 0.18 | 0.34 | 0.70 |
| 1104 | 0.17 | 0.18 | 0.34 | 0.69 |
| 1108 | 0.17 | 0.18 | 0.34 | 0.69 |
| 1112 | 0.17 | 0.18 | 0.34 | 0.69 |
| 1116 | 0.17 | 0.18 | 0.34 | 0.68 |
| 1120 | 0.17 | 0.18 | 0.33 | 0.68 |
| 1124 | 0.17 | 0.18 | 0.33 | 0.68 |
| 1128 | 0.17 | 0.18 | 0.33 | 0.67 |
| 1132 | 0.17 | 0.17 | 0.33 | 0.67 |
| 1136 | 0.17 | 0.17 | 0.33 | 0.67 |
| 1140 | 0.17 | 0.17 | 0.33 | 0.67 |
| 1144 | 0.17 | 0.17 | 0.33 | 0.66 |
| 1148 | 0.16 | 0.17 | 0.32 | 0.66 |
| 1152 | 0.16 | 0.17 | 0.32 | 0.66 |
| 1156 | 0.16 | 0.17 | 0.32 | 0.65 |
| 1160 | 0.16 | 0.17 | 0.32 | 0.65 |
| 1164 | 0.16 | 0.17 | 0.32 | 0.65 |
| 1168 | 0.16 | 0.16 | 0.32 | 0.64 |
| 1172 | 0.16 | 0.16 | 0.32 | 0.64 |
| 1176 | 0.16 | 0.16 | 0.31 | 0.64 |
| 1180 | 0.16 | 0.16 | 0.31 | 0.63 |

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Hydrograph Discharge Table

| Time (min) | Hyd. 11 + (cfs) | Hyd. 12 + (cfs) | Hyd. 13 = (cfs) | Outflow (cfs) |
|---------------|--------------------|--------------------|--------------------|------------------|
| 1184 | 0.16 | 0.16 | 0.31 | 0.63 |
| 1188 | 0.16 | 0.16 | 0.31 | 0.63 |
| 1192 | 0.16 | 0.16 | 0.31 | 0.62 |
| 1196 | 0.16 | 0.16 | 0.31 | 0.62 |
| 1200 | 0.16 | 0.16 | 0.30 | 0.62 |
| 1204 | 0.16 | 0.15 | 0.30 | 0.61 |
| 1208 | 0.15 | 0.15 | 0.30 | 0.61 |
| 1212 | 0.15 | 0.15 | 0.30 | 0.61 |
| 1216 | 0.15 | 0.15 | 0.30 | 0.60 |
| 1220 | 0.15 | 0.15 | 0.30 | 0.60 |
| 1224 | 0.15 | 0.15 | 0.30 | 0.59 |
| 1228 | 0.15 | 0.15 | 0.29 | 0.59 |
| 1232 | 0.15 | 0.14 | 0.29 | 0.59 |
| 1236 | 0.15 | 0.14 | 0.29 | 0.58 |
| 1240 | 0.15 | 0.14 | 0.29 | 0.58 |
| 1244 | 0.15 | 0.14 | 0.29 | 0.58 |
| 1248 | 0.15 | 0.14 | 0.29 | 0.57 |
| 1252 | 0.15 | 0.14 | 0.29 | 0.57 |
| 1256 | 0.15 | 0.14 | 0.28 | 0.57 |
| 1260 | 0.15 | 0.13 | 0.28 | 0.56 |
| 1264 | 0.15 | 0.13 | 0.28 | 0.56 |
| 1268 | 0.14 | 0.13 | 0.28 | 0.56 |
| 1272 | 0.14 | 0.13 | 0.28 | 0.55 |
| 1276 | 0.14 | 0.13 | 0.28 | 0.55 |
| 1280 | 0.14 | 0.13 | 0.27 | 0.55 |
| 1284 | 0.14 | 0.13 | 0.27 | 0.54 |
| 1288 | 0.14 | 0.13 | 0.27 | 0.54 |
| 1292 | 0.14 | 0.13 | 0.27 | 0.54 |
| 1296 | 0.14 | 0.12 | 0.27 | 0.53 |
| 1300 | 0.14 | 0.12 | 0.27 | 0.53 |
| 1304 | 0.14 | 0.12 | 0.27 | 0.53 |
| 1308 | 0.14 | 0.12 | 0.26 | 0.52 |
| 1312 | 0.14 | 0.12 | 0.26 | 0.52 |
| 1316 | 0.14 | 0.12 | 0.26 | 0.52 |
| 1320 | 0.14 | 0.12 | 0.26 | 0.51 |
| 1324 | 0.14 | 0.12 | 0.26 | 0.51 |
| 1328 | 0.14 | 0.12 | 0.26 | 0.51 |
| 1332 | 0.14 | 0.11 | 0.26 | 0.50 |
| 1336 | 0.13 | 0.11 | 0.25 | 0.50 |
| 1340 | 0.13 | 0.11 | 0.25 | 0.50 |
| 1344 | 0.13 | 0.11 | 0.25 | 0.50 |
| 1348 | 0.13 | 0.11 | 0.25 | 0.49 |
| 1352 | 0.13 | 0.11 | 0.25 | 0.49 |
| 1356 | 0.13 | 0.11 | 0.25 | 0.49 |
| 1360 | 0.13 | 0.11 | 0.24 | 0.48 |
| 1364 | 0.13 | 0.11 | 0.24 | 0.48 |
| 1368 | 0.13 | 0.11 | 0.24 | 0.48 |
| 1372 | 0.13 | 0.11 | 0.24 | 0.47 |
| 1376 | 0.13 | 0.10 | 0.24 | 0.47 |
| 1380 | 0.13 | 0.10 | 0.24 | 0.47 |
| 1384 | 0.13 | 0.10 | 0.23 | 0.46 |

Continues on next page...

Hydrograph Discharge Table

| Time (min) | Hyd. 11 + (cfs) | Hyd. 12 + (cfs) | Hyd. 13 = (cfs) | Outflow (cfs) |
|---------------|--------------------|--------------------|--------------------|------------------|
| 1388 | 0.13 | 0.10 | 0.23 | 0.46 |
| 1392 | 0.13 | 0.10 | 0.22 | 0.45 |
| 1396 | 0.13 | 0.10 | 0.21 | 0.44 |
| 1400 | 0.13 | 0.10 | 0.21 | 0.43 |
| 1404 | 0.12 | 0.10 | 0.20 | 0.42 |
| 1408 | 0.12 | 0.10 | 0.19 | 0.42 |
| 1412 | 0.12 | 0.10 | 0.19 | 0.41 |
| 1416 | 0.12 | 0.10 | 0.18 | 0.40 |
| 1420 | 0.12 | 0.10 | 0.18 | 0.39 |
| 1424 | 0.12 | 0.09 | 0.17 | 0.38 |
| 1428 | 0.12 | 0.09 | 0.16 | 0.38 |
| 1432 | 0.12 | 0.09 | 0.16 | 0.37 |
| 1436 | 0.12 | 0.09 | 0.15 | 0.36 |
| 1440 | 0.12 | 0.09 | 0.15 | 0.36 |
| 1444 | 0.12 | 0.09 | 0.14 | 0.35 |
| 1448 | 0.12 | 0.09 | 0.13 | 0.34 |
| 1452 | 0.11 | 0.09 | 0.13 | 0.33 |
| 1456 | 0.11 | 0.09 | 0.12 | 0.31 |
| 1460 | 0.11 | 0.08 | 0.11 | 0.30 |
| 1464 | 0.11 | 0.08 | 0.10 | 0.29 |
| 1468 | 0.11 | 0.08 | 0.09 | 0.28 |
| 1472 | 0.11 | 0.08 | 0.08 | 0.27 |
| 1476 | 0.11 | 0.08 | 0.06 | 0.25 |
| 1480 | 0.11 | 0.08 | 0.05 | 0.23 |
| 1484 | 0.11 | 0.08 | 0.04 | 0.22 |
| 1488 | 0.10 | 0.07 | 0.03 | 0.21 |
| 1492 | 0.10 | 0.07 | 0.02 | 0.20 |
| 1496 | 0.10 | 0.07 | 0.02 | 0.19 |
| 1500 | 0.10 | 0.07 | 0.01 | 0.18 |
| 1504 | 0.10 | 0.07 | 0.01 | 0.18 |
| 1508 | 0.10 | 0.07 | 0.01 | 0.17 |
| 1512 | 0.10 | 0.07 | 0.01 | 0.17 |
| 1516 | 0.10 | 0.06 | 0.00 | 0.17 |
| 1520 | 0.10 | 0.06 | 0.00 | 0.16 |
| 1524 | 0.09 | 0.06 | 0.00 | 0.16 |
| 1528 | 0.09 | 0.06 | 0.00 | 0.16 |
| 1532 | 0.09 | 0.06 | 0.00 | 0.15 |
| 1536 | 0.09 | 0.06 | 0.00 | 0.15 |
| 1540 | 0.09 | 0.06 | 0.00 | 0.15 |
| 1544 | 0.09 | 0.06 | 0.00 | 0.15 |
| 1548 | 0.09 | 0.05 | 0.00 | 0.14 |
| 1552 | 0.09 | 0.05 | 0.00 | 0.14 |
| 1556 | 0.09 | 0.05 | 0.00 | 0.14 |
| 1560 | 0.09 | 0.05 | 0.00 | 0.14 |
| 1564 | 0.09 | 0.05 | 0.00 | 0.14 |
| 1568 | 0.08 | 0.05 | 0.00 | 0.13 |
| 1572 | 0.08 | 0.05 | 0.00 | 0.13 |
| 1576 | 0.08 | 0.05 | 0.00 | 0.13 |
| 1580 | 0.08 | 0.05 | 0.00 | 0.13 |
| 1584 | 0.08 | 0.05 | 0.00 | 0.13 |
| 1588 | 0.08 | 0.04 | 0.00 | 0.12 |

Continues on next page...

Hydrograph Discharge Table

| Time (min) | Hyd. 11 + (cfs) | Hyd. 12 + (cfs) | Hyd. 13 = (cfs) | Outflow (cfs) |
|---------------|--------------------|--------------------|--------------------|------------------|
| 1592 | 0.08 | 0.04 | 0.00 | 0.12 |
| 1596 | 0.08 | 0.04 | 0.00 | 0.12 |
| 1600 | 0.08 | 0.04 | 0.00 | 0.12 |
| 1604 | 0.08 | 0.04 | 0.00 | 0.12 |
| 1608 | 0.08 | 0.04 | 0.00 | 0.12 |
| 1612 | 0.07 | 0.04 | 0.00 | 0.11 |
| 1616 | 0.07 | 0.04 | 0.00 | 0.11 |
| 1620 | 0.07 | 0.04 | 0.00 | 0.11 |
| 1624 | 0.07 | 0.04 | 0.00 | 0.11 |
| 1628 | 0.07 | 0.04 | 0.00 | 0.11 |
| 1632 | 0.07 | 0.04 | 0.00 | 0.11 |
| 1636 | 0.07 | 0.04 | 0.00 | 0.11 |
| 1640 | 0.07 | 0.03 | 0.00 | 0.10 |
| 1644 | 0.07 | 0.03 | 0.00 | 0.10 |
| 1648 | 0.07 | 0.03 | 0.00 | 0.10 |
| 1652 | 0.07 | 0.03 | 0.00 | 0.10 |
| 1656 | 0.07 | 0.03 | 0.00 | 0.10 |
| 1660 | 0.07 | 0.03 | 0.00 | 0.10 |
| 1664 | 0.07 | 0.03 | 0.00 | 0.10 |
| 1668 | 0.06 | 0.03 | 0.00 | 0.09 |
| 1672 | 0.06 | 0.03 | 0.00 | 0.09 |
| 1676 | 0.06 | 0.03 | 0.00 | 0.09 |
| 1680 | 0.06 | 0.03 | 0.00 | 0.09 |
| 1684 | 0.06 | 0.03 | 0.00 | 0.09 |
| 1688 | 0.06 | 0.03 | 0.00 | 0.09 |
| 1692 | 0.06 | 0.03 | 0.00 | 0.09 |
| 1696 | 0.06 | 0.03 | 0.00 | 0.09 |
| 1700 | 0.06 | 0.03 | 0.00 | 0.09 |
| 1704 | 0.06 | 0.03 | 0.00 | 0.09 |
| 1708 | 0.06 | 0.03 | 0.00 | 0.09 |
| 1712 | 0.06 | 0.03 | 0.00 | 0.09 |
| 1716 | 0.06 | 0.03 | 0.00 | 0.09 |
| 1720 | 0.06 | 0.03 | 0.00 | 0.09 |
| 1724 | 0.05 | 0.03 | 0.00 | 0.08 |
| 1728 | 0.05 | 0.03 | 0.00 | 0.08 |
| 1732 | 0.05 | 0.03 | 0.00 | 0.08 |
| 1736 | 0.05 | 0.03 | 0.00 | 0.08 |

...End

Water Quality Detention Time Calculation

Project: Ansuya Enterprises of Clinton
Location: Clinton Township, NJ
Basin: Number 2

SDI #: 201281
Calculated by: MRC
Date: 10/8/2004

Peak Storage Volume for One Year Water Quality Storm: 7891 cf
Peak Elevation for One Year Water Quality Storm: 231.74 ft
Time to Peak for One Year Water Quality Storm: 888.00 mins
14.80 hrs
Volume left in basin after 90% released: 789.1 cf
determine elevation of 10% storage:
upper elevation: 230.00 ft
upper storage: 822 cf
lower elevation: 229.33 ft
lower storage: 0 cf

therefore, elevation of 10% stored in basin: 229.97 ft
Time to 90% released: 51.96 hrs

Total detention time to release 90% of one year water
quality peak storm storage = **37.16 hrs**

Water Quality Detention Time Calculation

Project: Ansuya Enterprises of Clinton
Location: Clinton Township, NJ
Basin: Number 3

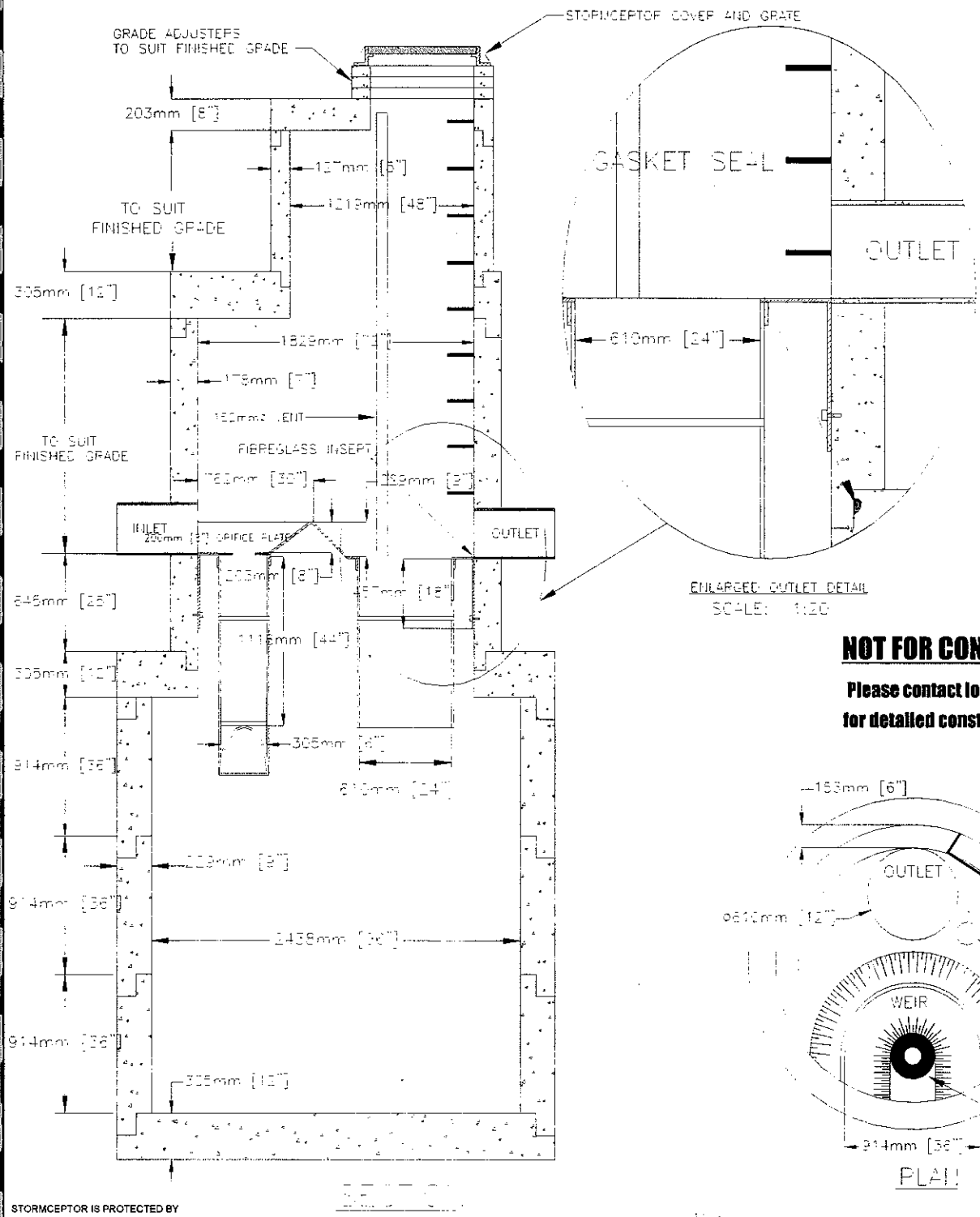
SDI #: 201281
Calculated by: MRC
Date: 10/8/2004

Peak Storage Volume for One Year Water Quality Storm: 6951 cf
Peak Elevation for One Year Water Quality Storm: 222.01 ft
Time to Peak for One Year Water Quality Storm: 814.00 mins
13.57 hrs
Volume left in basin after 90% released: 695.1 cf
determine elevation of 10% storage:
upper elevation: 220.00 ft
upper storage: 703 cf
lower elevation: 219.00 ft
lower storage: 0 cf

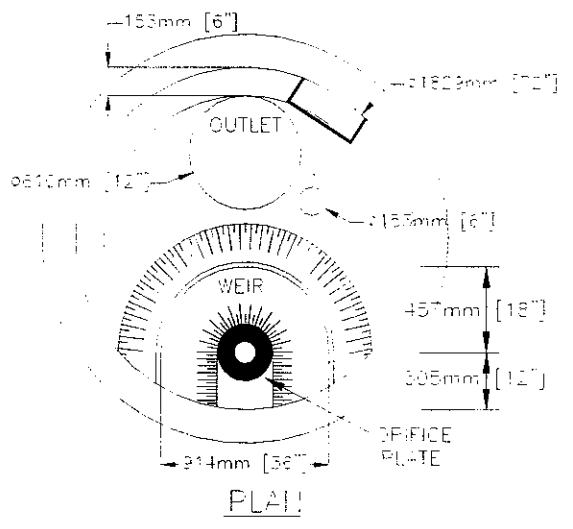
therefore, elevation of 10% stored in basin: 219.99 ft
Time to 90% released: 24.33 hrs

Total detention time to release 90% of one year water
quality peak storm storage = **10.76 hrs**

Basin #2



NOT FOR CONSTRUCTION:
 Please contact local manufacturer
 for detailed construction drawings



STORMCEPTOR IS PROTECTED BY ONE OR MORE OF THE FOLLOWING PATENTS:

Canadian Patent No. 2,009,208
 Canadian Patent No. 2,137,842
 Canadian Patent No. 2,175,277
 Canadian Patent No. 2,180,305
 Canadian Patent No. 2,180,383
 Canadian Patent No. 2,208,338
 U.S. Patent No. 4,985,148
 U.S. Patent No. 5,498,331
 U.S. Patent No. 5,725,780
 U.S. Patent No. 5,753,115
 U.S. Patent No. 5,849,181
 U.S. Patent No. 6,068,765
 U.S. Patent No. 6,371,880
 Australia Patent No. 693,184
 Australia Patent No. 707,133
 Australia Patent No. 729,096
 New Zealand Patent No. 314,848
 China Patent No. ZL 97 1 13074.4
 European Patent Treaty 95 307 996.9

- Notes:
1. Dimensions may vary regionally, due to different manufacturer's.
 2. Access way is offset to allow access to the fiberglass bypass pipe and to allow inspection and maintenance from the surface.
 3. Pipe installation by routing or flexible boots.
 4. Flexible boots may not be suitable for all installations. Please contact your sales representative for further information.
 5. 610 mm [24"] outlet to be used for cleanout access to the treatment chamber.
 6. Safety grates for the 610 mm [24"] outlet are available.

| | | |
|---------------|------------|--------|
| DATE REVISED: | # REVISED: | SCALE: |
| DATE: | D.E.S.: | UNITS: |
| 10/28/98 | C.J.G. | |

STC 5600 PRECAST CONCRETE STORMCEPTOR
 FIBREGLASS DISC DESIGN - 5600 U.S. GALLON CAPACITY

**Stormceptor CD Sizing Program
United States
Version 4.0.0**

Project Details

| | | | |
|-----------------|-------------------------------|------------------|----------------|
| Project | Ansuya Riverbend | Project # | 020128111 |
| Location | Clinton, Hunterdon County, NJ | Company | Schoor DePalma |
| Date | 7/22/04 | Contact | |

| Selected Rainfall Station | |
|---------------------------|-----------------|
| State | New Jersey |
| Name | WATCHUNG |
| ID # | 9271 |
| Elev. (ft) | 260 |
| Latitude | N 40 deg 40 min |
| Longitude | W 74 deg 25 min |

| Particle Size Distribution | | |
|----------------------------|-------------|---------------|
| Diam. (um) | Percent (%) | Spec. Gravity |
| 20 | 20 | 1.30 |
| 60 | 20 | 1.80 |
| 150 | 20 | 2.20 |
| 400 | 20 | 2.65 |
| 2000 | 20 | 2.65 |

| Site Parameters | |
|-----------------------------|------|
| Total Area (ac) | 2.46 |
| Imperviousness (%) | 66 |
| Impervious Area (ac) | 1.62 |

Stormceptor Sizing Table

| Stormceptor Model | % Runoff Treated | % TSS Removal |
|-------------------|------------------|---------------|
| STC 450 | 68 | 62 |
| STC 900 | 83 | 73 |
| STC 1200 | 83 | 74 |
| STC 1800 | 83 | 74 |
| STC 2400 | 90 | 78 |
| STC 3600 | 90 | 80 |
| STC 4800 | 95 | 83 |
| STC 6000 | 95 | 84 |
| STC 7200 | 97 | 86 |
| STC 11000 | 98 | 90 |
| STC 13000 | 98 | 90 |
| STC 16000 | 99 | 92 |

Comments :

Stormceptor CD Sizing Program Version 4.0.0

Country United States

Date 7/22/04

Project Number 020128111
Project Name Ansuya Riverbend
Project Location Clinton, Hunterdon County, NJ
Company Schoor DePalma
Designer

Notes

Rainfall Station WATCHUNG
Rainfall File NJ9271.NDC
Latitude = N 40 deg 40 min
Longitude = W 74 deg 25 min
Elevation = 260. ft
Rainfall Period of Record 1984 to 1996

Site Parameters

Total Drainage Area 2.46 ac
Total Imperviousness (%) 66.00
Overland Flow Width 655. ft
Overland Slope (%) 2.0
Impervious Depression Storage 0.020 in
Pervious Depression Storage 0.200 in
Impervious Mannings n 0.015
Pervious Mannings n 0.250

Infiltration Parameters

Horton Infiltration Used
Initial (Max) Infiltration Rate 2.44 in/h
Final (Min) Infiltration Rate 0.40 in/h
Infiltration Decay Rate (1/sec) 0.00055
Infiltration Regeneration Rate (1/sec) 0.010

Daily evaporation 0.100 in/day

Sediment build-up reduces the storage volume for settling calculations
A maintenance cycle of 12 months was chosen
(The Stormceptor will be cleaned out every 12 months)

TSS Loading Calculations

Buildup / Washoff Loading Chosen

Buildup Washoff allocates more washoff in the rising limb of the hydrograph

Target Event Mean Concentration (mg/l) 125.
Buildup Exponent 0.400
Washoff Exponent 0.200
Availability Factors for Particles \geq 400. μm
Availability = $A + Bi^C$
A = 0.057
B = 0.040
i = rainfall intensity
C = 1.100

Stormwater Particle Size Distribution Table

| Diameter (μm) | Percent (%) | Specific Gravity | Settling Velocity ft/s |
|-------------------------------|----------------|------------------|---------------------------|
| 20.0 | 20.0 | 1.30 | 0.0013 |
| 60.0 | 20.0 | 1.80 | 0.0051 |
| 150.0 | 20.0 | 2.20 | 0.0354 |
| 400.0 | 20.0 | 2.65 | 0.2123 |
| 2000.0 | 20.0 | 2.65 | 0.9417 |

Flocculated settling assumed for particles \leq 20 μm

Rainfall records 1984 to 1999
Total rainfall period 16 years
Total rainfall = 496.3 in
Average annual rainfall = 31.0 in

Rainfall event analysis

2.0 hour inter event time used to determine # of events

| < in | Events | % | Vol in | % |
|--------|--------|------|--------|------|
| 0.25 | 866 | 63.4 | 74. | 14.9 |
| 0.50 | 193 | 14.1 | 69. | 13.8 |
| 0.75 | 97 | 7.1 | 61. | 12.2 |
| 1.00 | 68 | 5.0 | 59. | 11.9 |
| 1.25 | 52 | 3.8 | 58. | 11.6 |
| 1.50 | 29 | 2.1 | 40. | 8.1 |
| 1.75 | 19 | 1.4 | 31. | 6.2 |
| 2.00 | 10 | 0.7 | 19. | 3.8 |
| 2.25 | 12 | 0.9 | 26. | 5.2 |
| 2.50 | 6 | 0.4 | 15. | 2.9 |
| 2.75 | 4 | 0.3 | 10. | 2.1 |
| 3.00 | 1 | 0.1 | 3. | 0.6 |
| 3.25 | 4 | 0.3 | 12. | 2.5 |
| 3.50 | 2 | 0.1 | 7. | 1.4 |
| 3.75 | 1 | 0.1 | 4. | 0.7 |
| 4.00 | 0 | 0.0 | 0. | 0.0 |
| 4.25 | 0 | 0.0 | 0. | 0.0 |
| 4.50 | 1 | 0.1 | 4. | 0.9 |
| 4.75 | 0 | 0.0 | 0. | 0.0 |
| 5.00 | 0 | 0.0 | 0. | 0.0 |
| 5.25 | 0 | 0.0 | 0. | 0.0 |
| 5.50 | 1 | 0.1 | 5. | 1.1 |
| 5.75 | 0 | 0.0 | 0. | 0.0 |
| 6.00 | 0 | 0.0 | 0. | 0.0 |
| 6.25 | 0 | 0.0 | 0. | 0.0 |
| 6.50 | 0 | 0.0 | 0. | 0.0 |
| 6.75 | 0 | 0.0 | 0. | 0.0 |
| 7.00 | 0 | 0.0 | 0. | 0.0 |
| 7.25 | 0 | 0.0 | 0. | 0.0 |
| 7.50 | 0 | 0.0 | 0. | 0.0 |
| 7.75 | 0 | 0.0 | 0. | 0.0 |
| 8.00 | 0 | 0.0 | 0. | 0.0 |
| 8.25 | 0 | 0.0 | 0. | 0.0 |
| > 8.25 | 0 | 0.0 | 0. | 0.0 |

Total rain 496. in
Number of rain events 1366

Rainfall intensity analysis

Average intensity = 0.13 in/h

| < in/h | Number | % | Vol in | % |
|--------|--------|------|--------|------|
| 0.25 | 13549 | 90.9 | 287. | 57.9 |
| 0.50 | 794 | 5.3 | 70. | 14.1 |
| 0.75 | 245 | 1.6 | 37. | 7.5 |
| 1.00 | 148 | 1.0 | 32. | 6.4 |
| 1.25 | 68 | 0.5 | 19. | 3.9 |
| 1.50 | 34 | 0.2 | 12. | 2.3 |
| 1.75 | 16 | 0.1 | 6. | 1.3 |
| 2.00 | 10 | 0.1 | 5. | 1.0 |
| 2.25 | 11 | 0.1 | 6. | 1.2 |
| 2.50 | 5 | 0.0 | 3. | 0.6 |
| 2.75 | 5 | 0.0 | 3. | 0.7 |
| 3.00 | 7 | 0.0 | 5. | 1.0 |
| 3.25 | 4 | 0.0 | 3. | 0.6 |
| 3.50 | 2 | 0.0 | 2. | 0.3 |
| 3.75 | 1 | 0.0 | 1. | 0.2 |
| 4.00 | 0 | 0.0 | 0. | 0.0 |
| 4.25 | 1 | 0.0 | 1. | 0.2 |
| 4.50 | 1 | 0.0 | 1. | 0.2 |
| 4.75 | 1 | 0.0 | 1. | 0.2 |
| 5.00 | 0 | 0.0 | 0. | 0.0 |
| 5.25 | 0 | 0.0 | 0. | 0.0 |
| 5.50 | 0 | 0.0 | 0. | 0.0 |
| 5.75 | 0 | 0.0 | 0. | 0.0 |
| 6.00 | 0 | 0.0 | 0. | 0.0 |
| 6.25 | 0 | 0.0 | 0. | 0.0 |
| 6.50 | 0 | 0.0 | 0. | 0.0 |
| 6.75 | 1 | 0.0 | 2. | 0.3 |
| 7.00 | 0 | 0.0 | 0. | 0.0 |
| 7.25 | 0 | 0.0 | 0. | 0.0 |
| 7.50 | 0 | 0.0 | 0. | 0.0 |
| 7.75 | 0 | 0.0 | 0. | 0.0 |
| 8.00 | 0 | 0.0 | 0. | 0.0 |
| 8.25 | 0 | 0.0 | 0. | 0.0 |
| > 8.25 | 0 | 0.0 | 0. | 0.0 |

Total rainfall = 496.3 in
Total evaporation = 20.4 in
Total infiltration = 166.2 in
% Rainfall as runoff = 63.1 %

Average Event Mean Concentration for TSS (mg/l) 145.4

TSS Removal Simulation Results Table

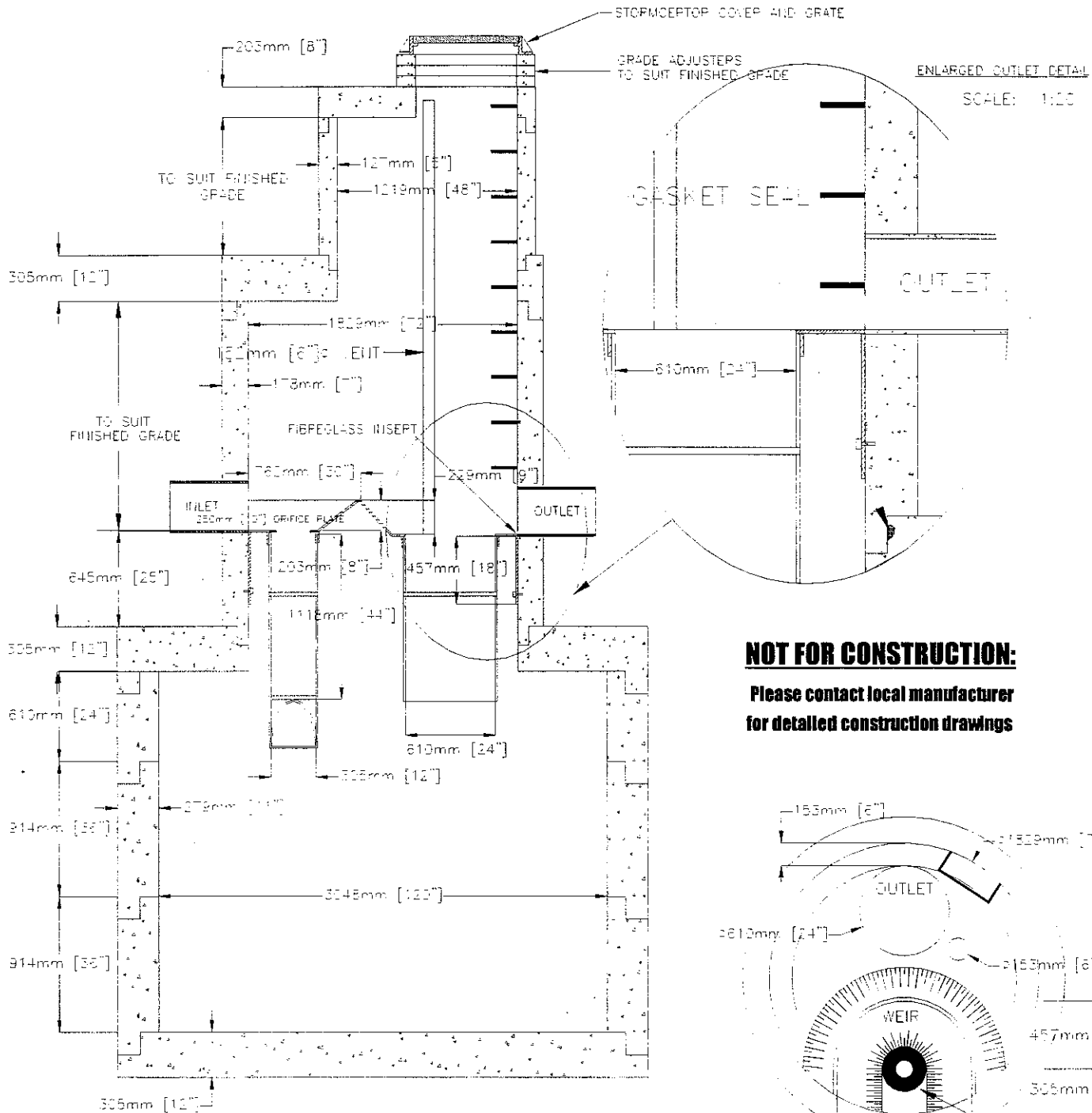
| Stormceptor Model | Treated Q cfs | % Runoff Treated | Tank TSS Removal (%) | Overall TSS Removal (%) |
|-------------------|---------------|------------------|----------------------|-------------------------|
| STC 450 | 0.283 | 68. | 70. | 62. |
| STC 900 | 0.636 | 83. | 77. | 73. |
| STC 1200 | 0.636 | 83. | 78. | 74. |
| STC 1800 | 0.636 | 83. | 79. | 74. |
| STC 2400 | 1.059 | 90. | 80. | 78. |
| STC 3600 | 1.059 | 90. | 82. | 80. |
| STC 4800 | 1.766 | 95. | 84. | 83. |
| STC 6000 | 1.766 | 95. | 85. | 84. |
| STC 7200 | 2.472 | 97. | 87. | 86. |
| STC 11000 | 3.531 | 98. | 90. | 90. |
| STC 13000 | 3.531 | 98. | 90. | 90. |
| STC 16000 | 4.944 | 99. | 92. | 92. |

Hydrology Table - Volume of Runoff Treated vs By-Pass Flow Rate

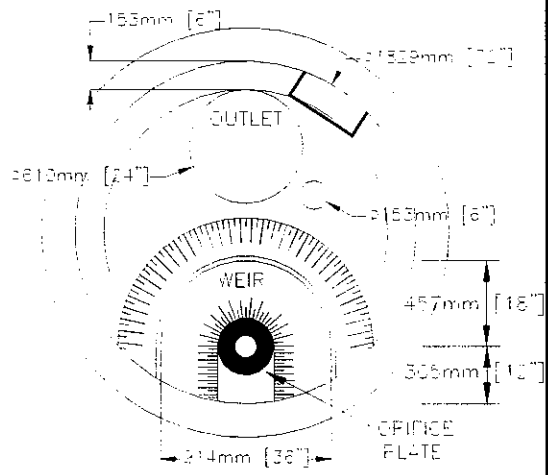
| Treated Q cfs | Treated Vol ft3 | Over Vol ft3 | Tot Vol | % Treated |
|---------------|-----------------|--------------|----------|-----------|
| 0.035 | 576525. | 2218454. | 2795042. | 20.6 |
| 0.141 | 1448154. | 1346828. | 2795042. | 51.8 |
| 0.318 | 1979252. | 815741. | 2795042. | 70.8 |
| 0.565 | 2260416. | 534569. | 2795042. | 80.9 |
| 0.883 | 2438563. | 356455. | 2795042. | 87.2 |
| 1.271 | 2561130. | 233894. | 2795042. | 91.6 |
| 1.730 | 2640488. | 154555. | 2795042. | 94.5 |
| 2.260 | 2689864. | 105180. | 2795042. | 96.2 |
| 2.860 | 2722158. | 72888. | 2795042. | 97.4 |
| 3.531 | 2745928. | 49119. | 2795042. | 98.2 |
| 4.273 | 2762379. | 32666. | 2795042. | 98.8 |
| 5.085 | 2774068. | 20980. | 2795042. | 99.2 |
| 5.968 | 2780855. | 14192. | 2795042. | 99.5 |
| 6.922 | 2785188. | 9856. | 2795042. | 99.6 |
| 7.946 | 2788332. | 6711. | 2795042. | 99.8 |
| 9.041 | 2790478. | 4566. | 2795042. | 99.8 |
| 10.206 | 2792044. | 2999. | 2795042. | 99.9 |
| 11.442 | 2793211. | 1831. | 2795042. | 99.9 |
| 12.749 | 2793995. | 1047. | 2795042. | 100.0 |
| 14.126 | 2794747. | 295. | 2795042. | 100.0 |
| 15.574 | 2795042. | 0. | 2795042. | 100.0 |
| 17.092 | 2795042. | 0. | 2795042. | 100.0 |
| 18.681 | 2795042. | 0. | 2795042. | 100.0 |
| 20.341 | 2795042. | 0. | 2795042. | 100.0 |
| 22.072 | 2795042. | 0. | 2795042. | 100.0 |
| 23.873 | 2795042. | 0. | 2795042. | 100.0 |
| 25.744 | 2795042. | 0. | 2795042. | 100.0 |
| 27.687 | 2795042. | 0. | 2795042. | 100.0 |
| 29.700 | 2795042. | 0. | 2795042. | 100.0 |
| 31.783 | 2795042. | 0. | 2795042. | 100.0 |

End of Simulation

Basin #3



NOT FOR CONSTRUCTION:
 Please contact local manufacturer
 for detailed construction drawings



STORMCEPTOR IS PROTECTED BY ONE OR MORE OF THE FOLLOWING PATENTS:

- Canadian Patent No. 2,009,208
- Canadian Patent No. 2,137,942
- Canadian Patent No. 2,175,277
- Canadian Patent No. 2,180,305
- Canadian Patent No. 2,180,383
- Canadian Patent No. 2,206,338
- U.S. Patent No. 4,985,148
- U.S. Patent No. 5,498,331
- U.S. Patent No. 5,725,760
- U.S. Patent No. 5,753,115
- U.S. Patent No. 5,849,181
- U.S. Patent No. 6,068,765
- U.S. Patent No. 6,371,690
- Australia Patent No. 693,164
- Australia Patent No. 707,133
- Australia Patent No. 729,096
- New Zealand Patent No. 314,646
- China Patent No. ZL 97 1 13074.4
- European Patent Treaty 95 307 996.9

- Notes:
1. Dimensions may vary regionally, due to different manufacturer's.
 2. Access via is offset to allow access to the fiberglass bypass slab and to allow inspection and maintenance from the surface.
 3. Pipe installation to, grouting or flexible boots.
 4. Flexible boots may not be suitable for all installations. Please contact your sales representative for further information.
 5. 610 mm [24"] outlet to be used for cleanout access to the treatment chamber.
 6. Safety grates for the 610 mm [24"] outlet are available.

| | | |
|-------------|--------------|--------|
| DATE REC'D: | # REVISIONS: | SCALE: |
| DATE: | D.E.I.: | UNITS: |
| 10 28 98 | 1 | 1:40 |

STC 4800 PRECAST CONCRETE STORMCEPTOR
 FIBREGLASS D/S DESIGN - 4800 U.S. GALLON CAPACITY

Stormceptor CD Sizing Program
United States
Version 4.0.0

Project Details

| | | | |
|----------|-------------------------------|-----------|----------------|
| Project | Ansuya Riverbend | Project # | 020128111 |
| Location | Clinton, Hunterdon County, NJ | Company | Schoor DePalma |
| Date | 7/22/04 | Contact | |

| Selected Rainfall Station | |
|---------------------------|-----------------|
| State | New Jersey |
| Name | WATCHUNG |
| ID # | 9271 |
| Elev. (ft) | 260 |
| Latitude | N 40 deg 40 min |
| Longitude | W 74 deg 25 min |

| Particle Size Distribution | | |
|----------------------------|-------------|---------------|
| Diam. (um) | Percent (%) | Spec. Gravity |
| 20 | 20 | 1.30 |
| 60 | 20 | 1.80 |
| 150 | 20 | 2.20 |
| 400 | 20 | 2.65 |
| 2000 | 20 | 2.65 |

| Site Parameters | |
|----------------------|------|
| Total Area (ac) | 3.46 |
| Imperviousness (%) | 69 |
| Impervious Area (ac) | 2.39 |

Stormceptor Sizing Table

| Stormceptor Model | % Runoff Treated | % TSS Removal |
|-------------------|------------------|---------------|
| STC 450 | 60 | 56 |
| STC 900 | 77 | 68 |
| STC 1200 | 77 | 70 |
| STC 1800 | 77 | 70 |
| STC 2400 | 85 | 74 |
| STC 3600 | 85 | 75 |
| STC 4800 | 91 | 80 |
| STC 6000 | 91 | 80 |
| STC 7200 | 94 | 83 |
| STC 11000 | 97 | 87 |
| STC 13000 | 97 | 87 |
| STC 16000 | 98 | 90 |

Comments :

Stormceptor CD Sizing Program Version 4.0.0

Country United States

Date 7/22/04

Project Number 020128111
Project Name Ansuya Riverbend
Project Location Clinton, Hunterdon County, NJ
Company Schoor DePalma
Designer

Notes

Rainfall Station WATCHUNG
Rainfall File NJ9271.NDC
Latitude = N 40 deg 40 min
Longitude = W 74 deg 25 min
Elevation = 260. ft
Rainfall Period of Record 1984 to 1996

Site Parameters

Total Drainage Area 3.46 ac
Total Imperviousness (%) 69.00
Overland Flow Width 776. ft
Overland Slope (%) 2.0
Impervious Depression Storage 0.020 in
Pervious Depression Storage 0.200 in
Impervious Mannings n 0.015
Pervious Mannings n 0.250

Infiltration Parameters

Horton Infiltration Used
Initial (Max) Infiltration Rate 2.44 in/h
Final (Min) Infiltration Rate 0.40 in/h
Infiltration Decay Rate (1/sec) 0.00055
Infiltration Regeneration Rate (1/sec) 0.010

Daily evaporation 0.100 in/day

Sediment build-up reduces the storage volume for settling calculations
A maintenance cycle of 12 months was chosen
(The Stormceptor will be cleaned out every 12 months)

TSS Loading Calculations

Buildup / Washoff Loading Chosen

Buildup Washoff allocates more washoff in the rising limb of the hydrograph

Target Event Mean Concentration (mg/l) 125.
Buildup Exponent 0.400
Washoff Exponent 0.200
Availability Factors for Particles \geq 400. μ m
Availability = $A + Bi^C$
A = 0.057
B = 0.040
i = rainfall intensity
C = 1.100

Stormwater Particle Size Distribution Table

| Diameter (μ m) | Percent (%) | Specific Gravity | Settling Velocity ft/s |
|------------------------|----------------|------------------|---------------------------|
| 20.0 | 20.0 | 1.30 | 0.0013 |
| 60.0 | 20.0 | 1.80 | 0.0051 |
| 150.0 | 20.0 | 2.20 | 0.0354 |
| 400.0 | 20.0 | 2.65 | 0.2123 |
| 2000.0 | 20.0 | 2.65 | 0.9417 |

Flocculated settling assumed for particles \leq 20 μ m

Rainfall records 1984 to 1999
Total rainfall period 16 years
Total rainfall = 496.3 in
Average annual rainfall = 31.0 in

Rainfall event analysis

2.0 hour inter event time used to determine # of events

| < in | Events | % | Vol in | % |
|--------|--------|------|--------|------|
| 0.25 | 866 | 63.4 | 74. | 14.9 |
| 0.50 | 193 | 14.1 | 69. | 13.8 |
| 0.75 | 97 | 7.1 | 61. | 12.2 |
| 1.00 | 68 | 5.0 | 59. | 11.9 |
| 1.25 | 52 | 3.8 | 58. | 11.6 |
| 1.50 | 29 | 2.1 | 40. | 8.1 |
| 1.75 | 19 | 1.4 | 31. | 6.2 |
| 2.00 | 10 | 0.7 | 19. | 3.8 |
| 2.25 | 12 | 0.9 | 26. | 5.2 |
| 2.50 | 6 | 0.4 | 15. | 2.9 |
| 2.75 | 4 | 0.3 | 10. | 2.1 |
| 3.00 | 1 | 0.1 | 3. | 0.6 |
| 3.25 | 4 | 0.3 | 12. | 2.5 |
| 3.50 | 2 | 0.1 | 7. | 1.4 |
| 3.75 | 1 | 0.1 | 4. | 0.7 |
| 4.00 | 0 | 0.0 | 0. | 0.0 |
| 4.25 | 0 | 0.0 | 0. | 0.0 |
| 4.50 | 1 | 0.1 | 4. | 0.9 |
| 4.75 | 0 | 0.0 | 0. | 0.0 |
| 5.00 | 0 | 0.0 | 0. | 0.0 |
| 5.25 | 0 | 0.0 | 0. | 0.0 |
| 5.50 | 1 | 0.1 | 5. | 1.1 |
| 5.75 | 0 | 0.0 | 0. | 0.0 |
| 6.00 | 0 | 0.0 | 0. | 0.0 |
| 6.25 | 0 | 0.0 | 0. | 0.0 |
| 6.50 | 0 | 0.0 | 0. | 0.0 |
| 6.75 | 0 | 0.0 | 0. | 0.0 |
| 7.00 | 0 | 0.0 | 0. | 0.0 |
| 7.25 | 0 | 0.0 | 0. | 0.0 |
| 7.50 | 0 | 0.0 | 0. | 0.0 |
| 7.75 | 0 | 0.0 | 0. | 0.0 |
| 8.00 | 0 | 0.0 | 0. | 0.0 |
| 8.25 | 0 | 0.0 | 0. | 0.0 |
| > 8.25 | 0 | 0.0 | 0. | 0.0 |

Total rain 496. in
 Number of rain events 1366

Rainfall intensity analysis

Average intensity = 0.13 in/h

| < in/h | Number | % | Vol in | % |
|--------|--------|------|--------|------|
| 0.25 | 13549 | 90.9 | 287. | 57.9 |
| 0.50 | 794 | 5.3 | 70. | 14.1 |
| 0.75 | 245 | 1.6 | 37. | 7.5 |
| 1.00 | 148 | 1.0 | 32. | 6.4 |
| 1.25 | 68 | 0.5 | 19. | 3.9 |
| 1.50 | 34 | 0.2 | 12. | 2.3 |
| 1.75 | 16 | 0.1 | 6. | 1.3 |
| 2.00 | 10 | 0.1 | 5. | 1.0 |
| 2.25 | 11 | 0.1 | 6. | 1.2 |
| 2.50 | 5 | 0.0 | 3. | 0.6 |
| 2.75 | 5 | 0.0 | 3. | 0.7 |
| 3.00 | 7 | 0.0 | 5. | 1.0 |
| 3.25 | 4 | 0.0 | 3. | 0.6 |
| 3.50 | 2 | 0.0 | 2. | 0.3 |
| 3.75 | 1 | 0.0 | 1. | 0.2 |
| 4.00 | 0 | 0.0 | 0. | 0.0 |
| 4.25 | 1 | 0.0 | 1. | 0.2 |
| 4.50 | 1 | 0.0 | 1. | 0.2 |
| 4.75 | 1 | 0.0 | 1. | 0.2 |
| 5.00 | 0 | 0.0 | 0. | 0.0 |
| 5.25 | 0 | 0.0 | 0. | 0.0 |
| 5.50 | 0 | 0.0 | 0. | 0.0 |
| 5.75 | 0 | 0.0 | 0. | 0.0 |
| 6.00 | 0 | 0.0 | 0. | 0.0 |
| 6.25 | 0 | 0.0 | 0. | 0.0 |
| 6.50 | 0 | 0.0 | 0. | 0.0 |
| 6.75 | 1 | 0.0 | 2. | 0.3 |
| 7.00 | 0 | 0.0 | 0. | 0.0 |
| 7.25 | 0 | 0.0 | 0. | 0.0 |
| 7.50 | 0 | 0.0 | 0. | 0.0 |
| 7.75 | 0 | 0.0 | 0. | 0.0 |
| 8.00 | 0 | 0.0 | 0. | 0.0 |
| 8.25 | 0 | 0.0 | 0. | 0.0 |
| > 8.25 | 0 | 0.0 | 0. | 0.0 |

Total rainfall = 496.3 in
Total evaporation = 21.7 in
Total infiltration = 151.6 in
% Rainfall as runoff = 65.7 %

Average Event Mean Concentration for TSS (mg/l) 143.0

TSS Removal Simulation Results Table

| Stormceptor Model | Treated Q cfs | % Runoff Treated | Tank TSS Removal (%) | Overall TSS Removal (%) |
|-------------------|---------------|------------------|----------------------|-------------------------|
| STC 450 | 0.283 | 60. | 66. | 56. |
| STC 900 | 0.636 | 77. | 74. | 68. |
| STC 1200 | 0.636 | 77. | 76. | 70. |
| STC 1800 | 0.636 | 77. | 76. | 70. |
| STC 2400 | 1.059 | 85. | 78. | 74. |
| STC 3600 | 1.059 | 85. | 79. | 75. |
| STC 4800 | 1.766 | 91. | 82. | 80. |
| STC 6000 | 1.766 | 91. | 82. | 80. |
| STC 7200 | 2.472 | 94. | 84. | 83. |
| STC 11000 | 3.531 | 97. | 87. | 87. |
| STC 13000 | 3.531 | 97. | 87. | 87. |
| STC 16000 | 4.944 | 98. | 90. | 90. |

Hydrology Table - Volume of Runoff Treated vs By-Pass Flow Rate

| Treated Q cfs | Treated Vol ft3 | Over Vol ft3 | Tot Vol | % Treated |
|---------------|-----------------|--------------|----------|-----------|
| 0.035 | 641292. | 3455752. | 4096924. | 15.7 |
| 0.141 | 1733247. | 2363714. | 4096924. | 42.3 |
| 0.318 | 2574589. | 1522427. | 4096924. | 62.8 |
| 0.565 | 3074358. | 1022574. | 4096924. | 75.0 |
| 0.883 | 3371870. | 725136. | 4096924. | 82.3 |
| 1.271 | 3580573. | 516365. | 4096924. | 87.4 |
| 1.730 | 3733515. | 363441. | 4096924. | 91.1 |
| 2.260 | 3840453. | 256469. | 4096924. | 93.7 |
| 2.860 | 3913652. | 183282. | 4096924. | 95.5 |
| 3.531 | 3962918. | 133996. | 4096924. | 96.7 |
| 4.273 | 3998607. | 98321. | 4096924. | 97.6 |
| 5.085 | 4026777. | 70146. | 4096924. | 98.3 |
| 5.968 | 4046854. | 50068. | 4096924. | 98.8 |
| 6.922 | 4062742. | 34181. | 4096924. | 99.2 |
| 7.946 | 4072970. | 23954. | 4096924. | 99.4 |
| 9.041 | 4079636. | 17289. | 4096924. | 99.6 |
| 10.206 | 4084216. | 12708. | 4096924. | 99.7 |
| 11.442 | 4087774. | 9149. | 4096924. | 99.8 |
| 12.749 | 4090344. | 6580. | 4096924. | 99.8 |
| 14.126 | 4092303. | 4621. | 4096924. | 99.9 |
| 15.574 | 4093816. | 3108. | 4096924. | 99.9 |
| 17.092 | 4094886. | 2038. | 4096924. | 100.0 |
| 18.681 | 4095840. | 1084. | 4096924. | 100.0 |
| 20.341 | 4096634. | 289. | 4096924. | 100.0 |
| 22.072 | 4096924. | 0. | 4096924. | 100.0 |
| 23.873 | 4096924. | 0. | 4096924. | 100.0 |
| 25.744 | 4096924. | 0. | 4096924. | 100.0 |
| 27.687 | 4096924. | 0. | 4096924. | 100.0 |
| 29.700 | 4096924. | 0. | 4096924. | 100.0 |
| 31.783 | 4096924. | 0. | 4096924. | 100.0 |

End of Simulation



Stormceptor®

Owner's Manual

April 2000

*The Stormceptor® System is protected by
one or more of the following patents:*

Canadian Patent No. 2,009,208

Canadian Patent No. 2,137,942

Canadian Patent No. 2,175,277

Canadian Patent No. 2,180,305

Canadian Patent No. 2,206,338

U.S. Patent No. 4,985,148

U.S. Patent No. 5,498,331

U.S. Patent No. 5,725,760

U.S. Patent No. 5,753,115

U.S. Patent No. 5,849,181

U.S. Patent No. 6,068,765

Australia 693,164

Australia 707,133

New Zealand 314,646

European Patent Treaty 95 307 996.9

The Stormceptor System for

Stormwater Quality Improvement

Congratulations!

Your selection of a Stormceptor® System means that you have chosen the most recognized and efficient stormwater oil/sediment separator available. Stormceptor is a pollution control device that protects our lakes, rivers and streams from the harmful effects of non-point source pollution. Please address any questions or concerns regarding the Stormceptor Systems to Stormceptor Canada Inc at 1-800-565-4801 or visit our website at www.stormceptor.com.

What is a Stormceptor?

Stormceptor is a patented water quality structure that takes the place of a conventional manhole with in a storm drain system. Stormceptor removes free oil (TPH) and suspended solids (TSS) from stormwater preventing spills and non-point source pollution from entering downstream lakes and rivers. Key benefits of a Stormceptor include:

- Capable of removing 50% to 80% of the total sediment load when properly applied as a source control for small areas
- Removes free oil from stormwater during low flow conditions
- Will not scour or re-suspend trapped pollutants
- Excellent spill control device for commercial and industrial developments
- Easy to maintain (vacuum truck)
- STORMCEPTOR *clearly* marked on the cover (excluding inlet designs)
- Engineered and continually tested
- Vertical orientation therefore resulting in a smaller footprint

Please Maintain Your Stormceptor

To ensure long-term environmental protection through continual performance, **Stormceptor must be maintained**. The need for maintenance is determined through inspection of the Stormceptor. Procedures for inspection are provided in this document. Maintenance of the Stormceptor is performed from the surface via vacuum truck. . If you require a list of contacts for cleaning your Stormceptor please call one of our Stormceptor offices or your nearest Stormceptor affiliate (affiliates listed in Appendix 1).

How does Stormceptor® Work?

Stormceptor can be divided into two components:

- Lower treatment chamber
- Upper by-pass chamber

Stormwater flows into the by-pass chamber via the storm drain pipe. Low flows are diverted into the treatment chamber by a weir and drop pipe arrangement. The treatment chamber is always full of water. Water flows up through the outlet pipe based on the head at the inlet weir, and is discharged back into the by-pass chamber downstream of the weir. The downstream section of the by-pass chamber is connected to the outlet storm drainpipe.

Free oils and other liquids lighter than water will rise in the treatment chamber and become entrapped beneath the fiberglass insert since the outlet pipe is submerged. Sediment will settle to the bottom of the chamber by gravity. The circular design of the treatment chamber is critical to prevent turbulent eddy currents and to promote settling.

During high flow conditions, stormwater in the by-pass chamber will flow overtop of the weir and be conveyed to the outlet storm drain directly. Water that overflows the weir creates a backwater effect on the outlet pipe (head stabilization between the inlet drop pipe and outlet riser pipe) ensuring that excessive flow will not be forced into the treatment chamber, which could scour or re-suspend the settled material. The by-pass is an integral part of Stormceptor since other oil/grit separators have been noted to scour during high flow conditions (Schueler and Shepp, 1993).

Stormceptor Models and Identification

Stormceptor is available in both concrete and fiberglass. There are currently nine different sizes available. A concrete Stormceptor is denoted by STC (e.g. STC6000) preceding the model number. A fiberglass Stormceptor is denoted by STA (e.g. STA6000) preceding the model number.

In the concrete Stormceptor, a fiberglass insert separates the treatment chamber from the by-pass chamber. There is three insert designs: the "spool", the "disc" and the "inlet". The different insert designs are illustrated in Figures 1, 2 and 3. These designs are easily distinguishable from the surface once the cover has been removed. In the "spool" design you will see one large 914 mm (36") opening in the center of the insert with two 200 mm (8") inspection ports located either vertically on the sides of the 914 mm (36") opening or horizontally on either side of the opening. There are three versions of the in-line disc insert: "single inlet/outlet", "multiple inlet" and "submerged". In the "disc" design you will be able to see the inlet pipe, the drop pipe opening to the lower chamber, the weir, a 150 mm (6") oil inspection/cleanout pipe, a large 610 mm (24") riser pipe-opening offset on the outlet side of the structure, and the outlet pipe from the unit. The weir will be around the 610 mm (24") outlet pipe on the "multiple inlet" disc insert. The "submerged" disc insert has a higher weir and a second inlet drop pipe. In the "inlet" design you will be

able to see the 305 mm (12") inlet drop pipe and 100 mm (4") outlet riser pipe as well as a central 100mm [4"] oil inspection/cleanout port.

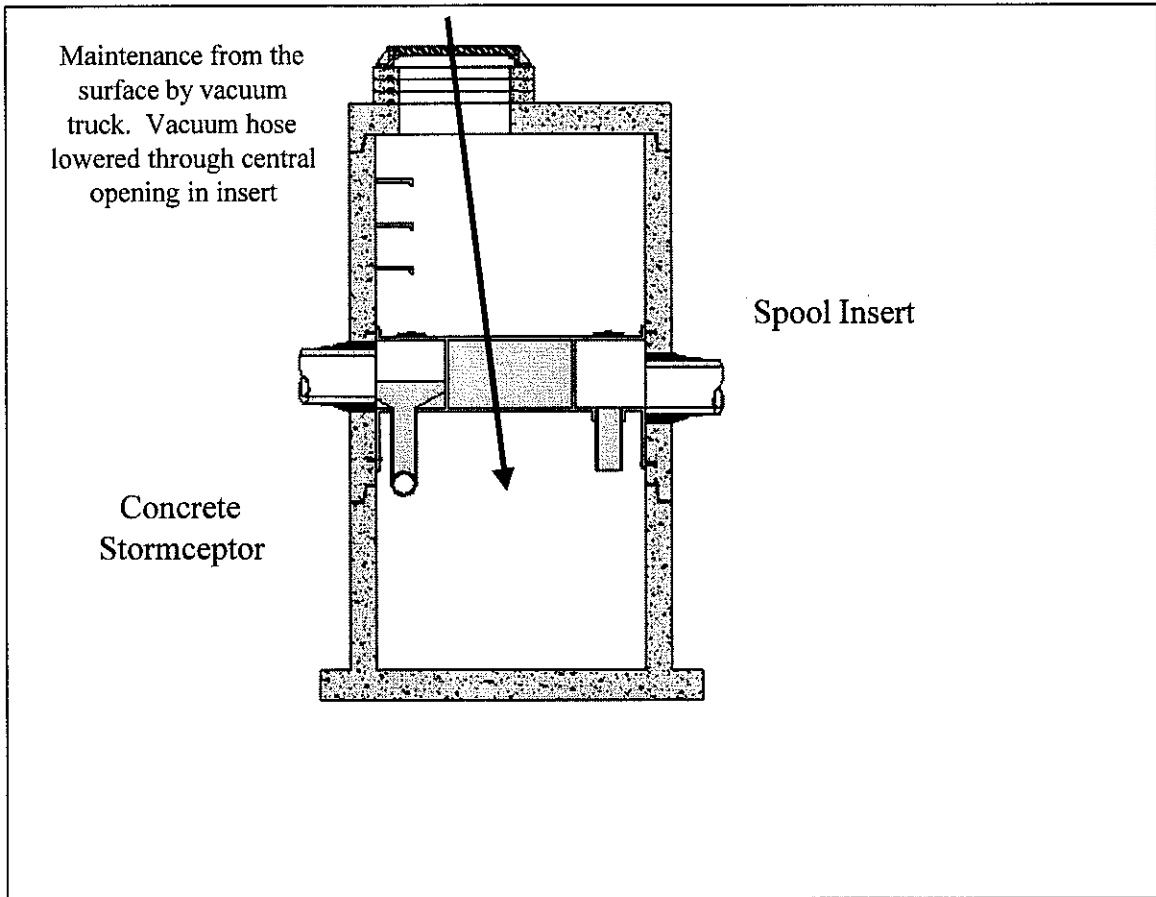


Figure 1 "Spool" Insert Concrete Stormceptor®

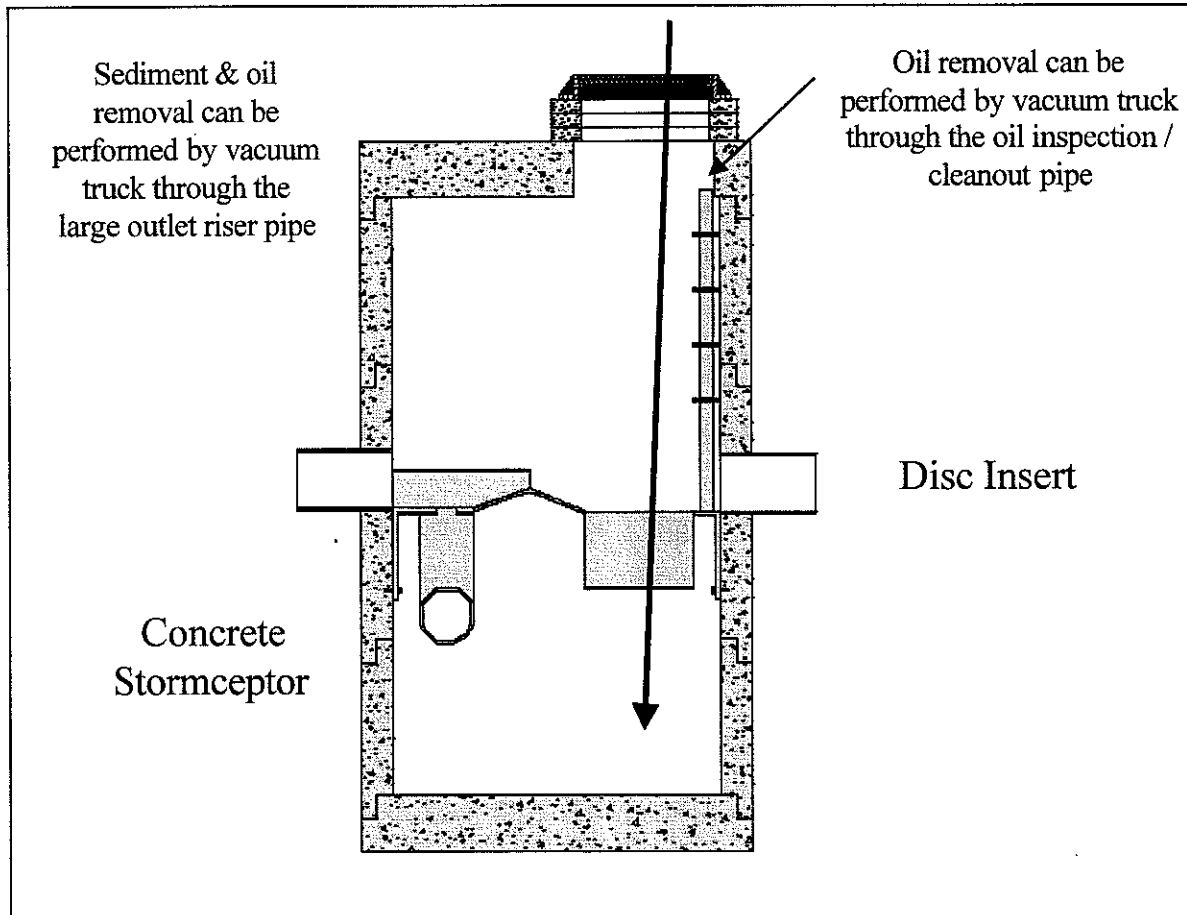


Figure 2 Single Inlet/Outlet "Disc" Insert Concrete Stormceptor®

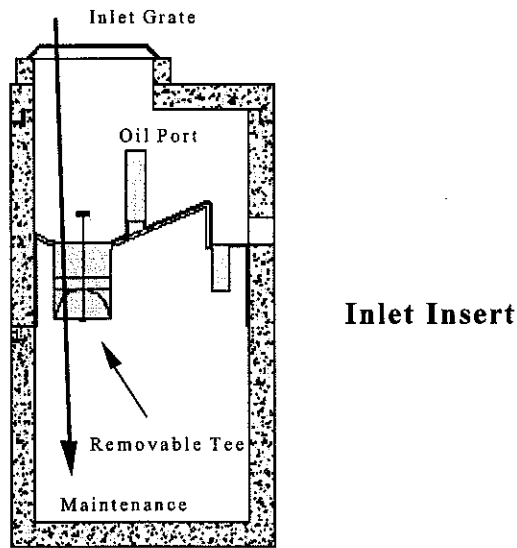


Figure 3 STC 300/450 Inlet Insert

Sizes/Models

Dimensions of the fiberglass and concrete Stormceptor® units are provided in Table 1. Values of invert to grade are provided later in this document for your site. The total depth for cleaning will be the sum of the depth from invert to grade and invert to the bottom of the unit.

| Table 1. Stormceptor Dimensions * | | | |
|--|------------|---|---|
| Model (Metric) | Model (US) | Pipe Invert to Bottom of STA Stormceptor m (in.) | Pipe Invert to Bottom of STC Stormceptor m (in.) |
| 300 | 450 | 1.6 (64) | 1.7 (68) |
| 750 | 900 | 1.6 (64) | 1.9 (74) |
| 1000 | 1200 | 2.1 (81) | 2.2 (86) |
| 1500 | 1800 | 2.9 (115) | 3.1 (122) |
| 2000 | 2400 | 2.3 (89) | 3.1 (122) |
| 3000 | 3600 | 3.2 (127) | 4.0 (158) |
| 4000 | 4800 | 2.9 (113) | 3.7 (146) |
| 5000 | 6000 | 3.5 (138) | 4.3 (170) |
| 6000 | 7200 | 3.3 (128) | 4.0 (158) |

*** Depths are approximate**

The capacities of the different Stormceptor units are provided in Table 2.

| Model (Metric) | Model (US) | Sediment Capacity L (US gal) | Oil Capacity L (US gal) | Total Holding Capacity L (US gal) |
|----------------|------------|------------------------------|-------------------------|-----------------------------------|
| 300 | 450 | 1275 (335) | 325 (85) | 1775 (470) |
| 750 | 900 | 2460 (565) | 915 (280) | 4325 (950) |
| 1000 | 1200 | 3260 (845) | 915 (280) | 5125 (1230) |
| 1500 | 1800 | 5660 (1445) | 915 (280) | 7525 (1830) |
| 2000 | 2400 | 6150 (1345) | 2945 (880) | 10925 (2495) |
| 3000 | 3600 | 10415 (2600) | 2945 (880) | 15195 (3750) |
| 4000 | 4800 | 14060 (3475) | 3490 (1025) | 20180 (5020) |
| 5000 | 6000 | 18510 (4550) | 3490 (1025) | 24635 (6095) |
| 6000 | 7200 | 23445 (5425) | 4150 (1100) | 31210 (7415) |

Identification

Even if you do not have plans of your storm drain system you will be able to easily identify where the inline Stormceptor unit(s) (spool or disc insert) are since the name STORMCEPTOR is clearly embossed on the cover. You will be able to determine the location of "inlet" Stormceptor units with horizontal catch basin inlets by looking down the grate since the insert will be visible. The name Stormceptor is not embossed on the inlet models due to the variability of inlet grates used/approved across North America. Once you have found the unit, you may still be uncertain which model number it is. Comparing the measured depth from the water level (bottom of insert) to the bottom of the tank with Table 1 should help determine the size of the unit.

Starting in 1996, a metal serial number tag has been affixed to the inside of the unit. The serial number has the model number written on it. If the unit does not have a serial number, or if there is any uncertainty regarding the size of the interceptor using depth measurements, please contact Stormceptor at 1 800 565-4801 and we will help you determine the size of a particular unit.

What is the Maintenance Procedure?

Maintenance of Stormceptor is performed using vacuum trucks. No entry into the unit is required for maintenance of the spool insert, inlet insert or the smaller disc inserts. Entry to the level of the disc insert may be required for servicing the larger disc insert models. **DO NOT ENTER THE STORMCEPTOR CHAMBER** unless you have the proper equipment, have been trained and are qualified to enter a confined space, as identified by local Occupational Safety and Health Regulations (*e.g.* Canada Occupational Safety and Health Regulations – SOR/86-304). Without the proper equipment and training, entry into confined spaces can result in serious bodily harm and potentially death. Consult local, provincial, and/or state regulations to determine the requirements for confined space entry. Be aware that the insert may be slippery. In addition, be aware that some units do not have a safety grate to cover the outlet riser pipe that leads to the submerged, lower treatment chamber.

The Vacuum Service Industry is a well-established sector of the service industry that cleans underground tanks, sewers and catch basins. Costs to clean a Stormceptor® will vary based on the size of unit and transportation distances.

The depth of oil in the interceptor can be determined by inserting a dipstick tube in the 150 mm (6") oil inspection/cleanout pipe ("disc" design), or in the 914 mm (36") central access way ("spool" design), or in the 100 mm (4") cleanout pipe ("inlet" design).

Similarly, the depth of sediment can be measured from the surface without entry into the Stormceptor via a dipstick tube equipped with a ball valve (Sludge Judge). This tube would be inserted in the central opening ("spool" design) or in the 610 mm (24") opening ("disc" design), or in the 100 mm (4") cleanout pipe ("inlet" design). Maintenance should be performed once the sediment depth exceeds the guideline values provided in Table 3.

For the "spool" design Stormceptor maintenance is performed through the large central 914 mm (36") diameter opening for both the oil and the sediment. In the "disc" design, oil is removed through the 150 mm (6") oil inspection/cleanout pipe and sediment is removed through the 610 mm (24") diameter outlet riser pipe. Alternatively, oil could be removed from the 610 mm (24") opening if water is removed from the lower chamber to lower the oil level to the level of the drop pipes. For the "inlet" design, maintenance is performed through the 305mm (12") inlet drop pipe for the sediment, and oil can be removed from the 100 mm (4") oil/inspection cleanout pipe.

We recommend the following procedure to clean out the Stormceptor:

1. Check for oil (using a dipstick tube)
2. Remove any oil separately using a small portable pump
3. Decant the water from the unit to the sanitary sewer using a portable pump (**prior approval is required from the sewer authority/municipality**)
4. Remove the sludge from the bottom of the unit using a vacuum truck
5. Re-fill the Stormceptor with water where required by the local jurisdiction

How Often Is Maintenance Required?

Generally, annual maintenance is recommended but the required maintenance frequency will vary with the amount of pollution on your site (number of hydrocarbon spills, amount of sediment, etc.). It is recommended that the frequency of maintenance be increased or reduced based on local conditions. If the sediment load is high, maintenance may be required semi-annually. Conversely once the site has stabilized, maintenance may be required less frequently. Maintenance should be performed immediately after an oil spill or once the sediment depth in Stormceptor reaches the value specified in Table 3 based on the unit size.

In the "disc" design and "inlet" design, any potential obstructions at the inlet can be observed from the surface. The "disc" insert has been designed as a platform to facilitate maintenance of the Stormceptor and the storm drain system.

| Model (Metric) | Model (US) | Sediment Depth mm (in.) |
|----------------|------------|-------------------------|
| 300 | 450 | 200 (8) |
| 750 | 900 | 200 (8) |
| 1000 | 1200 | 250 (10) |
| 1500 | 1800 | 375 (15) |
| 2000 | 2400 | 300 (12) |
| 3000 | 3600 | 425 (17) |
| 4000 | 4800 | 375 (15) |
| 5000 | 6000 | 450 (18) |
| 6000 | 7200 | 375 (15) |

What Should I do in the Event of an Oil Spill?

Stormceptor® is often implemented in areas where the potential for spills is great. Stormceptor should be cleaned immediately after a spill occurs by a licensed liquid waste hauler. You should also notify the appropriate regulatory agencies as required in the event of a spill.

Disposal of the Trapped Material Removed from Stormceptor

The requirements for the disposal of material from Stormceptor are similar to that of any other Best Management Practices (BMP). Local guidelines should be consulted prior to disposal of the separator contents.

In most areas the sediment, once dewatered, can be disposed of in a sanitary landfill. It is not anticipated that the sediment would be classified as hazardous waste. In some areas, mixing the water with the sediment will create a slurry that can be discharged into a trunk sanitary sewer. In all disposal options, approval from the disposal facility operator/agency is required. Petroleum waste products collected in Stormceptor (oil/chemical/fuel spills) should be removed by a licensed waste management company.

What if I see an oil rainbow or sheen at the Stormceptor outlet?

With a steady influx of water with high concentrations of oil, a sheen may be noticeable at the Stormceptor outlet. This may occur because a rainbow or sheen can be seen at very small oil concentrations (< 10 ppm). Stormceptor will remove over 95% of all free oil and the appearance of a sheen at the outlet with high influent oil concentrations does not mean that the unit is not working to this level of removal. In addition, if the influent oil is emulsified, the Stormceptor will not be able to remove it. The Stormceptor is designed for free oil removal and not emulsified or dissolved oil conditions.

Appendix 1
Stormceptor® Affiliates

Stormceptor® Affiliates

CANADA

FIBERGLASS

Stormceptor Canada Inc.

416-626-0840 / 1-800-565-4801

Todd Neff

CONCRETE

Lafarge Canada Inc.

403-292-9502 / 1-888-422-4022

AB, MB, NW, ON, SK

604-502-5236

Chris Hughes

BC

Centennial Concrete Pipe & Products Inc.

519-622-7574 / 1-888-888-3222

Brian Lee

ON

Lécuyer et Fils Ltée.

450-454-3928

Réjean Tremblay

PQ

Strescon Limited

902-494-7400

Andrew LeVatte

NS

506-633-8877

Gary Bennett

NB, PE, NF

UNITED STATES

CSR Hydro Conduit

1-800-909-7763 CSR National Stormceptor® Information

AK, AL, AR, AZ, CA, CT
DC, DE, FL, GA, HI, s. IL, IN,
KS, KY, LA, MA, MD, ME,
MI, MO, MS, NC, NE, NH,
NM, NV, OK, OR, RI, SC, TN,
TX, VA, VT, WA

The Cretex Companies

612-441-2121

Brad Fossum

MN, IA, n. IL WI

Camtek Construction Products

724-327-3400

Andy Virostek

NY, NJ, OH, PA, WV

Carder Concrete Products

303-791-1600

Don Grzesiek

CO

Wyoming Concrete Products

307-265-3100

John Finch

ID, MT, ND, SD, UT, WY

AUSTRALIA

CONCRETE

CSR Humes

61 7 3364-2933

Colin Roome

Australia

CSR Construction Materials

61 3 9286-2624

Keith Caporn

Pacific Rim



APPENDIX "F"
SOIL EROSION COMPUTATIONS

Sheet 1 E

CONDUIT OUTLET PROTECTION

PREFORMED SCOUR HOLE DESIGN

SOIL TEXTURE IN STABLE DOWNSTREAM CHANNEL IS
SANDY CLAY LOAM

| | | |
|--------------------------------------|---|----------|
| ALLOWABLE VELOCITY | = | 3.5 FPS |
| EXIT VELOCITY FROM CONDUIT | = | 5.0 FPS |
| DEPTH OF SCOUR HOLE | = | 1.5 FT |
| MAX. INSIDE CULVERT WIDTH | = | 36.0 IN. |
| MAX. INS. VERTICAL CULVERT DIMENSION | = | 36.0 IN. |
| FLOW RATE FROM CULVERT | = | 6.0 CFS |
| DEPTH OF TAILWATER | = | 0.6 FT |
| LENGTH OF SCOUR HOLE | = | 18.0 FT |
| WIDTH OF SCOUR HOLE | = | 15.0 FT |
| MEDIAN STONE DIAMETER FOR RIPRAP | = | 0.6 IN. |

SEE STANDARD 4.14 FOR DESIGN REQUIREMENTS AND DETAILS.

HEADWALL NO. 1A

CONDUIT OUTLET PROTECTION

RIPRAP APRON DESIGN

SOIL TEXTURE IN STABLE DOWNSTREAM CHANNEL IS
SANDY CLAY LOAM

| | | |
|--------------------------------------|---|----------|
| ALLOWABLE VELOCITY | = | 3.5 FPS |
| EXIT VELOCITY FROM CONDUIT | = | 5.5 FPS |
| MAX. INSIDE CULVERT WIDTH | = | 24.0 IN. |
| MAX. INS. VERTICAL CULVERT DIMENSION | = | 24.0 IN. |
| DEPTH OF TAILWATER | = | 0.4 FT |
| FLOW RATE FROM CULVERT | = | 18.0 CFS |
| LENGTH OF APRON | = | 25.5 FT |
| MEDIAN STONE DIAMETER FOR RIPRAP | = | 11.2 IN. |

THE BOTTOM WIDTH OF THE APRON MUST BE AT LEAST EQUAL TO THE BOTTOM WIDTH OF THE CHANNEL. THE STRUCTURAL LINING MUST EXTEND AT LEAST ONE FT ABOVE TAILWATER ELEVATION, BUT NO LOWER THAN 2/3 OF THE VERTICAL CONDUIT DIMENSION ABOVE THE CONDUIT INVERT.

THE SIDE SLOPES MUST BE 2:1 OR FLATTER.

THE BOTTOM GRADE MUST BE LEVEL.

THERE MUST BE NO OVERFALL AT THE END OF THE APRON OR AT THE END OF THE CULVERT.

SEE STANDARD 4.14 FOR DESIGN REQUIREMENTS AND DETAILS.

HW # 17A

CONDUIT OUTLET PROTECTION

RIPRAP APRON DESIGN

SOIL TEXTURE IN STABLE DOWNSTREAM CHANNEL IS
SANDY CLAY LOAM

| | | |
|--------------------------------------|---|----------|
| ALLOWABLE VELOCITY | = | 3.5 FPS |
| EXIT VELOCITY FROM CONDUIT | = | 7.6 FPS |
| MAX. INSIDE CULVERT WIDTH | = | 18.0 IN. |
| MAX. INS. VERTICAL CULVERT DIMENSION | = | 18.0 IN. |
| DEPTH OF TAILWATER | = | 0.4 FT |
| FLOW RATE FROM CULVERT | = | 12.0 CFS |
| LENGTH OF APRON | = | 22.3 FT |
| MEDIAN STONE DIAMETER FOR RIPRAP | = | 9.6 IN. |

THE BOTTOM WIDTH OF THE APRON MUST BE AT LEAST EQUAL TO THE BOTTOM WIDTH OF THE CHANNEL. THE STRUCTURAL LINING MUST EXTEND AT LEAST ONE FT ABOVE TAILWATER ELEVATION, BUT NO LOWER THAN 2/3 OF THE VERTICAL CONDUIT DIMENSION ABOVE THE CONDUIT INVERT.

THE SIDE SLOPES MUST BE 2:1 OR FLATTER.

THE BOTTOM GRADE MUST BE LEVEL.

THERE MUST BE NO OVERFALL AT THE END OF THE APRON OR AT THE END OF THE CULVERT.

SEE STANDARD 4.14 FOR DESIGN REQUIREMENTS AND DETAILS.

Conduit Outlet Protection

Horizontal Riprap Apron

Headwall Number = 17B

Q (cfs) = 0.52 cfs
Do (in.) = 6 in. = 0.50 ft.
Wo (in.) = 6 in. = 0.50 ft.

$q = Q/Do = 1.04$ cfs/ft.

Is the TW less than 1/2
the Do? y or n = y

Length

$La = 1.8(q/Do^{0.5}) + 7Do$ TW < 1/2 Do

$La = 3(q/Do^{0.5})$ TW > 1/2 Do

use $La = 1.8(q/Do^{0.5}) + 7Do$

$La = 6.15$ ft. increase by 25% use 8'

Width

Start Width = 3 Wo = 1.5 ft.

End Width

$W = 3 Wo + La$ TW < 1/2 Do

$W = 3 Wo + 0.4 La$ TW > 1/2 Do

use $W = 3 Wo + La$

$W = 7.65$ ft. Use 8'

Stone Size

TW = 0.10 ft.

$D_{50} = (0.016/Tw)q^{1.33}$

$D_{50} = 0.17$ ft.

$D_{50} = 2.02$ in.

1' thick gabion mattress with 3-4-inch angular stone is used - see detail on plan sheets

Conduit Outlet Protection

Horizontal Riprap Apron

Headwall Number = 24A

Q (cfs) = 5.8 cfs
Do (in.) = 15 in. = 1.25 ft.
Wo (in.) = 15 in. = 1.25 ft.

$q = Q/Do = 4.64$ cfs/ft.

Is the TW less than 1/2
the Do? y or n = n

Length

$La = 1.8(q/Do^{0.5}) + 7Do$ TW < 1/2 Do

$La = 3(q/Do^{0.5})$ TW > 1/2 Do

use $La = 3(q/Do^{0.5})$

$La = 12.45$ ft. Use 13'

Width

Start Width = $3 Wo = 3.75$ ft.

End Width

$W = 3 Wo + La$ TW < 1/2 Do

$W = 3 Wo + 0.4 La$ TW > 1/2 Do

use $W = 3 Wo + 0.4 La$

$W = 8.73$ ft. Use 9'

Stone Size

TW = 1.00 ft.

$D_{50} = (0.016/TW)q^{1.33}$

$D_{50} = 0.12$ ft.

$D_{50} = 1.48$ in.

1' thick gabion mattresses with 3-4-inch angular stone are use - see detail on plan sheets

Conduit Outlet Protection

Horizontal Riprap Apron

Headwall Number = 24C

$$Q \text{ (cfs)} = 6.3 \text{ cfs}$$

$$D_o \text{ (in.)} = 18 \text{ in.} = 1.50 \text{ ft.}$$

$$W_o \text{ (in.)} = 18 \text{ in.} = 1.50 \text{ ft.}$$

$$q = Q/D_o = 4.2 \text{ cfs/ft.}$$

Is the TW less than 1/2
the Do? y or n = n

Length

$$L_a = 1.8(q/D_o^{0.5}) + 7D_o \quad TW < 1/2 D_o$$

$$L_a = 3(q/D_o^{0.5}) \quad TW > 1/2 D_o$$

use $L_a = 3(q/D_o^{0.5})$

| |
|-----------------------------------|
| $L_a = 10.29 \text{ ft.}$ Use 11' |
|-----------------------------------|

Width

$$\text{Start Width} = 3 W_o = 4.5 \text{ ft.}$$

End Width

$$W = 3 W_o + L_a \quad TW < 1/2 D_o$$

$$W = 3 W_o + 0.4 L_a \quad TW > 1/2 D_o$$

use $W = 3 W_o + 0.4 L_a$

| |
|-------------------------------|
| $W = 8.62 \text{ ft.}$ Use 9' |
|-------------------------------|

Stone Size

$$TW = 1.50 \text{ ft.}$$

$$D_{50} = (0.016/TW)q^{1.33}$$

$$D_{50} = 0.07 \text{ ft.}$$

| |
|-----------------------------|
| $D_{50} = 0.86 \text{ in.}$ |
|-----------------------------|

1' thick gabion mattresses with 3-4-inch angular stone are use - see detail on plan sheets